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Geometric phases in soft materials

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Chapter 2.

Sonic Landau levels and synthetic gauge fields in mechanical metamaterials



Electronic systems subject to a uniform magnetic field experience a wealth of fascinating phenomena such as topological states [122] in the integer quantum Hall effect [100] and anyons associated with the fractional quantum Hall effect [123]. Recently, it has been shown that in a strained graphene sheet, electrons experience external potentials that can mimic the effects of a magnetic field, which results in the formation of Landau levels and edge states [99, 101]. Working in direct analogy with this electronic setting, pseudo-magnetic fields have been engineered by arranging CO molecules on a gold surface [92] and in photonic honeycomb-lattice metamaterials [88, 89].

In this chapter, we apply insights about wave propagation in the presence of a gauge field to acoustic phenomena in a nonuniform phononic crystal, using the appropriate mechanisms of strain-phonon coupling and frictional dissipation, in contrast to those present in electronic and photonic cases. The acoustic metamaterial context in which we implement gauge fields provides us with significant control [30, 90, 97] over frequency, wavelength, and attenuation scales unavailable in the analogous electronic realizations. For example, a metamaterial composed of stiff (e.g. metallic) components of micron-scale length may be suitable for control over ultrasound with gigahertz-scale frequencies, whereas cm-scale metamaterials may provide control over kHz-scale sound waves. We develop two strategies for realizing a uniform pseudo-magnetic field in a metamaterial based on the honeycomb lattice, i.e. “mechanical graphene” [63]. In the first strategy, we apply stress at the boundary to obtain nonuniform strain

in the bulk, which leads to a Landau-level spectrum, whereas in the second strategy, we exploit built-in, nonuniform patterning of the local metamaterial stiffness. This second strategy shows how the unique controllability of metamaterials can lead to novel designs inaccessible in the electronic context.

2.1 Mechanical graphene

We begin with a minimal, microscopic model of an acoustic metamaterial – a set of nodes positioned at the vertices of a honeycomb lattice and connected by rods to their nearest neighbors (see Fig. 2.1a) [63]. The compressional stiffness of the rods κ is determined by their fixed Young’s modulus E , variable cross-section area S , and length a via ES/a . We assume the rods to be so slender that their bending stiffness is significantly lower than their compressional stiffness. We model the rods as central-force harmonic springs, whose elastic energy U is given in terms of the strain $\delta r/a$ by $U(\delta r) = \frac{1}{2}\kappa(|\mathbf{r} + \delta\mathbf{r}| - a)^2$. For small strains, this energy can be linearized in terms of node displacements \mathbf{u}_1 and \mathbf{u}_2 as $U(\mathbf{u}_1, \mathbf{u}_2) = \frac{1}{2}\kappa(\mathbf{e} \cdot [\mathbf{u}_1 - \mathbf{u}_2])^2$, where $\mathbf{e} \equiv \mathbf{r}/|\mathbf{r}|$ is the unit vector along the spring. (In Fig. 2.1a, we define the initial configuration for the node positions and stiffnesses.) The total elastic energy associated with a unit cell at spatial point \mathbf{R} can be cast as

$$U_{\text{tot}}(\mathbf{R}) = U_1(\mathbf{R}, \mathbf{R}) + \frac{1}{2} [U_2(\mathbf{R}, \mathbf{R} - \mathbf{a}_1) + U_2(\mathbf{R} + \mathbf{a}_1, \mathbf{R})] + \frac{1}{2} [U_3(\mathbf{R}, \mathbf{R} - \mathbf{a}_2) + U_3(\mathbf{R} + \mathbf{a}_2, \mathbf{R})], \quad (2.1)$$

where by considering $\mathbf{u}_s(\mathbf{R})$ as the displacement of the s sublattice node of the unit cell centered at \mathbf{R} we defined

$$U_\alpha(\mathbf{R}_1, \mathbf{R}_2) = \frac{\kappa}{2} [\mathbf{e}_\alpha \cdot (\mathbf{u}_2(\mathbf{R}_2) - \mathbf{u}_1(\mathbf{R}_1))]^2, \quad (2.2)$$

which gives the potential energy of a single rod in the direction \mathbf{e}_α connecting two unit cells at points \mathbf{R}_1 and \mathbf{R}_2 . Note that we only considered the interaction between nearest neighbors, which guarantees that the interactions are only between the nodes from different sublattices. This consideration will lead to an effective chiral symmetry in this system, which as we will discuss later, will be crucial for the existence of topological sound modes in this setup.

Given this potential, we write down and solve the linear equation of motion for acoustic vibrations of the lattice:

$$-m\ddot{u}_i^\mu = \frac{\partial U}{\partial u_i^\mu} = \sum_{j,\nu} D_{ij}^{\mu\nu} u_j^\nu, \quad (2.3)$$

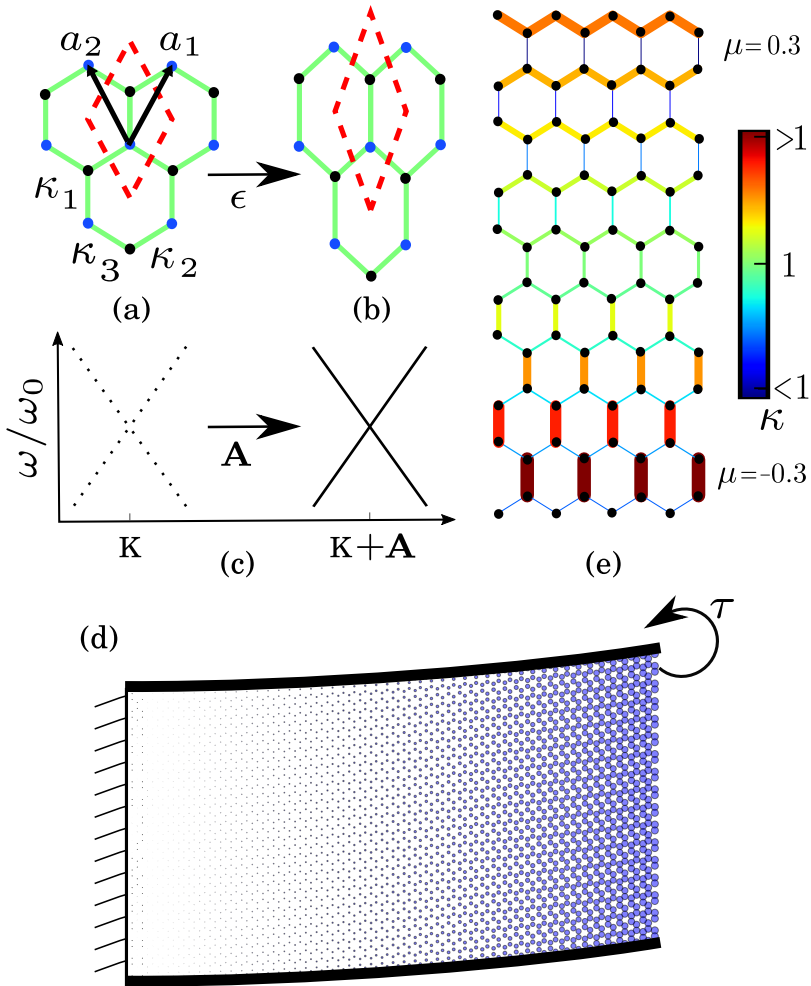


Figure 2.1: (a) Mechanical graphene – a set of rods and nodes based on the honeycomb structure. The dashed line indicates the shape of a unit cell. (b) The lattice with a pure shear strain. (c) The shift of a Dirac point within the phonon spectrum of mechanical graphene due to the applied strain can be used to define an effective vector potential. (d) An externally applied nonuniform pure shear deformation that corresponds to a constant magnetic field. The external stress is applied by a torque τ on the boundary rods. (e) A non-uniform patterning of the local material stiffness that leads to a constant magnetic field. We consider periodic boundary conditions along x and free boundary conditions along y .

where u_i^μ are the $\mu = x, y$ components of displacement of the i th site and $D_{ij}^{\mu\nu}$ are components of the dynamical matrix. In a periodic lattice, the solutions to this equation of motion are plane waves $\mathbf{u}_\mathbf{q} e^{i(\omega(\mathbf{q})t - \mathbf{q} \cdot \mathbf{x})}$, where both the dispersion relation $\omega(\mathbf{q})$ and the normal modes $\mathbf{u}_\mathbf{q}$ are found from the corresponding eigenvalue problem for each wavevector \mathbf{q} :

$$D(\mathbf{q})\mathbf{u}_\mathbf{q} = m\omega^2(\mathbf{q})\mathbf{u}_\mathbf{q}, \quad (2.4)$$

The dynamical matrix of the two-dimensional honeycomb lattice is:

$$D(\mathbf{q}) = \frac{1}{m} \sum_{\alpha=1}^3 \kappa_\alpha \begin{pmatrix} P_\alpha & -P_\alpha e^{i\mathbf{q} \cdot \delta_\alpha} \\ -P_\alpha e^{-i\mathbf{q} \cdot \delta_\alpha} & P_\alpha \end{pmatrix}, \quad (2.5)$$

where the projections $P_\alpha = \mathbf{e}_\alpha \mathbf{e}_\alpha^T$ and for the honeycomb lattice

$$P_1 = \begin{pmatrix} 0 & 0 \\ 0 & 1 \end{pmatrix}; \quad P_2 = \begin{pmatrix} 3/4 & \sqrt{3}/4 \\ \sqrt{3}/4 & 1/4 \end{pmatrix}; \quad P_3 = \begin{pmatrix} 3/4 & -\sqrt{3}/4 \\ -\sqrt{3}/4 & 1/4 \end{pmatrix} \quad (2.6)$$

The phonon dispersion relation $\omega(\mathbf{q})$ of the system can then be obtained from the square root of the eigenvalues of this dynamical matrix. This band structure exhibits a linear dispersion of the phonon modes around the Dirac point K [defined by $\mathbf{q}_K \equiv (0, 4\pi/3\sqrt{3}a)$], where the two middle bands are degenerate. Using first-order perturbation theory around the Dirac point, we find the following form for the dynamical matrix:

$$D(\mathbf{q}_K + \delta\mathbf{q}) \approx \omega_0^2 \begin{pmatrix} 0 & 0 & \frac{a(\delta q_x - i\delta q_y)}{2\sqrt{2}} & \frac{a(\delta q_x + i\delta q_y)}{2\sqrt{2}} \\ 0 & 2 & -\frac{a(\delta q_x - i\delta q_y)}{2\sqrt{2}} & \frac{a(\delta q_x + i\delta q_y)}{2\sqrt{2}} \\ \frac{a(\delta q_x + i\delta q_y)}{2\sqrt{2}} & -\frac{a(\delta q_x + i\delta q_y)}{2\sqrt{2}} & 1 & \frac{a(-\delta q_x - i\delta q_y)}{2} \\ \frac{a(\delta q_x - i\delta q_y)}{2\sqrt{2}} & \frac{a(\delta q_x - i\delta q_y)}{2\sqrt{2}} & \frac{a(-\delta q_x + i\delta q_y)}{2} & 1 \end{pmatrix}, \quad (2.7)$$

where $\omega_0 = \sqrt{3\kappa/2m}$ is the frequency of the degenerate bands at the Dirac point. We can then project the dynamical matrix for the two degenerate bands to get

$$D_r(\mathbf{q}_K + \delta\mathbf{q}) = \omega_0^2 \mathbb{1} - \frac{1}{2} \omega_0^2 a \delta\mathbf{q} \cdot \boldsymbol{\sigma} + \mathcal{O}(\delta\mathbf{q}^2), \quad (2.8)$$

where D_r is the reduced dynamical matrix for the two middle bands, $\mathbb{1}$ is the 2×2 identity matrix, $\delta\mathbf{q} \equiv \mathbf{q} - \mathbf{q}_K$, and $\boldsymbol{\sigma} \equiv (\sigma_x, \sigma_y)$ is composed of Pauli spin matrices

$$\sigma_x = \begin{pmatrix} 0 & 1 \\ 1 & 0 \end{pmatrix} \text{ and } \sigma_y = \begin{pmatrix} 0 & -i \\ i & 0 \end{pmatrix}. \quad (2.9)$$

From this reduced form, one can deduce that small perturbations on this system will lead to the following general form up to the lowest order in perturbation theory[♣]:

$$D_r(\mathbf{q}_K + \delta\mathbf{q}) = -\frac{1}{2}\omega_0^2(a\delta\mathbf{q} + \mathbf{A}) \cdot \boldsymbol{\sigma} + (1 + V)\omega_0^2\mathbb{1} + \mu\sigma_z, \quad (2.10)$$

where a gauge field \mathbf{A} minimally coupled to the momentum of the phonons[♡] and a potential V are introduced as a result. The sublattice breaking term which is proportional to the third Pauli matrix

$$\sigma_z = \begin{pmatrix} 1 & 0 \\ 0 & -1 \end{pmatrix} \quad (2.11)$$

will remain zero, as long as the perturbation does not violate the chiral symmetry. From the structure of Eq. (2.10), we note that the dispersion around \mathbf{q}_K has the form of a Dirac cone.

2.2 Synthetic gauge field

We now proceed to show that unlike uniform lattice deformations that merely shift this Dirac cone in wavevector space, nonuniform deformations can lead to an effective synthetic gauge field for sound. For uniform strain (Fig. 2.1b), \mathbf{A} and V are both constant throughout the lattice. On the other hand, for a nonuniform but slowly varying strain, the position of the local Dirac point varies from one region to another (Fig. 2.1c), which corresponds to fields \mathbf{A} and V that depend on spatial coordinates.

To see this, we consider a general deformation on the honeycomb structure with affine component \mathbf{U} and nonaffine component \mathbf{W} of the displacement denoting, respectively, the common and relative displacements of the two sublattices. The deformation of each sublattice is then given by $\mathbf{U}_{1,2} = \mathbf{U} \pm \mathbf{W}/2$, where the different signs correspond to the different sublattices. This deformation changes the components of the dynamical matrix via $\delta_\alpha \rightarrow \tilde{\delta}_\alpha$ and $P_\alpha \rightarrow \tilde{P}_\alpha$, where

$$\tilde{\delta}_\alpha = (I + \nabla\mathbf{U})\delta_\alpha + \mathbf{W} \quad (2.12)$$

$$\begin{aligned} \tilde{P}_\alpha &= P_\alpha + (\nabla\mathbf{U})P_\alpha + P_\alpha(\nabla\mathbf{U})^T \\ &+ (\mathbf{e}_\alpha^T \epsilon \mathbf{e}_\alpha + \mathbf{e}_\alpha^T \mathbf{W}/a) (I - 3P_\alpha) + \mathbf{e}_\alpha \mathbf{W}^T/a + \mathbf{W} \mathbf{e}_\alpha^T/a, \end{aligned} \quad (2.13)$$

[♣]Here, we use the fact that any general 2×2 Hermitian matrix can be expanded in the $\{\sigma_x, \sigma_y, \sigma_z, \mathbb{1}\}$ basis.

[♡]corresponding to a gauge transformation $u \rightarrow ue^{-i\mathbf{A} \cdot \mathbf{x}/a}$ in the wavefunction

and $(\nabla \mathbf{U})_{ij} = \partial_i U_j$. The potential energy of a single rod can now be expressed as

$$\tilde{U}_\alpha(\mathbf{R}_1, \mathbf{R}_2) = \frac{\kappa}{2} \left(\left| \tilde{\delta}_\alpha + \mathbf{u}_2(\mathbf{R}_2) - \mathbf{u}_1(\mathbf{R}_1) \right| - 1 \right)^2. \quad (2.14)$$

Taking the same steps as before, we find that the lattice deformations modify the dynamical matrix according to

$$\tilde{D}(\mathbf{q}) = \frac{1}{m} \sum_{\alpha=1}^3 \kappa_\alpha \begin{pmatrix} \tilde{P}_\alpha & -\tilde{P}_\alpha e^{i\mathbf{q} \cdot \tilde{\delta}_\alpha} \\ -\tilde{P}_\alpha e^{-i\mathbf{q} \cdot \tilde{\delta}_\alpha} & \tilde{P}_\alpha \end{pmatrix}. \quad (2.15)$$

We then obtain the gauge field

$$\begin{aligned} \mathbf{A}(x, y; \epsilon, W) = & a(\mathbf{q}_K \cdot \nabla) \mathbf{U} + \left[\frac{3}{2}(\epsilon_{xx} - \epsilon_{yy}), -3\epsilon_{xy} \right] \\ & + (W_y, -W_x)/a, \end{aligned} \quad (2.16)$$

and $V = \frac{1}{2} \text{Tr } \epsilon$, where $\epsilon_{ij} \equiv (\partial_i U_j + \partial_j U_i)/2$ is the linear affine strain.

To simplify the design of an acoustic device based on this strained lattice, we now consider those lattice strains that can be obtained by applying forces only on the boundary. Such a configuration requires that the forces in the bulk of the material balance each other. In the material we consider, this force-balance condition is satisfied provided that the nonaffine displacements depend on the affine strain via $W_x = \epsilon_{xy}a$ and $W_y = \frac{1}{2}(\epsilon_{xx} - \epsilon_{yy})a$, which can be obtained by solving the force-balance equation $\delta U_{tot}/\delta \mathbf{W} = 0$ using the total elastic potential energy. Thus, the resulting expression for the gauge field in a boundary-strained material is

$$\mathbf{A}(x, y; \epsilon) = a(\mathbf{q}_K \cdot \nabla) \mathbf{U} + [2(\epsilon_{xx} - \epsilon_{yy}), -4\epsilon_{xy}]. \quad (2.17)$$

For the acoustic systems under study we can also follow a second strategy: patterning the local material stiffness to achieve a spatially dependent gauge field \mathbf{A} . For example, we can smoothly vary the composition or thickness of the rods to change their effective spring constants to $\kappa_i = \kappa + \delta\kappa_i$, where $i = 1 \dots 3$ labels springs in the lattice unit cell. In this case, we find that the gauge field and potential are given by

$$\begin{aligned} \mathbf{A}(x, y; \delta\kappa) = & \left(-\frac{1}{3} \frac{2\delta\kappa_1 + \delta\kappa_2 + \delta\kappa_3}{\kappa}, \frac{\delta\kappa_2 - \delta\kappa_3}{\sqrt{3}\kappa} \right), \\ V = & \frac{\delta\kappa_1 + \delta\kappa_2 + \delta\kappa_3}{3\kappa}. \end{aligned} \quad (2.18)$$

One can then obtain a Landau-level spectrum by selecting \mathbf{A} and V such that (for units in which $a = 1$)

$$\nabla \times \mathbf{A} = B\hat{z} = \text{const}; \quad V = 0. \quad (2.19)$$

For any selection satisfying the conditions of Eqs. (2.19), the dynamical matrix in Eq. (2.10) has the form of the Hamiltonian for a Dirac electron in a plane with a constant magnetic field B applied perpendicular to that plane [163, 165]. Let us now consider two practical solutions to Eqs. (2.19): (i) an externally applied nonuniform pure shear deformation, and (ii) nonuniform patterning of the spring constants along the y -direction.

For case (i), we find the particle displacements throughout the lattice by substituting Eq. (2.17) into Eqs. (2.19) and solving the resulting partial differential equation: $\partial_y U_x + \partial_x U_y = -Bx/2$, with the additional constraint $\partial_x U_x = \partial_y U_y = 0$, which corresponds to nonvolumetric pure shear deformations. The resulting displacements satisfy

$$U_x = 0; \quad U_y = -Bx^2/4. \quad (2.20)$$

Note that for the honeycomb lattice, this condition can be realized using the boundary stresses illustrated in Fig. 2.1d.

For case (ii), we substitute Eqs. (2.18) into Eqs. (2.19) to find the condition

$$\sqrt{3}\partial_x(\delta\kappa_2 - \delta\kappa_3) - \partial_y(\delta\kappa_2 + \delta\kappa_3) = 3\kappa B \quad (2.21)$$

for the spatial dependence of the spring constants. We consider a material uniform along the x -direction. In this case, the condition in Eq. (2.21) is satisfied for spring constants given by

$$\mu \equiv \frac{\delta\kappa_2}{\kappa} = \frac{\delta\kappa_3}{\kappa} = -\frac{\delta\kappa_1}{2\kappa} = \frac{By}{3}, \quad (2.22)$$

which is visualized in Fig. 2.1e.

2.3 Mechanical Landau levels

Now that we have proposed metamaterial architectures that realize the acoustic analog of a constant magnetic field, we go on to explore the physical consequences of this field for sound waves. To proceed, we focus on an architecture that is peculiar to the acoustic context, i.e. we select the realization of a

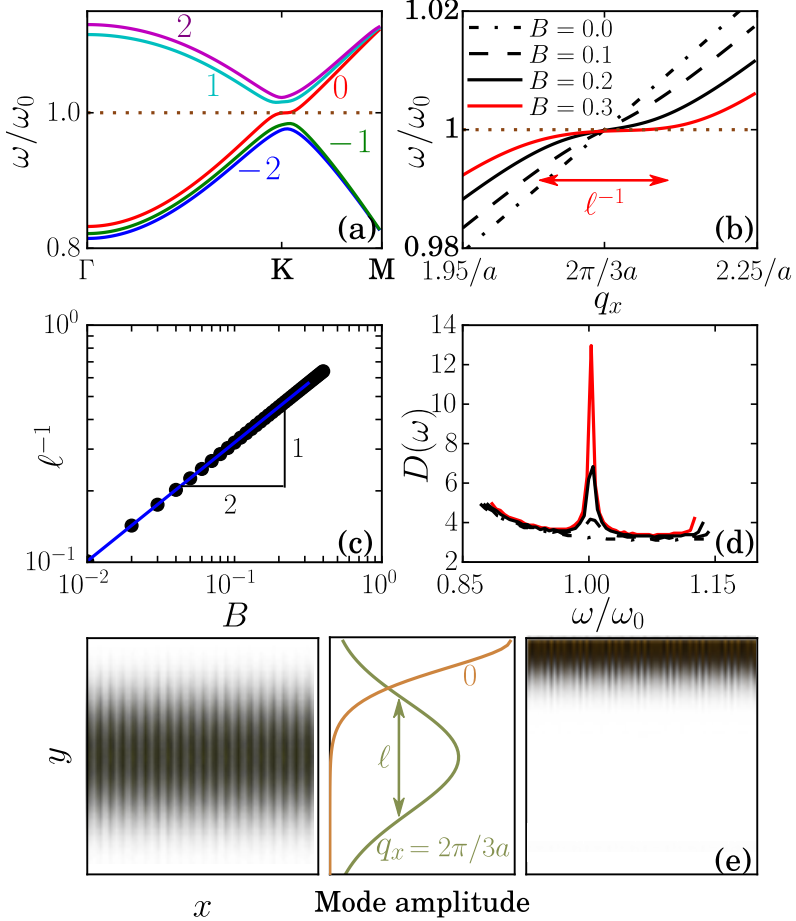


Figure 2.2: Mechanical Landau levels: (a) A pseudo-magnetic field leads to Landau levels around the Dirac point. (b) As the magnetic field increases, the zeroth-Landau-level band flattens. Band flatness can be characterized by the inverse magnetic length ℓ^{-1} . (c) The inverse magnetic length scales as the square root of the magnetic field. (d) Density of states for the zeroth Landau level, for the same values of B as in (b). The peak at the Dirac frequency rises as the bands flatten. (e) Visualizations of the zeroth Landau level at two different wavevectors. For $\mathbf{q} = \mathbf{q}_K$, this mode has a Gaussian profile around the waveguide center, whereas far from this point, at $\mathbf{q} = 0$, the mode decays exponentially away from the edge.

patterned metamaterial waveguide described by Eqs. (2.22). Such a quasi-one-dimensional waveguide is uniform along the x -direction, graded along the y -direction, and is subject to no-stress boundary conditions on its top and bottom (see Fig. 2.1e). The constant pseudo-magnetic field leads to a Landau-level spectrum for frequencies near ω_0 (Fig. 2.2a).

Let us focus on the acoustic band corresponding to the most prominent Landau level: $n = 0$. In Fig. 2.2b, this band is plotted for several values of the pseudo-magnetic field B ; as the pseudo-magnetic field increases, the band flattens over a larger region in wavevector space, which leads to an increasing peak in the density of acoustic states (shown in Fig. 2.2d). The width of this flat region defines an inverse length scale ℓ^{-1} , which scales as $\ell^{-1} \sim \sqrt{B/a}$ (Fig. 2.2c). This length scale is the acoustic analog of the magnetic length of a Landau-level state. Consequently, an acoustic mode in the Landau level has a Gaussian profile with a transverse confinement given by ℓ (Fig. 2.2e). The transverse location of this mode within the waveguide is controlled by the mode wavenumber q_x , in contrast to an index-graded waveguide in which the location is determined by the mode frequency. Consequently, in our case, the location of sound at a targeted frequency can be significantly tuned via the mode wavenumber (Fig. 2.2e and 2.4).

2.4 Sublattice-polarized domain wall modes

The $n = 0$ Landau level at $q_x = q_{K,x} \equiv 2\pi/3a$ has frequency ω_K , is located at the waveguide center, and involves displacements exclusively on one sublattice. Modes with these properties generically appear in regions across which A_x changes sign, i.e. their local dispersions have Dirac cones on opposite sides of point K . As an example, we consider a waveguide with two domain walls that separate a uniform central region with spring constants set by $\mu = -0.08$ from two regions, one above and one below, that each have $\mu = 0.08$ (Fig. 2.3a). At $q_x = q_{K,x}$, the spectrum as a function of q_y near point K is described by a gapped 1D Dirac Hamiltonian centered about ω_K , with effective mass proportional to A_x . The “spin” degree of freedom corresponds to the two sublattices of the honeycomb lattice: eigenstates of σ_z with eigenvalues $+1$ and -1 involve displacements solely on sublattice A and sublattice B, respectively. When the mass $m(y)$ varies spatially, domain walls at which $m(y)$ changes sign harbor exponentially localized midgap modes that are “spin-polarized”, i.e. confined to a single sublattice [172, 175]. The sublattice on which the mode

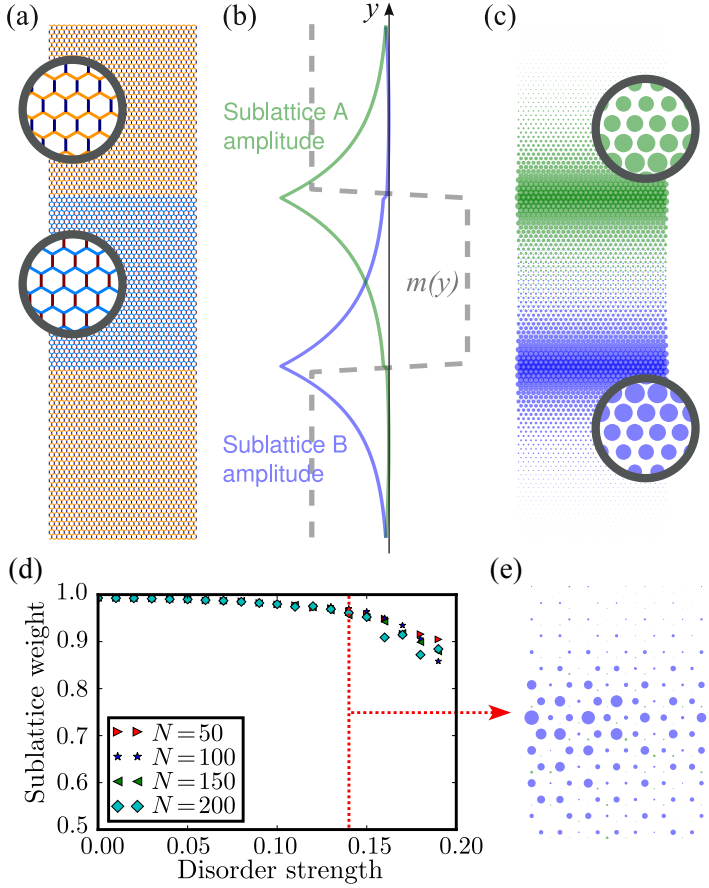


Figure 2.3: (a) Waveguide with two domain walls separating two regions with $\mu = 0.08$ from a central region with $\mu = -0.08$. The bonds are colored according to their spring constants as in Fig. 1(e). Periodic boundary conditions are applied along x . (b) Variation of the effective Dirac mass $m(y)$ (dashed line) and of the amplitude of the midgap mode at $q_x = 2\pi/3a$ on either sublattice (solid lines). (c) Visualization of the midgap mode with the sublattices distinguished. Each point is represented by a disc whose area is proportional to the amplitude of the midgap mode at that point. Points on sublattices A and B are drawn as green and blue discs respectively, showing the strong polarization of each domain wall mode onto a distinct sublattice. (d) The dependence of sublattice polarization of the domain-wall-bound mode on disorder in the spring constants. The polarization remains significant due to the topological origin of the mode (e) Even in the presence of strong (14%) disorder, we clearly observe the sublattice-polarized domain-wall-bound mode.

is localized is determined by the sign of the change in mass upon crossing the domain wall. Fig. 2.3b–c shows the numerically-obtained midgap mode for the domain wall geometry in Fig. 2.3a, whose components on sublattice A (sublattice B) fall off exponentially from the top (bottom) domain wall.

2.4.1 Connection to the Jackiw-Rebbi model

Some of our results for the sublattice-polarized modes can be understood using a connection between mechanical graphene and the Jackiw-Rebbi model [175]. Note that, for the waveguide described above, $\kappa_2 = \kappa_3$ and $V = 0$, which is equivalent to $\delta\kappa_2 = \delta\kappa_3 = -\delta\kappa_1/2 \equiv \kappa\mu$. This case with staggered spring constants along the y -direction is reminiscent of the Su-Schrieffer-Heeger model [172]. Using the formula for the synthetic gauge field in Eq. 2.18, we find the following form for the dynamical matrix:

$$D = D_0 + \frac{1}{3}\omega_0^2\mu(y)\sigma_x. \quad (2.23)$$

Thus, we see that the dimensionless parameter μ plays the role of the effective mass in the Jackiw-Rebbi model. For modes of the honeycomb-lattice waveguide near the Dirac frequency, we can obtain the form of the eigenmodes using the zero mode solution of the Jackiw-Rebbi model: $\mathbf{u}(y) \propto \exp[-\int_0^y \mu(y) dy]$. Thus, for the sharp domain wall of Fig. 3, for which the effective mass is a step-function, we find solutions at the domain wall which decay exponentially away from the domain wall. On the other hand, for a mechanical Landau-level mode obtained using material patterning, the mass varies linearly with y , i.e. $\mu \propto y$, and the mode indeed has a Gaussian profile (see Fig. 2.4). Furthermore, the solutions to the Jackiw-Rebbi model exhibit a parity anomaly, which can be used to ascertain that the domain-wall-bound modes as well as the Landau-level modes are both sublattice-polarized.

2.4.2 Topological robustness of the domain-wall mode

In this part, we explain in detail the robustness of the sublattice-polarized domain wall mode in the presence of disorder.

As explained in the previous section, a domain wall across which the mass $\mu(y)$ in Eq. (2.23) changes sign will always carry a domain-wall-bound mode. Intuitively, this mode corresponds to a Landau-level-like mode but in the presence of a spatially dependent magnetic field given by the derivative $\mu'(y)$. Thus, the existence of the domain-wall bound mode requires μ to change (and, in particular, change in sign) across the domain wall.

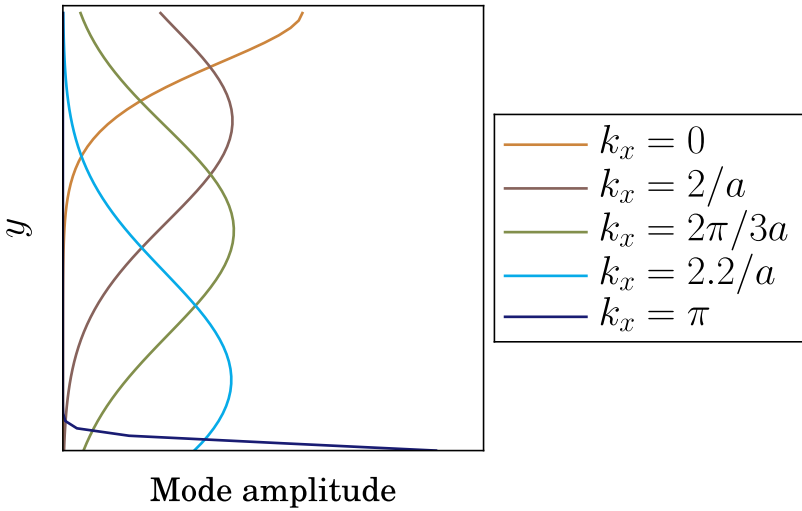


Figure 2.4: Visualizations of the zeroth Landau level for different wavenumbers. For $q_x = 2\pi/3a$, this mode has a Gaussian profile and is located precisely at the waveguide center due to a symmetry of the Dirac cone: the modes with frequency above (below) ω_K live on the lower (upper) half of the waveguide. We observe edge states with Gaussian profiles for wavenumber q_x near $2\pi/3a$. For example, when $q_x = 2/a$ (thus $q_x < 2\pi/3a$) the mode has a Gaussian profile and is located near the top edge of the waveguide (brown curve). In contrast, when $q_x = 2.2/a$ (thus $q_x > 2\pi/3a$) the mode has a similar shape, but is located near the bottom edge of the waveguide (light blue curve). Far from the Landau level, at $q_x = 0$ (π), the mode decays exponentially away from the top (bottom) edge. This figure is an expansion of Fig. 2.2e.

One of the consequences of nonzero μ is to break a chiral symmetry in this system. This chiral symmetry preserves the reflection symmetry of the Dirac cone: the cone looks the same right-side up as upside-down. Furthermore, this is the symmetry necessary to preserve the sublattice polarization (i.e. the fact that the mode lives on only one of the two sublattices) of the domain-wall bound mode. From the fact that μ has to vary across the domain wall and this violation of chiral symmetry, one might suppose that the domain-wall mode's existence also seems to presuppose that it will not be robust against disorder. However, quantitatively, the terms that break this chiral symmetry are small so that the domain-wall modes are nearly perfectly polarized on one sublattice (see Figs. 2.6 and 2.7).

Let us first explain the origins of topological robustness in this system and how it relies on chiral symmetry. If the dynamical matrix has form

$$D = \begin{pmatrix} 0 & H \\ H^\dagger & 0 \end{pmatrix}, \quad (2.24)$$

then we say that the system does have chiral symmetry. For this dynamical matrix, we can calculate the *winding number* of $\det H$, which is the integral of $\nabla_{\mathbf{k}} \ln \det H$, over a periodic contour γ in the Brillouin zone. The determinant $\det H$ is a complex number for each wavevector, and traces out a closed path in the complex plane as the wavevector follows the contour γ (see Fig. 2.5b). The integral counts how many times the path encloses the origin $\det H = 0$, and in particular, $\frac{1}{2\pi i} \int_{\gamma} d\mathbf{k} \cdot \nabla_{\mathbf{k}} \ln \det H$ is unity when the origin is enclosed once and zero otherwise. It thus forms a topological invariant for our system, which is called the *Herring number* in the context of Dirac cones [63, 190]. Only in the case when the vector potential is zero does this integral become not well-defined, because in that case the contour passes through the center of the Dirac cone, at which point $\det H = 0$.

Notably, in our system, D has the form of Eq. (2.24) only near the Dirac cone. Away from points K and K' , chiral symmetry does not hold and other diagonal terms enter the dynamical matrix. However, near the Dirac cone, where all of the phenomena considered in this work take place, these achiral terms are small and the chiral symmetry holds approximately. As a result, the topological robustness associated with this chiral symmetry can also be observed, as we explore in Fig. 2.7 for the sublattice polarization.

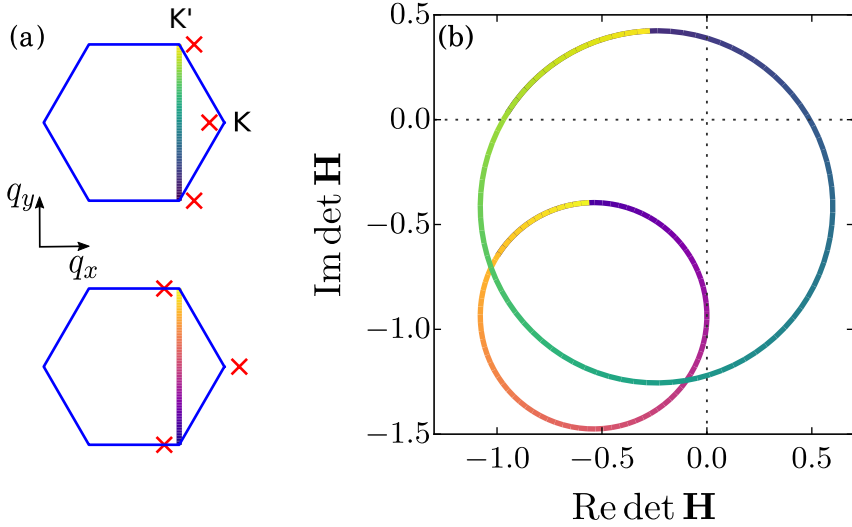


Figure 2.5: Topological invariants in a 2D Brillouin zone with a constant gauge field \mathbf{A} . (a) A schematic of the location of the Dirac points when the gauge field is constant. When $\mathbf{A} = (A_x, 0)$ and the x -component A_x is positive, the Dirac cone at \mathbf{q}_K shifts to the left and the cone at $\mathbf{q}_{K'}$ shifts to the right (top panel). For A_x negative, these cones shift in the opposite direction. When the Dirac cones shift, it is possible to define a winding contour around the Dirac cones that connects $\mathbf{q}_{K'}$ with itself via a vertical path across the Brillouin zone. (b) When the quantity $\nabla_{\mathbf{k}} \ln \det H$ [see Eq. (S7)] is integrated along the contour defined in (a), as long as the chiral symmetry of the honeycomb lattice is respected, the resulting quantity is an integer called the Herring number. This number is zero when $A_x > 0$ (small circle, which doesn't enclose the origin) and unity when $A_x < 0$ (large circle, which does enclose the origin). Thus, this number counts the Dirac cones within the contour and can only change when the sign of A_x changes as, e.g. in the case of the Landau level or the domain wall.

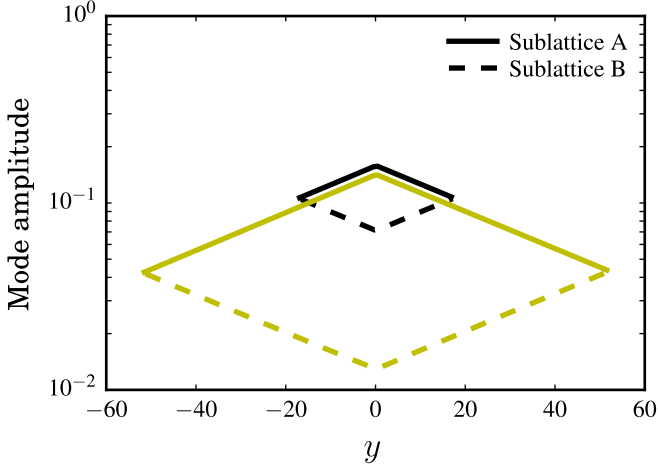


Figure 2.6: Amplitude of the midgap mode for quasi-one dimensional waveguides with different sizes $N = 20$ (black) and $N = 60$ (yellow) along the transverse direction plotted on a log-linear scale. For each system size, the amplitude of the vibrational mode on the two sublattices A and B are shown as solid and dashed lines respectively, as a function of y -position relative to the domain wall at $y = 0$. The component on sublattice A decays exponentially away from the domain wall, similar to the exponentially decaying domain-wall mode shown in Fig. 2.3b. The mode also has a component on sublattice B, which decays exponentially away from the waveguide edges. This component arises because an edge termination is similar to a domain wall with a different mass sign change compared to the actual domain wall in the system. The relative amplitudes of the two components are set by the boundary conditions at the edges: the loose node condition at the system edge requires that $\mathbf{u}_A = \mathbf{u}_B$, as the nodes at the boundary can not balance a nonzero force from the interior springs.

To check that the sublattice polarization remains significant in the presence of system disorder, we have performed numerical simulations of disordered waveguides. In Figure 2.7 we present the results of these simulations in which we note that although increasing disorder does somewhat affect the sublattice polarization, the effect is small in absolute terms. Even when the disorder strength is around 15% of the initial spring stiffness, the mode remains polarized within 5% of its initial, near-perfect, polarization.

2.5 Selective enhancement

The sublattice polarization of the Landau-level states can be used to selectively enhance these modes under external drive by employing site-dependent damping. For example, for positive magnetic fields, the Landau-level states live only on the A-sublattice of the honeycomb unit cell [99, 163]. If we introduce damping of the form $-\gamma\dot{\mathbf{u}}_B$ into the equation of motion, Eq. (2.3), such that only the displacements of the B-sublattice are damped, then the Landau-level acoustic waves would not be attenuated, whereas the rest of the sound waves, which generically are split between the A and B sublattices, would have a nonzero attenuation. To characterize this selective enhancement, we study the attenuation rate $\eta(\mathbf{q})$ as a function of mode wavevector, as well as the self-response function $\chi(\omega)$ which measures the displacements in response to a drive at frequency ω .

We use the drag matrix $\Gamma = \begin{pmatrix} \gamma_{\parallel} & 0 \\ 0 & \gamma'_{\parallel} \end{pmatrix}$ with $\gamma' = 0$ to model sublattice-biased dissipation. With the presence of these drag forces, the equation of motion becomes $m\ddot{\mathbf{u}} + \Gamma\dot{\mathbf{u}} + D\mathbf{u} = 0$. Now consider an external driving force $\mathbf{F}(\mathbf{R}, t) = \mathbf{F}(\mathbf{R})e^{i\omega t}$ which oscillates in time. With this force, the inhomogenous equation of motion is $m\ddot{\mathbf{u}} + \Gamma\dot{\mathbf{u}} + D\mathbf{u} = \mathbf{F}$. To find the solutions, we use Bloch functions, i.e. the normal modes of the periodic structure, to expand the drive as $\mathbf{F}(\mathbf{R}, t) = e^{i\omega t} \sum_{n\mathbf{k}} \mathbf{F}_{n\mathbf{k}} \mathbf{u}_{n\mathbf{k}} e^{i\mathbf{k}\cdot\mathbf{R}}$. A steady-state solution, if it exists, oscillates with the same frequency ω as the drive. The steady-state solution can be expanded as $\mathbf{u}(\mathbf{R}, t) = e^{i\omega t} \sum_{\mathbf{k}} c_{n\mathbf{k}} \mathbf{u}_{n\mathbf{k}} e^{i\mathbf{k}\cdot\mathbf{R}}$. From the equation of motion, we find that the coefficients $c_{n\mathbf{k}}$ obey

$$c_{n\mathbf{k}} = \frac{\mathbf{F}_{n\mathbf{k}}}{-m\omega^2 + i\Gamma_{n\mathbf{k}}\omega + \lambda_{n\mathbf{k}}}, \quad (2.25)$$

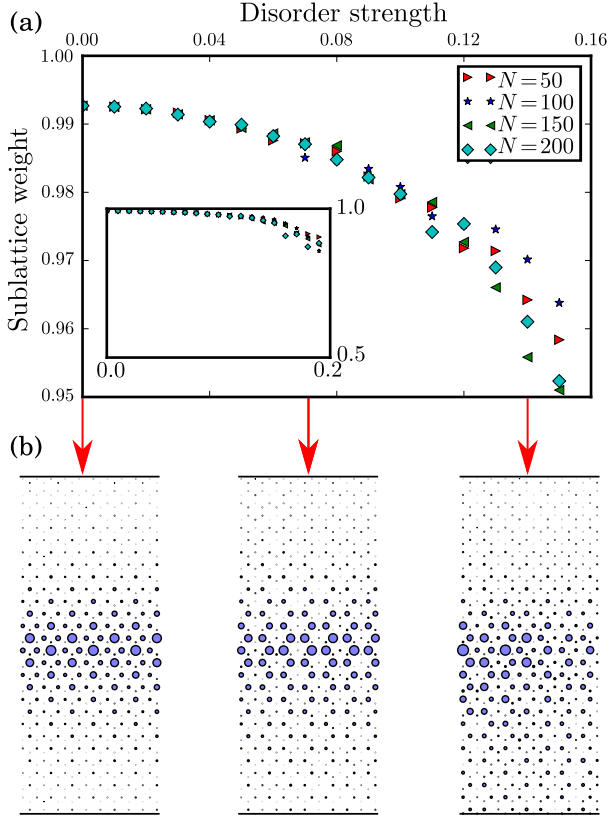


Figure 2.7: Effect of disorder in the spring constants on the sublattice polarization of modes bound to domain walls (see Fig. 2.3). (a) We consider waveguides that are infinite along the x -direction and have N unit cells along the y -direction. The disorder is implemented by rescaling each spring constant with spring constant $\kappa + \delta\kappa$ by a random number X via $(1 + X)\kappa + \delta\kappa$, where X is chosen from a uniform distribution on the interval $[-s, s]$ where we call the number s the disorder strength (x -axis of panel a). We then plot the relative weight of each mode on a sublattice averaged over 100 realizations of the disorder in panel (a). We note that it is always near unity (see inset). Even for disorder strength $\sim 10\%$, we note that the modes are still mostly polarized on one sublattice. Even for the most disordered cases we consider, the relative sublattice weight is 0.95, which indicates that the sublattice polarization of the domain-wall bound mode is robust against disorder in the spring constant. (b) Domain-wall bound mode amplitudes on each lattice site for several realizations of the disorder, with different disorder strengths. We note that even in the case in which the effects of the disorder on the mode are appreciable, the mode is still very strongly polarized on one of the sublattices.

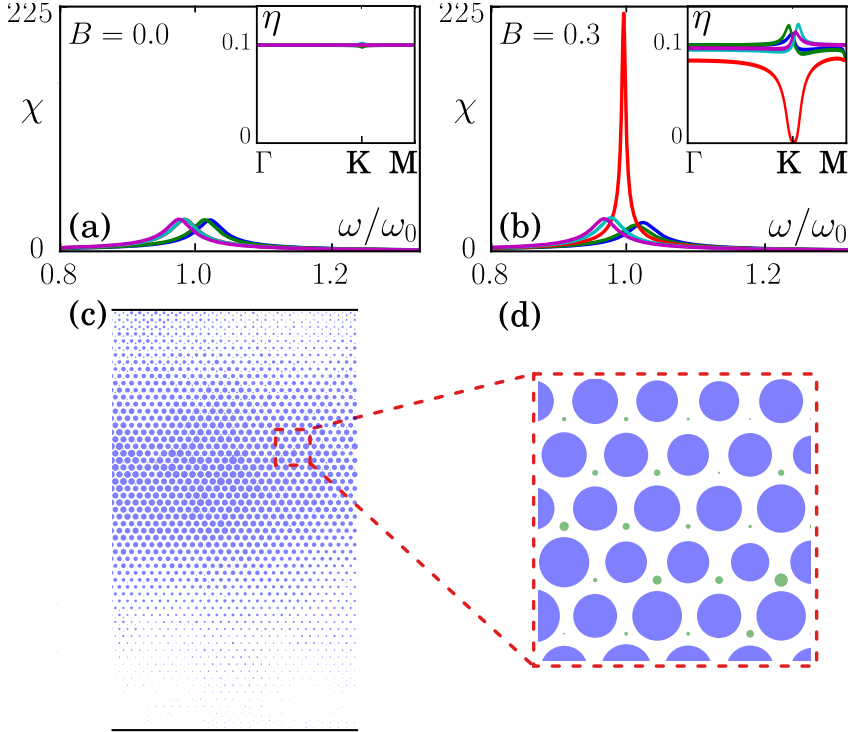


Figure 2.8: Single-mode response χ of Landau-level states in mechanical graphene, including the effect of damping on one sublattice and for pseudo-magnetic field values (a) $B = 0.0$ and (b) $B = 0.3$. Colors correspond to the different Landau-level bands identified in Fig. 2a. Insets: wavenumber-dependent attenuation rate η of the corresponding bands. (c) The steady-state response (for $B = 0.3$) to external periodic forcing with frequency close to the Dirac frequency and at an edge that is situated 50 unit cells to the left of the section shown. Each point is represented by a disc whose area is proportional to the amplitude of the response. (d) Zoom-in of (c) shows that the Landau-level mode is selectively enhanced due to the presence of sublattice-biased damping.

where $\Gamma_{n\mathbf{k}} = \sum_{n'} \mathbf{u}_{n'\mathbf{k}}^\dagger \Gamma \mathbf{u}_{n\mathbf{k}}$ and $\lambda_{n\mathbf{k}}$ are the eigenvalues of the dynamical matrix, Eq. 2.4. We expect the response to depend strongly on the damping. To see this, consider $\Gamma_{n\mathbf{k}}$ to be a real number. If $\Gamma_{n\mathbf{k}}^2 > 2\lambda_{n\mathbf{k}}m$ (corresponding to the overdamped limit), then the amplitude of the response never rises above $\mathbf{F}_{n\mathbf{k}}/\lambda_{n\mathbf{k}}$ – it attains this limiting value at low frequencies and falls off as $\mathbf{F}/m\omega^2$ at higher frequencies. If on the other hand, $\Gamma_{n\mathbf{k}}^2 < 2\lambda_{n\mathbf{k}}m$ (corresponding to the underdamped limit), the response develops a peak at $\omega_p^2 = \lambda_{n\mathbf{k}}/m - \Gamma_{n\mathbf{k}}^2/2m^2$, whose height diverges as $1/\Gamma_{n\mathbf{k}}$. Therefore, at low damping, the response will be dominated by modes whose natural frequency is close to the driving frequency. If for example, the lattice is driven by forcing atoms along one edge in an oscillatory manner, then $\mathbf{F}_{n\mathbf{k}}$ will be appreciable for several modes, but the only modes to have a strong response will be those whose natural frequency is close to the driving frequency.

This observation can be used to selectively enhance the zeroth Landau level mode, as seen in Fig. 2.8. In Fig. 4a-b, we plot $\chi(\omega) \equiv c_{n\mathbf{k}}/F_{n\mathbf{k}}$ for the Landau-level bands with $-2 \leq n \leq 2$, in response to an oscillatory drive that is proportional to the corresponding mode displacement vector, for $\mathbf{k} = \mathbf{q}_K$. In the absence of the pseudo-magnetic field B , the response is underdamped, but no mode stands out as having a largest peak in χ (Fig. 2.8a), whereas for nonzero B , χ exhibits a strong peak at a frequency ω_0 , corresponding to the zeroth Landau-level (Fig. 2.8b). In the insets, we plot the attenuation rates η , corresponding to the imaginary parts of the frequency spectrum, for these modes as a function of \mathbf{k} along the ΓKM cut of the Brillouin zone. We also observe from here that the zeroth Landau level mode is selected for nonzero B : it smaller attenuation than the other modes. We then drive the lattice with force $\mathbf{F}(t) = e^{i\omega t} \hat{x}$ (ω near ω_0), on two of the lattice points (near but slightly above the waveguide center), and observe the amplitude of the steady-state response sufficiently far away from this drive. We note that the pseudo-magnetic field combined with selective damping leads to selective enhancement of acoustic Landau-level modes relative to the rest of the attenuated acoustic spectrum.

2.6 Towards mechanical lasers

This phenomenon is the acoustic analog of selective enhancement of microwave modes realized in Ref. [72]. Just as selective enhancement for light waves may lead to the design of novel parity-time-symmetric [78, 81] and topological [89] lasers, analogously, the selective enhancement of sound waves may be useful in the design of sound amplification by stimulated emission

of radiation (SASERs), i.e. the acoustic analog of lasers, as well as acoustic couplers and rectifiers. The detailed design of such devices [87] would involve acoustic resonators, an acoustic drive, and nonlinearity of the response. A potential architecture for this device may involve resonators at every node in the metamaterial, with an external acoustic source populating the states within each resonator.

2.7 Conclusion

We explored acoustic phenomena associated with the Landau-level spectrum. For example, the acoustic analog of Shubnikov-de Haas oscillations [192] corresponds to a sharp peak in the phonon density of states at the Landau-level frequency. In addition, sound modes are confined within a length scale set by the analog of the magnetic length. Our theoretical findings pave the way towards realizations of these acoustic phenomena associated with the synthetic gauge fields [21]. In §2.4, we showed that even stronger confinement of sound modes can be engineered at a domain wall associated with a change in the effective mass of the phononic excitations, which localizes phonon modes that are analogous to the topological domain-wall states in the Su-Schrieffer-Heeger model of polyacetylene [172]. In §2.5, we showed how this domain-wall-bound mode exhibits robustness against a type of disorder that may come in the manufacturing of acoustic metamaterials – disorder in the stiffness of each component. Like other realizations of topological states [95, 109] in mechanical [44, 49, 53, 54, 55, 68, 70, 71, 73, 77, 82], acoustic [37, 57, 62, 64, 67, 74, 75, 76], and photonic [17, 83, 85, 86, 88], metamaterials, this characterization may help with the design of robust devices. We show that introducing dissipation on just one of the two sublattices enhances the domain-wall-bound sound mode. This feature may be implemented in the acoustic context by considering a material immersed in a viscous fluid (appropriate for low-Reynolds number, e.g. micro-scale metamaterials), or by including dampers (e.g. small dashpot dampers at every components for cm-scale realizations) within the material design. We suggest this feature may be exploited for the design of acoustic couplers, rectifiers, and sound amplification by stimulated emission of radiation (SASERs).