

Automated planning approaches for non-invasive cardiac valve replacement procedures from CT angiography Gao, X.; Gao X.

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Automatic Detection of Aorto-femoral Vessel Trajectory from Whole-body Computed Tomography Angiography Data Sets

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Abstract

Purpose: Extraction of the aorto-femoral vascular trajectory is important to utilize computed tomography angiography (CTA) in an integrated workflow of the image-guided work-up prior to trans-catheter aortic valve replacement (TAVR). The aim of this study was to develop a new, fully-automated technique for the extraction of the entire arterial access route from the femoral artery to the sino-tubular junction.

Methods: An automatic vessel tracking algorithm was first used to find the centerline that connected the femoral accessing points and the aortic valve. Subsequently, a deformable 3D-model fitting method was used to delineate the lumen boundary of the vascular trajectory in the whole-body CTA dataset. A validation was carried out by comparing the automatically obtained results with semi-automatically obtained results from two experienced observers.

Results: The whole framework was validated on whole body CTA datasets of 36 patients. The average Dice similarity indexes between the segmentations of the automatic method and observer 1 for the left ilio-femoral artery, the right ilio-femoral artery and the aorta were 0.977 ± 0.030 , 0.980 ± 0.019 , 0.982 ± 0.016 ; the average Dice similarity indexes between the segmentations of the automatic method and observer 2 were 0.950 ± 0.040 , 0.954 ± 0.031 and 0.965 ± 0.019 , respectively. The inter-observer variability resulted in a Dice similarity index of 0.954 ± 0.038 , 0.952 ± 0.031 and 0.969 ± 0.018 for the left ilio-femoral artery, the right ilio-femoral artery and the aorta. The average minimal luminal diameters of the ilio-femoral artery were 6.03 ± 1.48 mm, 5.70 ± 1.43 mm and 5.52 ± 1.32 mm for the automatic method, observer 1 and observer 2 respectively. The minimal luminal diameters of the aorta were 13.43 ± 2.54 mm, 12.40 ± 2.93 mm and 12.08 ± 2.40 mm for the automatic method, observer 2 respectively. The automatic measurement overestimated the minimal luminal diameter slightly in the ilio-femoral artery at the average by 0.323 mm (SD= 0.49mm, p<0.001) compared to observer 1 and by 0.51mm (SD = 0.71mm, p<0.001) compared to observer 2.

measurements of the entire arterial accessing route that can be used to support TAVR procedures. To the best of our knowledges, this approach is the first fully automatic segmentation method of the whole aorto-femoral vessel trajectory in CTA images.

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3.1 Introduction

Aortic valve stenosis is a disease particularly prevalent among senior citizens over the age of 65 years (Nkomo et al. 2006). If left untreated, it is associated with a significant mortality. Historically surgical aortic valve replacement (SAVR) was used to treat this disease. Unfortunately, not all patients are suitable for such a procedure. Especially, SAVR may be associated with a high perioperative mortality risk in elderly patients (Nkomo et al. 2006; Schoenhagen, Hausleiter, et al. 2011). Trans-catheter Valve Replacement (TAVR) / Trans-catheter Aortic Valve Aortic Implantation (TAVI) has been developed as a therapeutic option during the last decade for the inoperable or very high-risk patients (Zajarias and Cribier 2009).

To minimize the procedure-related complications, special attention should be given to the selection procedure to decide which patients are suitable TAVR candidates. Computed tomography (CT) imaging has been proven to be able to predict vascular complications among patients undergoing transfemoral transcather aortic valve replacement (TF-TAVR) (Krishnaswamy et al. 2014). Evaluation of the size and tortuosity of the ilio-femoral arteries is required to determine the feasibility of a transfemoral (TF) approach (Agarwal et al. 2015; Schoenhagen, Kapadia, et al. 2011). Furthermore, the size of the entire aorta is also needed for proper device selection in TAVR (Achenbach et al. 2012; Leipsic et al. 2011). To integrate such measurements seamlessly and conveniently into the TAVR clinical workflow, a fully automatic framework was developed, allowing detection of the femoral/aorta access route and the vessel sizes based on 3D contour detection approaches.

In the literature, several approaches have been described for the detection of the arterial contours in CTA data sets. David Lesage et al al. 2009) reviewed the state-of-the-art (Lesage et on vascular segmentation in multi-modality images. The model-based vascular segmentation approach is commonly used. In our study, the vessel surface was modeled by a centerline curve with a generalized cylinder. This crosssection model with prior shape information can reduce the complexity of the contour detection procedure (Kitslaar et al. 2015).

The approach that we have taken consists of 2 steps (Fig 3.1), firstly, a centerline extraction from the femoral arteries to the aortic root (Gao et al. 2014); and secondly, a 3D contour detection approach using a subdivision surface model fitting method to accurately delineate the vascular access route (Kitslaar et al. 2015). Validation of this study was realized on 36 CTA datasets which were acquired during routine clinical practice prior to the TAVR procedures.



Fig 3.1. The general pipeline of trajectory contour detection, including two steps: centerline extraction and contour detection.

3.2 Methods

<u>Centerline extraction</u>

Since the details of the fully automatic centerline extraction algorithm were published in (Gao et al. 2014), we briefly summarize the steps below.

The CTA datasets were resampled at first to reduce the computation time. The centerline extraction step was executed on the resampled images. A wave-propagation algorithm was used, starting from the aortic arch which is detected automatically. To detect the aorta arch, prior knowledge about aorta diameter from clinical research (Mao et al. 2008) was integrated into a Gaussian probabilistic distribution model (Metz et al. 2009). After calculating the probabilistic model, a probability map was generated. From a point in the aorta arch, the algorithm propagated in two directions. One side propagated into the aortic root, and the other side propagated into the femoral arteries. After the wave propagation, the result image was used as a weight image for the Dijkstra shortest path algorithm. The Dijkstra algorithm was executed twice. First, to extract the centerline from the left femoral artery end to the aortic root. Second, to extract the centerline from the right femoral artery end to the aortic root. After these two centerlines were found, the bifurcation point of the two centerlines was detected. Finally, the centerlines were split into 3 parts: the centerline in the aorta, in the left ilio-femoral artery and in the right ilio-femoral artery.

Next, the centerlines in the femoral arteries were improved by a centerline refinement step. For this, a multi-scale medialness response based wave-propagation scheme (Gülsün and Tek 2008) was used. First, multi planar reconstruction (MPR) transversal image slice stacks were generated according to the initial centerline along the femoral artery. Next, the medialness response was computed from a circle centered at the initial centerline point, with multi-scale radius. This response was constructed as to give high values inside the center of the lumen and lower values inside calcifications. The response was used as the speed function for the wave propagation and back tracking method to generate the final refined centerline. Fig 3.2 shows an example of the comparison of the automatic extracted centerline and the refined centerline.



Fig 3.2. Result of centerline refinement step. The red crosses are the original centerline points; the blue crosses are the refined centerline points. The blue points avoid the calcium, and are better located in the middle of the cross-section of the artery lumen compared to the red points.

Contour detection

The vascular trajectory was segmented by a deformable model fitting method (Kitslaar et al. 2015). The deformable model was constructed from a coarse surface mesh representation created from the obtained centerlines. From this coarse mesh a smooth higher resolution surface mesh was created using a standard subdivision refinement scheme. This higher resolution subdivision surface was next deformed by iteratively updating the coarse mesh description by fitting to the lumen edge information in the CT scans. In (Kitslaar et al. 2015), this model was applied in CTA images of the carotid artery including bifurcations, and provided good results. A big advantage of the subdivision surface approach is that it is able to model the bifurcation of the iliac arteries.

Pre-processing

In our study, whole-body CTA datasets were used. In these images different kinds of anatomic tissues can be distinguished. The surrounding background of the contrast-filled vessels is quite complex and may confuse the subdivision surface fitting. For our purposes, we distinguished two background categories: high intensity tissue (calcifications, bones, and metal artifacts), and low intensity tissue (muscles, fat, liver etc.). We masked out the surrounding background by an adaptive threshold method similar to Shahzad et al (Shahzad et al. 2013).



Fig 3.3. Intensity profile along the centerline (yellow curve), polynomial curves (green).Yellow curve: intensity values in HU of the voxels along the centerline (in mm). Green curves: 2nd order polynomial fit (b) of the intensity values with standard deviation margin above (a) and below (c).

This method is based on the assumption that the HU value (intensity) along the artery should be a smooth gradual decreasing curve when this artery is without the presence of calcium (Steigner et al. 2010).

Based on this, an intensity profile of the voxels along our initially extracted centerline was extracted (Fig 3.3). Next, a 2nd order polynomial curve was fitted through the intensity profile data; this curve simulated the ideal case without calcium. Curve "b" in Fig3. shows this polynomial fit curve. Also shown is curve "a" which is an upward shifted version of curve "b" obtained by adding a constant value proportional to the standard deviation of the intensities in the profile. The values on curve "a" were used as the intensity threshold values for the high intensity structures (e.g calcium) on the corresponding image slices along the vessel centerline. A similar method was used to find the tissue with lower intensity than the contrast-filled lumen using curve "c" which is a downward shifted version of curve "b". Fig 3.4 shows examples of the original and mask slices in the CTA data using this method.



Fig 3.4. Examples of pre-processed slices. (a). original femoral artery image (b) processed femoral artery image (c) original aorta image (d) processed aorta image. The purple arrows in (a) and (b) indicate low intensity tissue that has been removed in processed image, other arrows indicate the processed high intensity tissue.

Model fitting

The deformable model was initialized from the centerline curves as a generalized cylinder with local diameter information obtained during the centerline extraction step (Gao et al. 2014). At the bifurcation a dedicated model was used to best describe the current bifurcation configuration. After initialization, the complete surface model was subdivided using the Loop subdivision scheme to generate a smoother surface model (Loop 1987). The subdivision surface model fitting was next performed on the processed intensity image. The fitting of the surface was based on the iterative movement of the control points according to the computed image forces.

During the deformation iterations, a re-initialization step was used (Kitslaar et al. 2015). During this re-initialization, a new subdivision surface model is generated based on the current fitted surface. For this, new centerline and diameter information was extracted from the current deformed subdivision surface and used to initialize the new surface model.

The re-initialization allows adapting the surface mesh model to various vessel radii in the vessel trajectory.



Fig 3.5. a, self-intersection in 2d cross-section contour b. 3D surface with selfintersection c.d. 2D cross section contour and 3D surface with no self- intersection when using a non-self-intersection force.

To prevent unwanted deformations during the fitting, a non-self-intersection force was used, similar to the method in (Park et al. 2001) (see Fig 3.5).

The whole algorithm pipeline was implemented in C++ and Python using the MeVisLab environment (version 2.7, Bremen, Germany).

VALIDATIONS

Segmentation evaluation

To evaluate the automatic segmentation method two experienced observers independently corrected the automatic segmentation result. This was done using a dedicated editing tool in which the automatically obtained surface model could interactively be deformed.

To compare the different segmentation results to obtained 3D surface models where resliced along the centerlines to obtain planar 2D contours. From these contours the cross sectional area and the minimal diameter were calculated as clinical parameters and compared between the different segmentation results. Also the Dice similarity index (or coefficient) was calculated between the contours from the different segmentation results. To investigate the influence of image quality, also the mean and standard deviation of the HU values in the descending aorta were measured for each subject.

Statistical analysis

The results of the clinical parameters from the automatic segmentations were compared with the results from the semi-automatic segmentations of the observers by the paired t-test. The Bland-Altman plots were calculated to quantify the mean error and the standard deviation (SD). The correlations were estimated by Pearson's correlation coefficient.

The statistical analyses were conducted with SPSS (version 20.0, SPSS Inc, Chicago, IL, USA) and MedCalc (version 15.6, Ostend, Belgium). **3.3 Results**

Data acquisition protocols

This is a retrospective study; the datasets were acquired before this research project started as part of routine clinical care protocols. Only anonymous routine clinical datasets were used.

A total of 38 patients underwent pre-operative CTA scanning for TAVR. The baseline characteristics of these patients are listed in Table 3.1. Two patients were excluded for the following reasons: one patient did not have a whole-body CTA dataset, whereas in the other patient the contrast in the aorto-femoral vessel trajectory was very low.

The datasets were acquired in two hospitals: Leiden University Medical Center (LUMC) in Leiden, the Netherlands, and Fuwai Hospital in Beijing, China. The CTA datasets from LUMC were collected on a 320-row CT scanner (Aquilion ONE, Toshiba Medical System, Japan) by using a helical scan protocol. A bi-phasic injection protocol with intravenous contrast was used: 70ml contrast (5ml/sec) and 50ml saline (5ml/sec) (de Graaf, Schuijf, van Velzen, Boogers, et al. 2010). The datasets from Fuwai Hospital were acquired on a dual source CT scanner (SOMATOM Definition FLASH, Siemens, Germany) by using a helical scan protocol. A single-phasic injection protocol was used: 350mgI/ml (3-4ml/s).The axial image size of the whole-body CTA image was 512×512. In each patient, there were approximately 1000 image slices in the z axis.

<u>Centerline evaluation</u>

As was described in (Gao et al. 2014), in all the 36 patients (100%) the centerlines were extracted successfully from the common femoral arteries to the sino-tubular junction, inside the lumen of the vessel. The average root mean square error between the automatic and manual corrected centerlines was 2.55 ± 0.70 mm and the average mean error was 1.63 ± 0.40 mm.

Contour evaluation

	Total (38)
Age (years)	77±13
Gender (% male)	21 (55)
Diabetes	7 (18)
Hypertension ^a	23 (61)
Hypercholesterolemia ^b	21 (55)
Family history of CAD ^c	8 (21)
Smoking	10 (26)
Obesity	4 (11)
Previous PCI	12 (32)
Previous CABG	10 (26)
Previous MI	6 (16)

Data are represented as mean \pm SD, median (interquartile range) or as number and percentages of patients

CABG coronary artery bypass graft, *CAD* coronary artery disease, *MI* myocardial infarction, *PCI* percutaneous coronary intervention

^a Defined as systolic blood pressure ≥140 mmHg and/or diastolic blood pressure ≥90 mmHg or the use of antihypertensive medication

 b Defined as serum total cholesterol $\geq\!\!230\,$ mg/dl or serum triglycerides $\geq\!\!200\,$ mg/dl or treatment with lipid lowering medication

^c Defined as the presence of coronary artery disease in first-degree family members at age <55 years in men and age <65 years in women

Table 3.1 Baseline characteristics

Table 3.2 shows the Dice similarity results comparisons between the automatic and the observer corrected segmentations for the different parts of the segmented trajectory.

The average Dice similarity indexes between the automatic method and the first observer were 0.977 ± 0.030 , 0.980 ± 0.019 , 0.982 ± 0.016 for the left ilio-femoral artery, the right ilio-femoral artery and the aorta, respectively; the average Dice similarity indexes between the automatic method and the second observer were 0.950 ± 0.040 , 0.954 ± 0.031 and 0.965 ± 0.019 , for the left ilio-femoral artery, the right ilio-femoral artery and the aorta, respectively. The inter-observer variability resulted in a Dice similarity index of 0.954 ± 0.038 , 0.952 ± 0.031 and 0.969 ± 0.018 for the left ilio-femoral artery (Table 3.2).

Dice similarity index (mean±SD)	Automatic vs observer 1	Automatic vs observer 2	Observer 1 vs observer 2
Left ilio-femoral artery	0.977 ± 0.030	0.950 ± 0.040	0.954±0.038
Right ilio-femoral artery	0.980 ± 0.019	0.954 ± 0.031	0.952 ± 0.031
Aorta	0.982 ± 0.016	$0.965 \!\pm\! 0.019$	0.969 ± 0.018

Table 3.2 Performance of automatic segmentation comparing to each of the observers and the observers to each other.

To find if there is any correlation between the contour detection and the quality of the datasets, the mean and standard deviation of the HU value within the descending aorta of each patient were measured and plotted together with the Dice similarity index of the aorta between the automatic system and observer 1 (Fig 3.6).

Clinical evaluation

The most important clinical parameter for the vascular access route is the minimal luminal diameter (MLD). In this study we separated the vascular access route into 3 segments: the two ilio-femoral arteries and the aorta. The cross-sectional diameter was calculated at every point along each centerline segment to build a diameter curve.



Fig 3.6. The image qualities and the contour detection evaluation of the datasets: the blue line is the mean of HU value of the descending aorta, the red is the standard deviation (left vertical axis) and the green is the Dice index (right vertical axis).

For the ilio-femoral access, the diameter and area measurements were taken along the centerline bilaterally with the minimum luminal measurement in both left and right side, including common iliac artery(CIA), external iliac artery(EIA), and common femoral artery(CFA) (Krishnaswamy et al. 2014; Kurra et al. 2009; Leipsic et al. 2011; Okuyama et al. 2014). For the aorta, the diameter measurements were taken along the centerline from the abdominal aorta until the sino-tubular junction,

including abdominal aorta, descending aorta and ascending aorta (Achenbach et al. 2012).

The mean value, standard deviation and 95% confidence interval of the parameters are shown in Table 3.3. The correlation and Bland-Altman bias are shown in Table 4. The correlations between automatic group and observer groups were 0.81- 0.94, with p-values smaller than 0.001. With the commonly used significance level value 0.05, the correlations can be called statistically significant.

	Automatic measurement			Observer 1 measurement			Observer 2 measurement		
	Mean	SD	95% CI	Mean	SD	95% CI	Mean	SD	95% CI
Ilio-femoral									
Minimal luminal diameter (mm)	6.03	1.48	5.53-6.53	5.70	1.43	5.22-6.19	5.52	1.32	5.07-5.97
Minimal luminal area (mm ²)	38.43	12.95	34.04-42.81	35.90	12.28	31.74-40.05	32.24	11.14	28.47-36.01
Aorta									
Minimal luminal diameter (mm)	13.43	2.54	12.57-14.29	12.40	2.93	11.41-13.39	12.08	2.40	11.27-12.89

Table 3.3. Results of minimal luminal diameter and area measurements from automatic, the observer 1 and the observer 2 measurement.

	Observer 1 vs	Observer 2 vs	Observer 1 vs		
	automatic	automatic	observer 2		
Ilio-femoral					
Diameter					
Correlation	0.94	0.88	0.87		
Bias (95% CI)	-0.32 (0.64 to -1.28)	-0.51 (0.89 to -1.90)	0.18 (1.57 to -1.20)		
p value	< 0.001	< 0.001	< 0.001		
Area					
Correlation	0.92	0.81	0.83		
Bias (95% CI)	-2.5 (7.7 to -12.8)	-6.2 (8.7 to -21.1)	3.7 (17.2 to -9.9)		
p value	< 0.001	< 0.001	< 0.001		
Aorta					
Diameter					
Correlation	0.88	0.92	0.90		
Bias (95% CI)	-1.0 (1.7 to -3.8)	-1.3 (0.6 to -3.3)	0.3 (2.8 to -2.2)		
p value	< 0.001	< 0.001	< 0.001		

Table 3.4. Results of minimal luminal diameter and area measurements: comparing the automatic to observer 1 and observer 2, and the observers to each other.

The Bland-Altman plots of the minimal ilio-femoral luminal lumen diameter and area are shown in Fig 3.7. The mean and SD of the difference between the minimal luminal diameters (MLD) of the automatic segmentation and the observer1 segmentation were 0.32mm and 0.49mm, respectively, and for the minimal luminal area (MLA) 2.53mm² and 5.23mm². The mean and SD of the difference between the MLD of automatic segmentation and the observer2 segmentation were 0.51mm and 0.71mm,

respectively, and for the MLA 6.19mm2 and 7.58mm². The mean and SD of the difference between the MLD of the observer1 segmentation and the observer2 segmentation were 0.18mm and 0.71mm, respectively, and for the MLA 3.66mm² and 6.89mm².

The Bland-Altman plots of the aorta minimal luminal diameter are shown in Fig 3.8. The mean and stand deviation of the difference between the MLD of the automatic segmentation and the observer1 segmentation were 1.03mm and 1.41mm. The mean and stand deviation of the difference between the MLD of the automatic segmentation and the observer2 segmentation were 1.35mm and 1.00mm. The mean and stand deviation of the difference between the MLD of the observer1 and the observer2 segmentation were 0.32mm and 1.28mm.

3.4 Discussion

Over the past few years, the development of TAVR pre-operative planning applications has been driven by the increasing need for proper access route selections and prosthesis size selection during TAVR, and prediction of post-TAVR vascular complications. Computed tomography has received a lot of interest because of its 3D imaging specifications as compared to 2D angiography's limited information (Okuyama et al. 2014). With multiplanar reformatting (MPR) images, the arterial lumen can be measured accurately in each cross-section, appreciating the elliptical nature of the artery (Delgado et al. 2010; Goenka et al. 2014; Krishnaswamy et al. 2014). However, such a manual detection procedure will require too much time and will introduce variabilities. An automatic procedure will be able to reduce the effort and support both inexperienced and experienced observers.

In this paper, a 3D method was introduced for the automatic segmentation of the vessel trajectory for TAVR pre-operative planning in whole-body CTA images. To our knowledge, this is the first solution which can automatically segment the whole vessel trajectory from femoral artery, iliac artery, abdominal aorta, descending aorta up to the ascending aorta in a whole-body CTA image data set published in articles.

The whole procedure only requires about 90 seconds on a computer with Core i7 3770 and 8GB RAM with 4 CPU threads, and can be further optimized. In our procedure, the quantification of the entire aorta-femoral trajectory is implemented, including the ilio-femoral arteries, the thoracic and abdominal aorta. In previous studies on aortic aneurysms, aortic measurement have also been implemented. In the work by Müller-Eschner et al it took 2.5-5.7 minutes with purely manually measurement on axial slices, and 4.6- 9.3 minutes on MPR images on the thoracic aorta; with a semi-automatic centerline extraction method, the analysis time was 3.5-9.3 minutes (Müller-Eschner et al. 2013). In the study by Kaufmann et al, the mean time to only detect the maximal diameter of the abdominal aorta aneurysm manually was 104.7 ± 24.9 s with double-oblique images and 175.2 ± 100.9 s to segment semi-automatically the abdominal aorta aneurysm to achieve maximal diameter (Kauffmann et al. 2011).

In our fully automatic segmentation procedure, a deformable subdivision surface model fitting was used. The deformable subdivision surface model is a new 3D model which processes the entire 3D data set instead of detecting the 2D transversal contour separately in each 2D image slice or detecting the 2D longitudinal contour on stretched MPR image. The control points on the subdivision surface are always searching in 3D space for the target boundary of artery. Another method which is similar to our method is the 3D deformable cylindrical Non-Uniform Rational B-Spline (NURBS) model fitting (van't Klooster et al. 2012). However, the advantages of deformable subdivision surface model fitting are that it is able to deal with objects with complex topology such as artery bifurcations and it is flexible to deal with complex shapes in the ilio-femoral luminal areas. However, when the model is too flexible, there might be selfintersection of surface. In this study, therefore, a non-self-intersection force was added to overcome this problem. In the future, we believe that the deformable subdivision surface model can also be used to segment other complex anatomical structures, such as the aortic root.

The ability to detect the minimal luminal diameter and area of the iliofemoral arteries in each patient is another important feature of this application. For the pre-operative planning of TF-TAVR, the minimal iliofemoral artery diameter decides the external sheath size. Post-operatively, vascular access site issues in TF-TAVR procedure are the most common companion disease (Toggweiler et al. 2013). It is the main complication in more than 15% of the patients undergoing TF-TAVR in (Krishnaswamy et al. 2014). Sheath-to-ilio-femoral artery ratio (SIFAR), defined as "sheath outer diameter divided by access-side vascular diameter" is known to be predictive of major vascular complications which have high correlation with higher mortality. Whether the TF-TAVR is acceptable will depend on the value of SIFAR (Okuyama et al. 2014). In (Krishnaswamy et al. 2014), the sheath to artery ratio was calculated by diameter and area, and the area's result seems more reliable. In this study, both diameter and area of the iliofemoral arteries were calculated, making the patient selection procedure in TAVR pre-operative planning reliable.

Quantitative evaluations were performed in two stages. The first stage was a comparison of the automatic contours with the manually corrected contours. The dice similarity index in our study was found to be at least 0.95.

In Fig 6, the measurement of the Hounsfield units of the contrast in the descending aorta was shown. This provides the indication on the quality of the datasets, which are the amount and the standard deviation of contrast in the aorta. It is apparent that if there is less contrast in the aorta and the contrast is inhomogeneous, the extraction of the aorta will be more difficult. But however, in our procedure, the automatic segmentation results of different datasets were always good according to dice similarity index. This proves the robustness of our method.

The second stage was the comparison of clinical parameters from automatic and manually-corrected segmentation. The correlation between the automatic method and the first observer was much higher than the **36**

inter-observer variability, and the correlation between the automatic method and the second observer was similar to the inter-observer variability. The result indicates that the automatic method is trustful compared to the manual corrected method. The automatic method overestimated the lumen area and diameter in the ilio-femoral arteries comparing to the results from both observers slightly by around 1 pixel. The variabilities between the observers of clinical parameters are much higher than the variabilities between automatic measurement and observer 1; the variabilities between automatic measurement and observer 2. This means that our technique is more reproducible than between the observers.

In research, CTA-based semi-automatic segmentation software was used to measure minimal luminal diameter for TF-TAVR. The result was evaluated by manual results on projection angiography (XA). The difference in minimal luminal diameter between the software and the ground truth was higher than 1.2 mm in the ilio-femoral artery segments. In our study, the automatic measurement overestimated the MLA only by 0.323 mm compared to observer1, and by 0.51mm compared to observer2, similar to the size of one pixel in the images we used.

In three cases the automatic procedure showed segmentation issue, this can be explained as follows. During the subdivision surface model fitting step, the strongest edge in the intensity image was searched for within certain distance range. This search range was the same for both tiny vessel (such as femoral artery) and larger vessel such as the aorta. Making the search ranges variable for the different vessel sizes should improve the framework and prevent these issues in the future.

3.5 Conclusions

In conclusion, this automatic TAVR pre-operative application has demonstrated to be able to accurately segment the whole vascular access and measure minimal lumen of the vascular access for TAVR planning in CTA data set.



Fig 3.7. Bland-Altman plot of minimal ilio-femoral luminal lumen comparing automatic measurement, the observer1 and the observer2



Fig 3.8 Bland-Altman plots comparing minimal aorta luminal diameter measurements between automatic, observer 1 and observer 2.

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-2

-3

observer1 - observer2(mm)

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Mean of obse

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C

observer1 - automatic(mm)