

BULLETIN OF THE ASTRONOMICAL INSTITUTES OF THE NETHERLANDS.

1935 October 4

Volume VII.

No. 273.

COMMUNICATIONS FROM THE OBSERVATORY AT LEIDEN.

Estimates of 11 variable stars on Franklin-Adams-plates with the centre η Carinae, by *L. Plant.*

Among the various areas on Franklin-Adams-plates taken at Johannesburg for the investigation of variable stars, the series of plates with the centre η Carinae is by far the most numerous, containing at present 939 plates and 17 copies on glass from older plates present at Johannesburg. Table 1 shows the distribution of the plates over the different oppositions. The plates cover an area of $10^\circ \times 10^\circ$; they are normally exposed for 30 minutes. The plates were taken by Prof. HERTZSPRUNG and Dr. VAN GENT.

The estimates are made in the ordinary way using ARGELANDER's method. Most of the 11 stars treated in this paper had already been estimated by HERTZSPRUNG on a smaller number of plates. All these older plates have been reestimated. The condensed results of the estimates are given in Table 2, the columns being self-explanatory. The total number of new estimates used in the present paper is 9776.

As the right-ascension of VX Vel on the Leiden card catalogue differed by 3^s from that given in PRAGER's Katalog und Ephemeriden (K.V.B.B. 14) the position was redetermined.

The first 8 stars are of the δ Cep-type, the last 3 of the RR Lyr-type. The periods have been determined by least square solutions; for 4 stars the maximum and for 6 stars a certain point on the ascending branch has been used for the solutions; in the case of UY Car the period has been taken from an unpublished investigation by the late Mr. W. E. KRUYTBOSCH. Table 4 contains the epochs used and the (O-C)'s from the least square solutions.

The greatest difficulty in the reduction of these estimates is to get a good scale for the magnitudes of the comparison stars. For this purpose the following 4 different methods have been applied:

1. By the aid of counts of all stars brighter than each comparison star, using the tables of Groningen Publication 43. In 7 cases such star counts have been made in the neighbourhood of the comparison

stars over an area of one or half a square degree. These magnitudes are assumed to be on the International Scale.

2. On plate 5240 with the centre 11^h-59^m stars in the Selected Area 193 (H.A. 193) and the comparison stars of 7 variables could be measured with the Schilt-microphotometer. An inaccuracy is caused by the dependance of the star image on its distance from the platecentre. A least square solution of the Selected Area magnitudes with the provisional magnitudes of the Schilt-photometer measurements derived with the tables described in B.A.N. 190, gives a mean error of ± 0.23 for one determination of magnitude.

3. For the comparison stars of 7 variables C.P.D. magnitudes reduced by the aid of H.A. 80, 231 were available.

4. For 8 variables the comparison stars could be measured with the Schilt-microphotometer on some of the 23 plates taken with a coarse grating in front of the objective. This method gives an absolute scale but no zero-point. The mean error of one determination of magnitude is ± 0.06 .

It was the intention to obtain a uniform scale and zero-point for the comparison stars of all 11 variables. For the reduction the following solutions have been used:

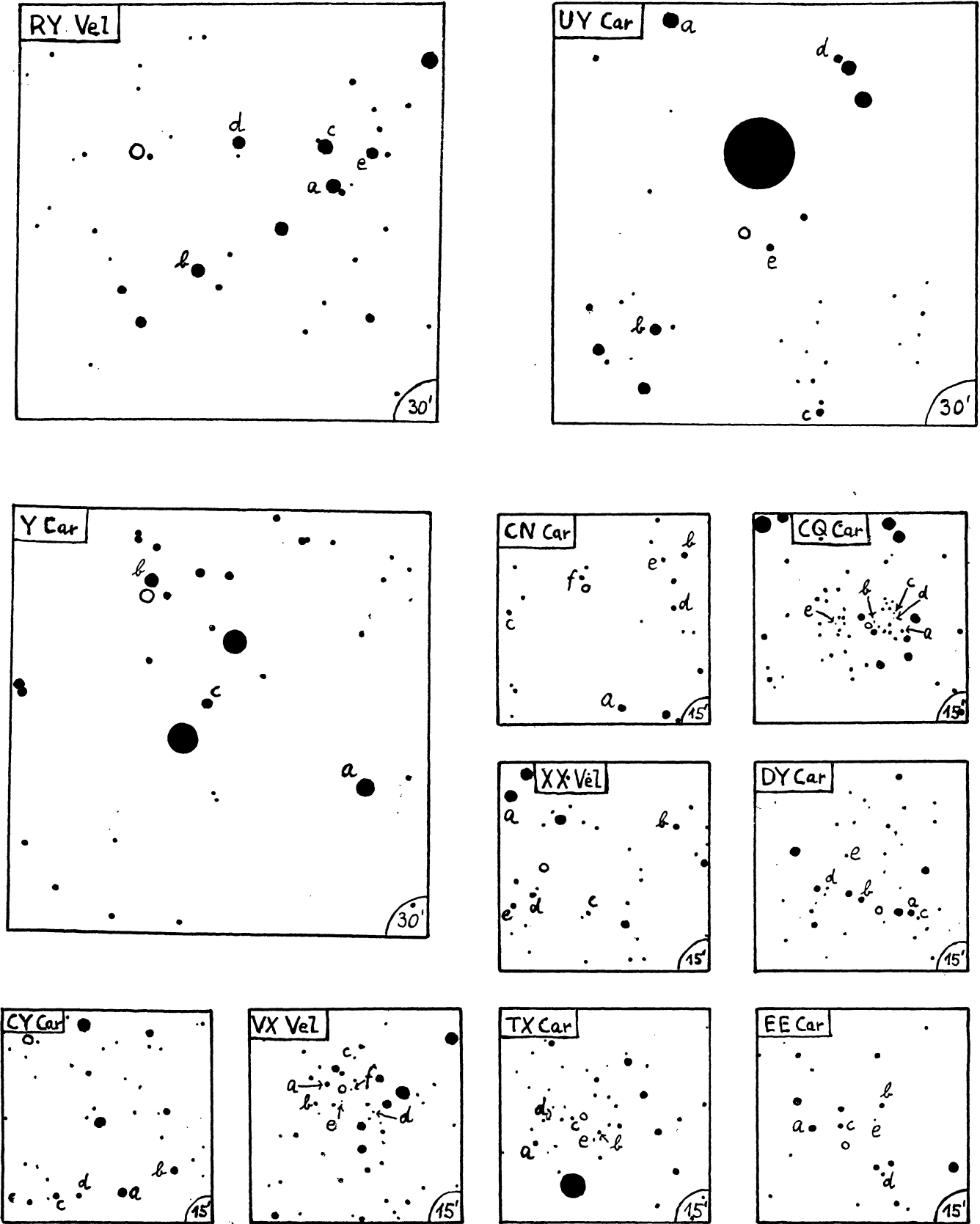
$$\begin{aligned} m_1 &= + 2.55 + 0.830 m_2 && (24 \text{ stars}) \\ &\pm 0.18 \pm 0.030 && (m. e.) \\ m_2 &= - 2.44 + 1.236 m_3 && (12 \text{ stars}) \\ &\pm 0.27 \pm 0.130 && (m. e.) \end{aligned}$$

$$\begin{aligned} \text{hence} \\ m_1 &= + 0.52 + 1.026 m_3 && \\ &\pm 0.29 \pm 0.114 && (m. e.) \end{aligned}$$

$$\begin{aligned} m_1 &= m \text{ (starcounts)} \\ m_2 &= m \text{ (Selected Area)} \\ m_3 &= m \text{ (CPD, reduced)} \end{aligned}$$

The methods used in the case of each set of comparison stars are indicated in Table 3, where the

FIGURE 1.



linear formulae finally adopted for the relation between magnitudes and steps are given in the last column. Table 5 gives the brightness in magnitudes and steps for each comparison star.

The phases were computed by the formula

$$\text{phase} = \text{reciprocal period} \times (\text{J. D. hel. M. Astr. T. Gr.} - 2420000)$$

Normal points of the lightcurve are given in Table 6 in the usual way and represented graphically in Figures 2—12. A record of the individual estimates is kept at the Leiden Observatory.

Figure 1 gives the diagrams of the surrounding, North being at the top and the size scale being given in the lower right hand corner.

FIGURE 2.

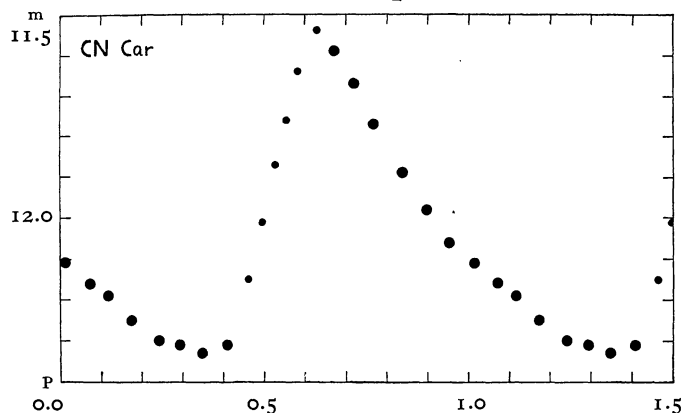


FIGURE 3.

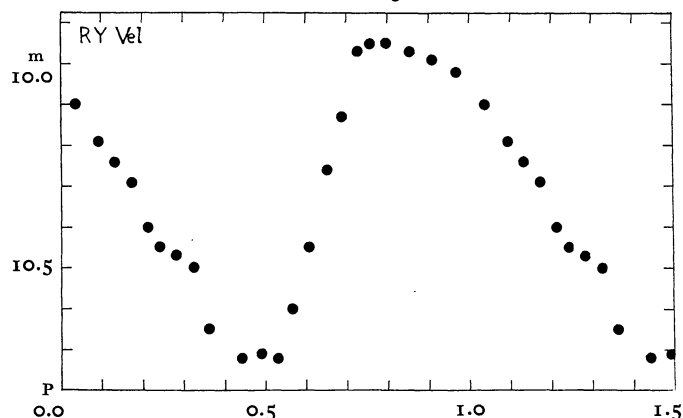


FIGURE 4.

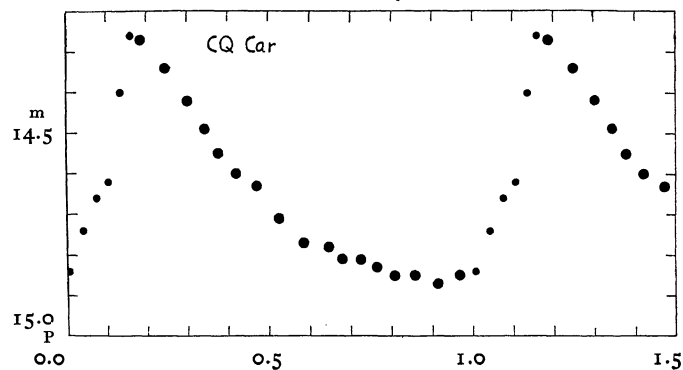


FIGURE 5.

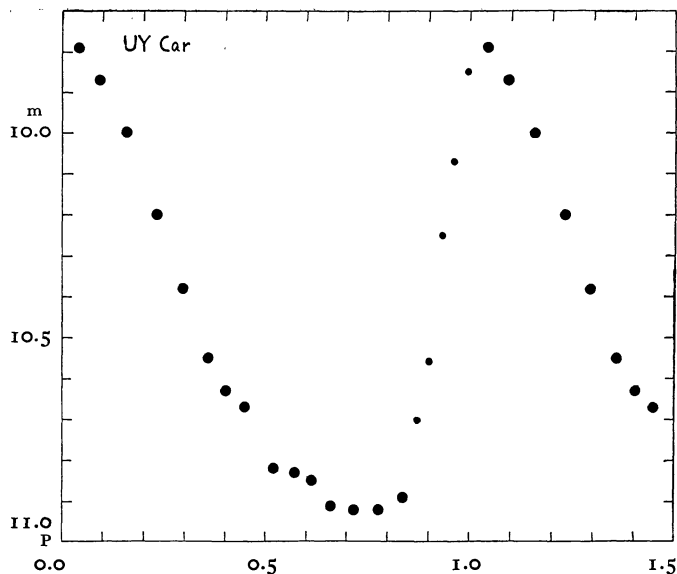


FIGURE 6.

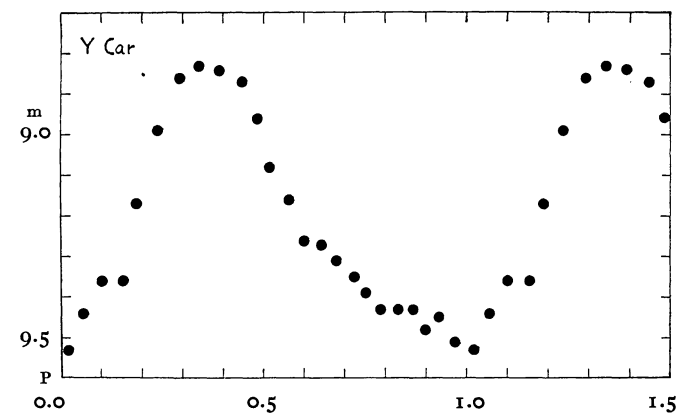


FIGURE 7.

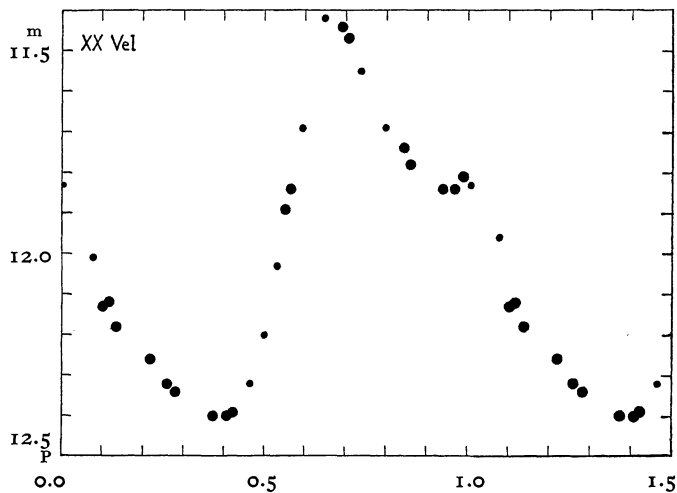


FIGURE 8.

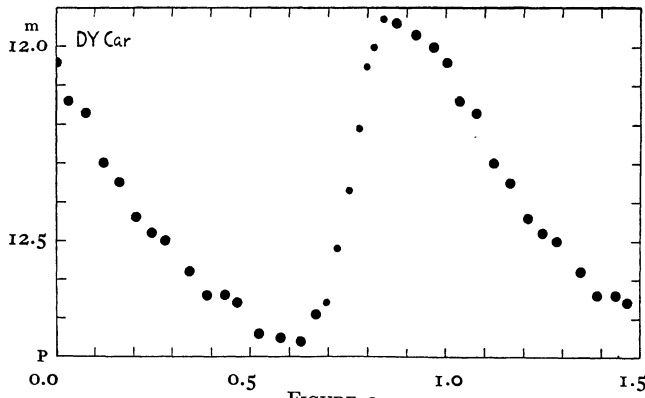


FIGURE 9.

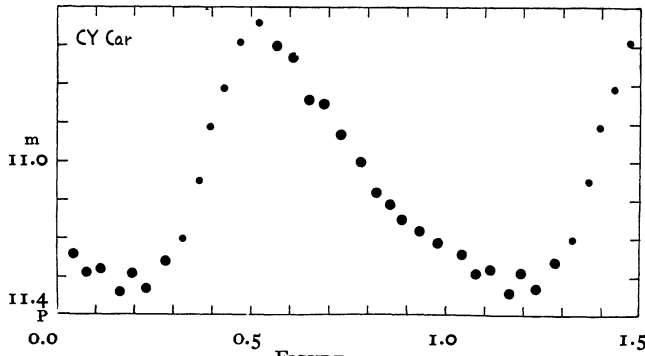


FIGURE 10.

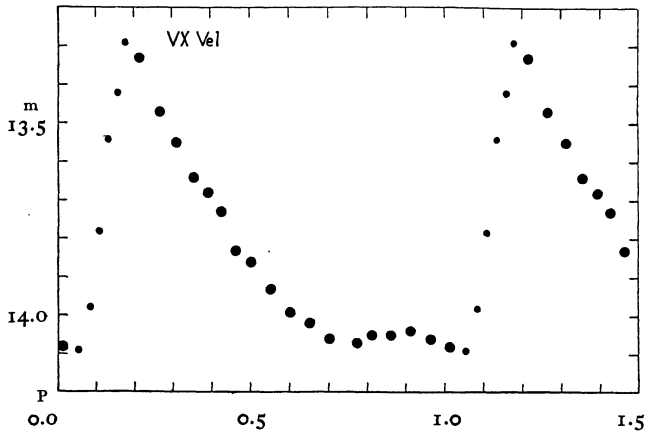


FIGURE 11.

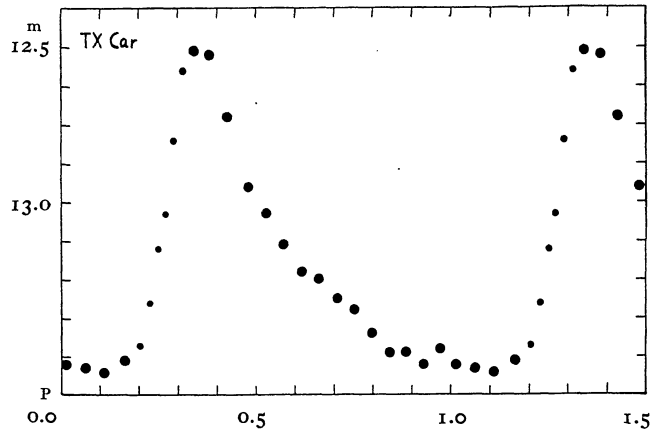


FIGURE 12.

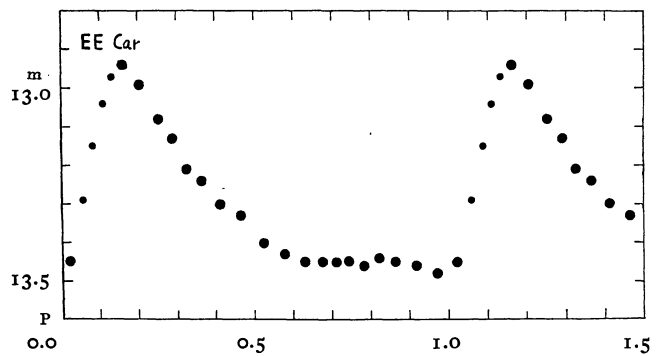


TABLE I.

Copies on glass 1913—1927	17 plates
1923—1924	409 "
1924—1925	198 "
1925—1926	33 "
1926—1927	24 "
1927—1928	61 "
1928—1929	100 "
1929—1930	49 "
1930—1931	22 "
1931—1932	11 "
1932—1933	— "
1933—1934	13 "
1934—1935	2 "

total 939 plates
including 23 " with a coarse-grating in front of the objective.

TABLE 2.

*	α (1875)	δ (1875)	number of plates	period	m.e.	reciprocal period	epoch 2420000+	m.e. of a single epoch	number of epochs	phase of epoch	max.	range	m.e. of a single estimate
1	CN Car	10 11 9	906	4 ^d .93285	± .00017	^d -.2027224	4585 ^d .84	± .26	38	^P .652	11 ^m .54	0 ^m .79	± 1 st .68 = ± .096
2	RY Vel	10 15 59	889	28 ^d .1311	± .0032	^d -.0355478	5024 ^d .60	± .78	46	^P .613	9 ^m .95	0 ^m .77	± 1 st .79 = ± .103
3	CQ Car	10 26 47	802	5 ^d .318934	± .000082	^d -.1880076	4298 ^d .405	± .076	47	^P .133	14 ^m .26	0 ^m .61	± 1 st .57 = ± .088
4	UY Car	10 27 38	905	5 ^d .543698	—	^d -.180385	—	—	—	—	9 ^m .79	1 ^m .13	± 1 st .37 = ± .132
5	Y Car	10 28 29	912	3 ^d .639061	± .000075	^d -.2747962	4626 ^d .53	± .34	42	^P .353	8 ^m .83	0 ^m .70	± 1 st .63 = ± .173
6	XX Vel	10 31 15	896	6 ^d .98464	± .00020	^d -.1431713	4915 ^d .03	± .26	46	^P .691	11 ^m .42	0 ^m .98	± 1 st .16 = ± .076
7	DY Car	10 47 38	907	4 ^d .674543	± .000055	^d -.2139247	4290 ^d .134	± .088	78	^P .766	11 ^m .93	0 ^m .83	± 1 st .38 = ± .106
8	CY Car	10 52 50	917	4 ^d .265827	± .000079	^d -.2344211	4297 ^d .407	± .138	84	^P .403	10 ^m .64	0 ^m .70	± 1 st .26 = ± .093
9	VX Vel	10 53 47	852	0 ^d .50940266	± .00000055	^d -.19630836	4190 ^d .4104	± .0093	92	^P .126	13 ^m .29	0 ^m .80	± 1 st .79 = ± .099
10	TX Car	10 53 50	911	0 ^d .6011360	± .0000015	^d -.16635171	4566 ^d .442	± .021	51	^P .354	12 ^m .51	0 ^m .83	± 1 st .70 = ± .085
11	EE Car	10 54 54	879	0 ^d .6787054	± .0000011	^d -.14733933	4553 ^d .4888	± .0121	75	^P .080	12 ^m .94	0 ^m .54	± 1 st .06 = ± .058

TABLE 3.

1	CN Car	star counts, 1 sq. degree	—	CPD 2	coarse grating plates	$m = 11^{\circ}52' + 0^{\circ}0574 \text{ st}$
2	RY Vel	—	—	CPD 12	coarse grating plates	$m = 10^{\circ}08' + 0^{\circ}0575 \text{ st}$
3	CQ Car	star counts, $\frac{1}{2}$ sq. degree	—	—	—	$m = 13^{\circ}93' + 0^{\circ}0559 \text{ st}$
4	UY Car	—	Selected Area	CPD 17	coarse grating plates	$m = 9^{\circ}56' + 0^{\circ}0903 \text{ st}$
5	Y Car	—	—	CPD 22	coarse grating plates	$m = 8^{\circ}74' + 0^{\circ}1061 \text{ st}$
6	XX Vel	star counts, 1 sq. degree	Selected Area	CPD 11	coarse grating plates	$m = 11^{\circ}18' + 0^{\circ}0654 \text{ st}$
7	DY Car	star counts, 1 sq. degree	Selected Area	—	8 coarse grating plates	$m = 11^{\circ}66' + 0^{\circ}0765 \text{ st}$
8	CY Car	star counts, 1 sq. degree	Selected Area	CPD 16	coarse grating plates	$m = 10^{\circ}54' + 0^{\circ}0739 \text{ st}$
9	VX Vel	star counts, $\frac{1}{2}$ sq. degree	Selected Area	—	—	$m = 13^{\circ}15' + 0^{\circ}0551 \text{ st}$
10	TX Car	star counts, 1 sq. degree	Selected Area	—	—	$m = 12^{\circ}52' + 0^{\circ}0498 \text{ st}$
11	EE Car	—	Selected Area	—	—	$m = 12^{\circ}81' + 0^{\circ}0545 \text{ st}$

TABLE 4.

I. CN Car			J.D. 242....	Epoch	O—C	J.D. 242....	Epoch	O—C	J.D. 24....	Epoch	O—C
Maxima. Means of the plates of one night, $v \downarrow 1^{\text{st}}0$.			3787'57	0	+ '74	3814'303	0	— 0'79	12869'2	0	+ '47
J.D. 242....	Epoch	O—C	3814'18	1	— '78	'324	0	— 58	5041'40	597	+ 12
			'19	1	— '77	'351	0	— 31	21722'27	2433	— 29
			'24	1	— '72	'360	0	— 22	3789'53	3001	— 2
			15'26	1	+ '30	'466	0	+ 84	3815'43	3008	+ 41
0605'26	0	+ '24	41'66	2	— 1'43	78'123	12	— 86	18'56	3009	— 10
3786'54	645	— '18	42'39	2	— '70	'168	12	— 41	77'16	3025	+ 28
91'53	646	— '12	'50	2	— '59	'188	12	— 21	80'27	3026	+ 25
3816'43	651	— '08	43'00	2	— '09	'193	12	— 16	87'41	3028	— 39
80'35	664	— '08	70'31	3	— '91	'218	12	+ 9	3902'37	3032	+ 2
85'35	665	— '02	'39	3	— '83	83'517	13	— 11	13'29	3035	+ 2
3900'29	668	+ '12	99'17	4	— '18	'591	13	+ 63	31'29	3040	— 18
10'29	670	+ '26	'71	4	+ '36	99'389	16	— 96	46'25	3044	+ 23
39'29	676	— '34	3900'53	4	+ 1'18	3910'134	18	+ 11	49'20	3045	+ 46
44'26	677	— '31	26'54	5	— '94	'197	18	+ 78	64'23	3049	+ 1
49'20	678	— '30	27'81	5	+ '33	15'322	19	— 120	67'23	3050	— 63
59'21	680	— '15	'84	5	+ '36	'482	19	+ 40	75'23	3052	+ 9
64'23	681	— '06	28'43	5	+ '95	'483	19	+ 41	78'71	3053	— 7
69'22	682	— '00	56'54	6	+ '92	'509	19	+ 67	89'20	3056	— 50
74'23	683	+ '07	84'99	7	+ 1'24	26'098	21	+ 19	4171'45	3106	— 20
79'21	684	+ '12	4210'10	15	+ 1'30	31'294	22	— 104	4200'43	3114	— 33
89'20	686	+ '24	36'54	16	— '39	'386	22	— 12	04'42	3115	+ 2
4171'45	723	— '02	65'29	17	+ '23	'406	22	+ 8	40'42	3125	— 37
76'47	724	+ '07	'58	17	+ '52	'407	22	+ 9	66'24	3132	— 2
96'53	728	+ '39	'61	17	+ '55	47'364	25	+ 9	77'28	3135	+ 10
4201'38	729	+ '31	92'50	18	— '69	63'394	28	+ 82	84'24	3138	— 21
05'97	730	— '43	93'09	18	— '10	'419	28	+ 107	4550'38	3210	+ 27
40'42	737	— '12	'67	18	+ '48	'550	28	+ 238	53'45	3211	— 30
45'35	738	— '12	5024'33	44	— '27	4245'148	81	— 67	86'47	3220	— 3
94'36	748	— '14	5389'86	57	— '44	61'205	84	+ 33	4626'24	3231	— 29
4586'46	807	+ '62	5446'85	59	+ '29	'294	84	+ 122	5067'26	3352	+ 41
5330'24	958	— '46	47'11	59	+ '55	93'128	90	+ 42	5561'56	3488	— 21
80'25	968	+ '23	5617'31	65	+ 1'96	98'293	91	— 112	5641'48	3510	— 34
5641'50	1021	+ '04	43'15	66	— '33	4915'346	207	— 55	5740'20	3537	+ 12
51'55	1023	+ '22	5926'61	76	+ 1'82	'363	207	— 38	66'20	3544	+ 65
5740'20	1041	+ '08	6008'76	79	— '42	5330'279	285	+ 1	73'28	3546	+ 45
74'23	1048	— '42	'77	79	— '43	83'418	295	— 49	76'30	3547	— 17
89'20	1051	— '25	37'09	80	— '23	'440	295	— 27	91'22	3551	+ 19
5922'57	1078	— '07	6120'69	83	— 1'02	5447'240	307	— 55	6122'22	3642	+ 3
6036'36	1101	+ '27	21'00	83	— '71	'263	307	— 32	55'21	3651	+ 28
6120'28	1118	+ '33	21'51	83	— '20	5745'139	363	— 16	6828'30	3836	+ 15
7427'55	1383	+ '40	6824'45	108	— '54	'251	363	+ 96	7604'31	4049	+ 102
7619'20	1422	— '34	81'21	110	— '04	60'981	366	— 131			
			'26	110	+ '01	61'122	366	+ 10			
						77'133	369	+ 64			
						'200	369	+ 131			
2. RY Vel			3. CQ Car			5. Y Car			6. XX Vel		
Reduced to 6 st on the ascending branch using the gradient d/st 4125.			Reduced to 9 st on the ascending branch using the gradient d/st 0447.			Maxima. The first two maxima are from ROBERTS (A.J. 313 and 491), the other means of the plates of one night, $v \downarrow 0^{\text{st}}$.			Maxima. Means of the plates of one night, $v \downarrow 5^{\text{st}}7$.		
J.D. 242....	Epoch	O—C	J.D. 242....	Epoch	O—C	J.D. 242....	Epoch	O—C	J.D. 242....	Epoch	O—C
3786'21	0	— '62	3814'299	0	— '083	0605'26	0	— '25			
'77	0	— '06				1010'27	58	— 35			
						3790'53	456	+ 3			
						3818'56	460	+ 12			

TABLE 4 (continued).

J.D. 242....	Epoch	O—C	J.D. 242....	Epoch	O—C	J.D. 242....	Epoch	O—C	J.D. 242....	Epoch	O—C
3874'29	468	— ^d 04									
81'40	469	+ 9									
3902'38	472	+ 12									
16'35	474	+ 12									
30'26	476	+ 6									
37'28	477	+ 10									
44'25	478	+ 8									
58'23	480	+ 9									
65'22	481	+ 10									
72'22	482	+ 12									
79'22	483	+ 13									
4202'42	515	— 18									
58'26	523	— 21									
86'49	527	+ 8									
93'50	528	+ 10									
4537'41	563	— 46									
58'86	566	+ 5									
66'46	567	+ 66									
86'47	570	— 28									
4642'36	578	— 28									
49'78	579	+ 16									
4915'41	617	+ 38									
5068'25	639	— 45									
5320'32	675	+ 18									
27'31	676	+ 19									
83'41	684	+ 40									
5446'24	693	+ 37									
5564'56	710	— 4									
71'50	711	— 9									
5641'47	721	+ 4									
5732'23	734	— 1									
46'31	736	+ 11									
53'30	737	+ 11									
60'25	738	+ 7									
74'26	740	+ 12									
6123'31	790	— 7									
6269'60	811	— 45									
6423'37	833	— 35									
6828'30	891	— 52									
84'23	899	— 47									
7604'33	1002	+ 21									
18'20	1004	+ 11									
7. DY Car											
Reduced to 8 st on the ascending branch using the gradient ^d /s ^t 0580.											
J.D. 242....	Epoch	O—C									
1401'295	0	+ ^d 029									
3813'194	516	— 136									
223	516	— 107									
247	516	— 83									
272	516	— 58									
272	516	— 58									
323	516	— 7									
338	516	+ 8									
390	516	+ 60									
41'351	522	— 27									
456	522	+ 78									
477	522	+ 99									
74'101	529	+ 2									
78'703	530	— 71									
713	530	— 61									
83'313	531	— 135									
521	531	+ 73									
97'531	534	+ 59									
3911'345	537	— ^d 151									
514	537	+ 18									
546	537	+ 50									
597	537	+ 101									
16'306	538	+ 136									
30'044	541	— 150									
166	541	— 28									
301	541	— 107									
331	541	— 137									
39'558	543	+ 15									
587	543	+ 44									
613	543	+ 70									
44'153	544	— 64									
191	544	— 26									
213	544	— 4									
267	544	+ 50									
281	544	+ 64									
58'190	547	— 51									
239	547	— 2									
242	547	+ 1									
72'355	550	+ 90									
382	550	+ 117									
86'389	553	+ 101									
4168'493	592	+ 103									
617	592	+ 21									
719	592	+ 123									
756	592	+ 160									
73'138	593	— 132									
96'655	598	+ 12									
4201'188	599	— 129									
205	599	— 112									
281	599	— 36									
305	599	— 12									
345	599	+ 28									
57'283	611	— 129									
362	611	— 50									
62'006	612	— 80									
093	612	+ 7									
85'302	617	— 157									
365	617	— 94									
389	617	— 70									
465	617	+ 6									
90'134	618	0									
255	618	+ 121									
5038'090	778	+ 29									
114	778	+ 53									
5206'649	814	+ 305									
5360'533	847	+ 71									
632	847	+ 28									
79'310	851	+ 8									
363	851	+ 61									
5561'563	890	— 46									
564	890	— 45									
5753'417	931	+ 151									
6010'364	986	— 1									
386	986	+ 21									
6155'204	1017	— 72									
316	1017	+ 40									
6828'336	1161	— 75									
7604'339	1327	— 46									
8. CY Car											
Reduced to 5 st on the ascending branch using the gradient ^d /s ^t 0983.											
J.D. 242....	Epoch	O—C									
0991'236	0	— ^d 155									
3789'850	656	+ 76									
872	656	+ 98									
985	656	+ 211									
3815'197	662	— 172									
324	662	— 45									
493	662	+ 124									
45'093	669	— 105									
125	669	— 137									
79'066	677	— 291									
171	677	— 186									
224	677	— 133									
317	677	— 40									
375	677	+ 18									
439	677	+ 82									
463	677	+ 106									
488	677	+ 131									
591	677	+ 234									
83'522	678	— 100									
650	678	+ 28									
3913'125	685	— 358									
518	685	+ 35									
591	685	+ 108									
707	685	+ 224									
26'254	688	— 26									
30'584	689	+ 37									
39'198	691	+ 121									
263	691	+ 186									
43'242	692	— 102									
413	692	+ 69									
438	692	+ 94									
460	692	+ 116									
514	692	+ 170									
56'356	695	+ 215									
491	695	+ 350									
60'516	696	+ 109									
588	696	+ 181									
73'185	699	— 19									
77'508	700	+ 38									
90'402	703	+ 135									
4169'234	745	— 199									
246	745	— 187									
307	745	— 126									
354	745	— 79									
377	745	— 56									
441	745	+ 8									
457	745	+ 24									
470	745	+ 37									
480	745	+ 47									
497	745	+ 64									
4263'046	767	— 234									
082	767	— 198									
123	767	— 157									
164	767	— 116									
179	767	— 101									
80'401	771	+ 57									
92'895	774	— 247									
93'205	774	+ 63									
97'262	775	— 145									
295	775	— 112									
383	775	— 24									
484	775	+ 77									
4553'358	835	— 99									
420	835	+ 63									
494	835	+ 137									
5077'978	958	+ 24									
78'182	958	+ 128									
223	958	+ 169									
5385'075	1030	— 118									
5385'240	1030	+ ^d 047									
5564'390	1072	+ 32									
441	1072	+ 83									
5615'677	1084	+ 129									
40'999	1090	— 144									
5709'309	1106	— 87									
361	1106	— 35									
527	1106	+ 131									
73'127	1121	— 257									
268	1121	— 116									
407	1121	+ 23									
6123'084	1203	— 97									
283	1203	+ 102									
6413'141	1271	— 116									
433	1271	+ 176									
9. VX Vel											
Reduced to 9 st on the ascending branch using the gradient ^d /s ^t 00369.											
J.D. 242....	Epoch	O—C									
0605'2406	0	+ ^d 0061									
1287'3286	1339	+ 40									
3788'4849	6249	— 68									
4855	6249	— 62									
4903	6249	— 14									
89'4910	6251	— 195									
5026	6251	— 79									
5128	6251	+ 23									
90'5336	6253	+ 43									
91'5455	6255	— 26									
3813'4501	6298	— 24									
4590	6298	+ 65									
4597	6298	+ 72									
4617	6298	+ 92									
14'4689	6300	— 24									
4696	6300	— 17									
15'4973	6302	+ 72									
16'5097	6304	+ 8									
17'5436	6306	+ 159									
18'5515	6308	+ 50									
5521	6308	+ 56									
57'2040	6384	+ 29									
58'2921	6386	+ 122									
84'2438	6437	— 156									
85'2701	6439	— 81									
86'2899	6441	— 71									
3910'2294	6488	— 96									
2448	6488	+ 58									
11'2594	6490	+ 16									
13'3035	6494	+ 81									
3045	6494	+ 91									
15'3438	6498	+ 108									
3507	6498	+ 177									
16'3402	6500	— 116									
3644	6500	+ 126									
36'2144	6539	— 41									
37'2474	6541	+ 101									
38'2557	6543	— 4									
2709	6543	+ 148									
39'2680	6545	— 69									
2896	6545	+ 147									
40'2857	6547	— 80									
3023	6547	+ 86									
41'3234	6549	+ 109									
42'3201	6551	— 112									

TABLE 4 (continued).

J.D. 242....	Epoch	O—C	I. TX Car			J.D. 242....	Epoch	O—C	J.D. 242....	Epoch	O—C
			Means of the plates of one night, $v \leq 0.8$.						Means of the plates of one night, $v \leq 0.8$.		
3962'1901	6590	+0079	J.D. 242....	Epoch	O—C	6120'386	9637	+007	3958'2473	253	+0169
63'1962	6592	-206				25'197	9645	+9	73'1841	275	-116
'2122	6592	-46				26'375	9647	-15	75'2402	278	+84
64'2227	6594	+130				29'373	9652	-23	'2406	278	+88
'2466	6594	+109				55'216	9695	-29	4141'4981	523	+165
65'2591	6596	+46	0327'248	0	+017	6364'454	10043	+14	'5344	523	+198
66'2791	6598	+58	3525'259	5320	-16	6423'362	10141	+11	71'3834	567	+57
88'1723	6641	-53	3791'567	5763	-10	6883'233	10906	+13	73'4075	570	+63
89'1895	6643	-69	3814'426	5801	+2	7605'184	12107	0	77'4835	576	-25
4141'4962	6942	-116	17'418	5806	-8				'4844	576	-16
'5112	6942	+34	76'340	5904	+2				'5013	576	+153
68'4838	6995	-223	85'360	5919	+5				90'3916	595	+102
'5033	6995	-28	3903'386	5949	-4				98'5206	607	-53
'5043	6995	-18	11'264	5962	+60				'5298	607	+39
69'5109	6997	-140	26'214	5987	-18				'5347	607	+88
'5133	6997	-116	29'238	5992	0				4205'3088	617	-41
'5217	6997	-32	32'235	5997	-9				45'3520	676	-46
90'4016	7038	-88	35'277	6002	+27				58'2460	695	-60
'4268	7038	+164	38'254	6007	-1				62'3305	701	+63
4238'2855	7132	-88	41'282	6012	+21	3786'5218	0	-0299	64'3762	704	+159
'2874	7132	-69	44'253	6017	-13	'5434	0	-83	77'2721	723	+164
61'2171	7177	-3	62'268	6047	-33	3814'3798	41	+12	94'2110	748	-123
62'2180	7179	-182	4168'476	6390	-14	'3805	41	+19	96'2489	751	-106
'2273	7179	-89	71'457	6395	-39	58'4611	106	+334	'2541	751	-54
63'2457	7181	-93	77'524	6405	+17	'4993	106	+48	4553'4858	1130	-30
'2491	7181	-59	98'928	6440	-19	71'3864	125	-35	'4915	1130	+27
90'2602	7234	+68	4200'348	6443	-2	77'4812	134	-170	4642'3972	1261	-20
91'2727	7236	+5	04'568	6450	+10	'5015	134	+33	51'2309	1274	+85
'2816	7236	+94	06'357	6453	-5	80'2096	138	-34	5067'2598	1887	-90
92'2979	7238	+69	54'434	6533	-18	82'2357	141	-135	'2671	1887	-17
94'3316	7242	+30	63'430	6548	-40	84'2861	144	+8	'2679	1887	-9
4543'4207	7731	-58	77'279	6571	-17	86'3134	147	-80	'2772	1887	+84
'4304	7731	+39	86'331	6586	+19	'3304	147	+150	5329'2541	2273	+50
'4356	7731	+91	92'342	6596	+18	3901'2576	169	+47	5686'2529	2799	+47
5320'2715	9256	+60	4560'469	7042	+38	'2742	169	+213	5709'3165	2833	-77
77'3212	9368	+26	66'460	7052	+18	'2860	169	+331	'3483	2833	+241
'3281	9368	+95	5406'215	8449	-14	'2911	169	+382	45'2956	2886	+1
79'3546	9372	-17	5562'547	8709	+22	07'3619	178	+6	'2973	2886	+18
'3732	9372	+169	71'504	8724	-37	'3643	178	+30	60'2326	2908	+55
83'4410	9380	+95	5615'410	8797	-14	37'2181	222	-62	'2335	2908	+64
5731'3487	10063	-48	86'357	8915	-1	39'2555	225	-49	77'1918	2933	-29
'772052	10153	+55	5745'286	9013	+16	'2578	225	-26	6123'3269	3443	-76
6010'5083	10611	+21	60'278	9038	-21	41'2791	228	-174	'3314	3443	-31
30'3786	10650	+57	72'339	9058	+17	'2876	228	-89	55'2274	3490	-62
6155'1610	10895	-155	75'333	9063	+6	43'3373	231	+47	'2360	3490	+24
7618'1917	13767	+107	89'200	9086	+47	56'2152	250	-128	6423'3252	3885	+29
19'1906	13769	-92	6007'368	9449	+3	'2349	250	+69	7619'1872	5647	-140

TABLE 5.

CN Car			CQ Car			Y Car			DY Car		
*	st	m	*	st	m	*	st	m	*	st	m
a	0'0	11'52	a	0'0	13'93	a	0'0	8'74	a	0'0	11'66
b	3'5	11'73	b	5'2	14'22	b	6'4	9'42	b	5'4	12'07
c	7'4	11'95	c	10'2	14'50	c	11'8	9'99	c	10'1	12'43
d	10'3	12'12	d	12'5	14'63				d	14'6	12'77
e	14'4	12'35	e	16'9	14'88				e	18'5	13'07
f	18'0	12'56									
RY Vel			UY Car			XX Vel			CY Car		
*	st	m	*	st	m	*	st	m	*	st	m
a	0'0	10'08	a	0'0	9'56	a	0'0	11'18	a	0'0	10'54
b	4'6	10'34	b	5'0	10'05	b	5'6	11'55	b	4'6	10'88
c	9'0	10'60	c	9'5	10'48	c	11'4	11'93	c	9'6	11'25
d	11'0	10'71	d	12'1	10'73	d	15'8	12'21	d	13'6	11'54
e	14'6	10'93	e	17'2	11'22	e	19'4	12'45			

TABLE 5 (continued).

VX Vel			TX Car			EE Car		
*	st	m	*	st	m	*	st	m
a	0'0	13'15	a	0'0	12'52	a	0'0	12'81
b	4'7	13'41	b	4'3	12'73	b	2'8	12'96
c	9'7	13'68	c	8'5	12'94	c	4'3	13'04
d	15'1	13'98	d	14'4	13'23	d	7'8	13'23
e	17'5	14'11	e	18'9	13'46	e	13'2	13'53
f	21'4	14'33						

TABLE 6.

CN Car			CQ Car			Y Car			Phase	m	n
Phase	m	n	Phase	m	n	Phase	m	n			
P	m		P	m		P	m		P	m	
0145	12'11	52	0069	14'84	20	0191	9'53	38	8590	11'78	39
0725	12'16	52	0426	14'74	20	0554	9'44	38	9396	11'84	39
1174	12'19	52	0757	14'66	20	1000	9'36	38	9669	11'84	39
1740	12'25	52	1056	14'62	20	1547	9'36	38	9873	11'81	39
2426	12'30	52	1361	14'40	20	1889	9'17	38			
2921	12'31	52	1598	14'26	20	2380	8'99	38	DY Car		
3470	12'33	52	1861	14'27	40	2942	8'86	38	Phase	m	n
4096	12'31	51	2463	14'34	40	3409	8'83	38	P	m	
4624	12'15	30	3006	14'42	40	3900	8'84	38	0012	12'04	41
4962	12'01	30	3450	14'49	40	4487	8'87	38	0334	12'14	41
5282	11'87	30	3787	14'55	40	4843	8'96	38	0760	12'17	41
5543	11'76	30	4209	14'60	40	5150	9'08	38	1241	12'30	41
5812	11'64	30	4722	14'63	40	5636	9'16	38	1638	12'35	41
6300	11'54	30	5268	14'71	40	5998	9'26	38	2081	12'44	41
6714	11'59	51	5862	14'77	40	6411	9'27	38	2464	12'48	41
7197	11'67	52	6436	14'78	40	6799	9'31	38	2835	12'50	40
7660	11'77	52	6808	14'81	40	7231	9'35	38	3447	12'58	40
8385	11'89	52	7251	14'81	40	7524	9'39	38	3874	12'64	40
8966	11'98	52	7640	14'83	40	7872	9'43	38	4353	12'64	40
9507	12'06	52	8083	14'85	40	8328	9'43	38	4657	12'66	40
			8564	14'85	40	8680	9'43	38	5228	12'74	40
			9139	14'87	41	8992	9'48	38	5769	12'75	40
			9664	14'85	41	9310	9'45	38	6292	12'76	40
						9712	9'51	38	6672	12'69	40
									6942	12'66	20
									7225	12'52	20
									7522	12'37	20
									7763	12'21	20
									7970	12'05	20
									8133	12'00	20
									8403	11'93	20
									8744	11'94	40
									9236	11'97	40
									9664	12'00	40
RY Vel			UY Car			XX Vel			CY Car		
Phase	m	n	Phase	m	n	Phase	m	n	Phase	m	n
P	m		P	m		P	m		P	m	
0361	10'10	41	0424	9'79	50	0060	11'83	20	0430	11'24	41
0929	10'19	41	0928	9'87	50	0789	12'01	20	0758	11'29	41
1329	10'24	41	1564	10'00	50	1018	12'13	40	1141	11'28	41
1743	10'29	41	2310	10'20	50	1179	12'12	40	1632	11'34	41
2143	10'40	41	2947	10'38	50	1355	12'18	40	1945	11'29	41
2424	10'45	41	3571	10'55	50	2187	12'26	40	2312	11'33	41
2837	10'47	41	4007	10'63	50	2594	12'32	40	2802	11'26	40
3258	10'50	41	4463	10'67	50	2803	12'34	40	3250	11'20	30
3630	10'65	41	5179	10'82	50	3740	12'40	40	3675	11'05	30
4424	10'72	40	5720	10'83	50	4055	12'40	40	3965	10'91	30
4911	10'71	40	6147	10'85	50	4204	12'39	40	4319	10'81	30
5393	10'72	40	6607	10'91	50	4631	12'32	20	4709	10'69	30
5662	10'60	40	7184	10'92	50	4987	12'20	20	5197	10'64	30
6073	10'45	40	7777	10'92	50	5308	12'03	20			
6510	10'26	40	8337	10'89	50	5502	11'89	40			
6864	10'13	40	8714	10'70	31	5637	11'84	40			
7264	9'97	40	8979	10'56	31	5927	11'69	20			
7583	9'95	40	9332	10'25	31	6487	11'42	20			
7959	9'95	40	9618	10'07	31	6921	11'44	40			
8536	9'97	40	9949	9'85	31	7084	11'47	40			
9084	9'98	40				7358	11'55	20			
9673	10'02	40				7982	11'69	20			
						8423	11'74	40			

TABLE 6 (continued).

Phase	m	n	Phase	m	n	Phase	m	n	EE Car		
									Phase	m	n
P	m		P	m		P	m		P	m	n
5668	10'70	41	2154	13'33	40	0607	13'33	41	0204	13'45	40
6080	10'73	41	2662	13'47	40	1093	13'34	41	0575	13'29	20
6498	10'84	41	3129	13'55	40	1638	13'31	41	0847	13'15	20
6866	10'85	41	3562	13'64	40	2033	13'27	22	1095	13'04	20
7309	10'93	41	3944	13'68	40	2261	13'16	22	1311	12'97	20
7802	11'00	41	4270	13'73	40	2493	13'02	22	1605	12'94	40
8223	11'08	41	4627	13'83	40	2673	12'93	22	2045	12'99	40
8552	11'11	41	5032	13'86	40	2885	12'74	22	2516	13'08	40
8844	11'15	41	5528	13'93	40	3118	12'56	22	2901	13'13	40
9335	11'18	41	6042	13'99	40	3407	12'51	41	3254	13'21	40
9793	11'21	41	6541	14'02	40	3810	12'52	41	3651	13'24	40
			7034	14'06	40	4262	12'68	41	4129	13'30	40
VX Vel			7757	14'07	40	4801	12'86	41	4657	13'33	40
			8127	14'05	40	5254	12'93	41	5242	13'40	40
Phase	m	n	8623	14'05	40	5705	13'01	41	5784	13'43	40
			9128	14'04	40	6178	13'08	41	6308	13'45	40
			9641	14'06	40	6636	13'10	41	6753	13'45	40
P	m		TX Car			7082	13'15	41	7110	13'45	40
0128	14'08	40	Phase	m	n	7513	13'18	41	7435	13'45	40
0527	14'09	22				7970	13'24	41	7823	13'46	40
0845	13'98	22				8450	13'29	41	8201	13'44	40
1101	13'78	22				8861	13'29	41	8620	13'45	40
1337	13'54	22				9303	13'32	41	9166	13'46	40
1571	13'42	22	P	m		9724	13'28	41	9710	13'48	39
1776	13'29	22	0120	13'32	41						

Photographic exposures of RR Leonis in the beginning of the year 1935 measured and discussed by C. *Ƴ.* Kooreman.

In continuation of the publication by P. TH. OOSTERHOFF in *B.A.N.* 206 „On the variability of the period of RR Leonis” 16 plates were taken with the 34 cm refractor, 7 by A. J. WESSELINK, 6 by J. UITTERDIJK and 3 by L. PLAUT. Of these 16 plates 9 contain an ascending branch of the lightcurve. Guilleminot Superguil plates of size 9 × 12 cm were used. The time of one exposure was 2½ min. with an interval of ¼ min. between two consecutive exposures. The total number of exposures is 286. The plates have been measured in the Schilt-photometer. The same comparison stars *a*, *b*, *c* and *d* as in *B.A.N.* 206 have been used.

The reduction of the measurements to differences of magnitude was made in the following manner. By the aid of a normal table the galvanometer readings were converted into provisional magnitudes. Then the variable was interpolated between ½ ($m_a + m_b$) and ½ ($m_c + m_d$). As in Table 1 of *B.A.N.* 206 the mean of the comparison stars was taken as zero point.

The individual results here given in the first three columns of Table 1 form a direct continuation of the same Table of *B.A.N.* 206, the phases having again been calculated from the formula

$$\text{phase} = 2^{d-1} \cdot 210541 \times \\ (\text{J. D. hel. M. astr. T. Grw.} - 242000)$$

In order to derive accurate epochs, those observations were used which lie on that part of the ascending branch that may be considered as rectilinear. For each ascending branch a least square solution was made, assuming Δm to be a linear function of the time. The corresponding residuals are given in the last column of Table 1. The mean error in magnitude for a single observation as derived from the least square solutions was practical the same for OOSTERHOFF's plates and the new ones, viz. ± 0.032 .

In Table 2 the slope of the ascending branch is given separately for each of the 13 plates of OOSTERHOFF and of the 9 new plates, all slopes reduced to $m/2.5$ min.

The two plates 3110 and 3134, which show irregular fog, have nevertheless been given full weight.

The mean slope of OOSTERHOFF's plates is $-0.0884/2.5$ min. and of the new plates $-0.0894/2.5$ min.

The mean error of the slope as derived from the deviations from the mean is $\pm 0.0054/2.5$ min., while the least square solutions give a mean value of $\pm 0.0033/2.5$ min. The difference between these two values is in the direction to be expected, but too small to be considered as real in view of the scantiness of the material.