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PHOTOELECTRIC OBSERVATIONS OF RR LYRAE, BY TH. WALRAVEN

In 1947, 3038 photoelectric observations were made of RR Lyrae. These enabled us to study the changes that take place in the light-curve during the 41-day secondary period. It appeared that the variation is more complicated and that, besides the 41-day period, another period exists, about 3 times longer.

If the phase shift $\Delta\varphi$, for a point on the rising branch where Δm equals $-m\cdot300$, is the decimal fraction of E in PRAGER's elements: J.D. 2414856^d.408 + d^s56683735 E , it may be represented by the formula:

$$\Delta\varphi = P\cdot2908 - P\cdot000037 t - P\cdot0173 \sin \frac{2\pi}{P_k} t - P\cdot0060 \cos \frac{2\pi}{P_k} t - P\cdot0060 \sin \frac{2\pi}{P_k'} t + P\cdot0024 \cos \frac{2\pi}{P_k'} t,$$

where the values 72^P.37 and 108^P.55 have been assumed for P_k and P_k' , respectively. From this formula it appears that the mean phase shift differs P[·]199 from the value found by extrapolating BALAZS and DETRE's formula. The phase in the secondary period agrees with that given by BALAZS and DETRE.

Both periods P_k and P_k' show themselves also in the variation of the shape of the light-curve.

At the phase in the secondary period P_k where the ascending branch of the light-curve is most retarded, it shows a flexure, which was hitherto masked by observational errors. At this same phase Dr STRUVE found some interesting features in the spectrum.

The observations of RR Lyrae were started in order to obtain the exact phase of light variation at the time of Dr STRUVE's observations of the radial velocity at the McDonald Observatory. The previous photometric observations, collected and extensively discussed by BALAZS and DETRE¹⁾, do not permit a reliable prediction of this phase as a consequence of the secondary period and other peculiarities of the light variation.

The Observations.

In March 1947 a provisional photoelectric equipment with a 1P21 RCA multiplier was attached to the 19" reflector of the Leiden Observatory and its performance was sufficiently good to justify the start of the RR Lyrae programme. Some technical data of the instrument follow. Both primary mirror and Newton secondary of the reflector are aluminized, the aperture and focal length are 19 and 100 inch. The mounting is of the fork type, permitting quick and easy manipulation. At the Newton focus a diaphragm with a diameter of .04 inch was placed. A guider telescope provided with crosswired eye piece, attached parallel to the tube of the reflector, permitted exact centring of the star on the diaphragm. After the light has passed the diaphragm it is projected by a simple cylindrical

lens onto the cathode of the phototube as an elongated spot. The multiplier phototube was fed by 90-Volt batteries, one for each of the dynodes, and a 50-Volt battery for the anode circuit which included the galvanometer. This is a Leeds and Northrup type R 2500-g galvanometer having a sensitivity of 5×10^{-10} Ampère per millimetre for a scale distance of 1 metre. No colour filters were used and a large wavelength interval was active. In order to find the effective wavelength some stars with different colours were measured. These were selected from the list of SEARES, ROSS and JOYNER¹⁾.

In Table 1 some data about these stars are reproduced from this list. The sixth column of the table contains measured magnitudes m_{pe} , with arbitrary zero point. Their internal mean error is $\pm m\cdot004$. By least squares the equations of the type

$$m_{pe} = a + b m_{pg} + c m_{pv}$$

were solved and the result was:

$$m_{pe} = -m\cdot622 + \cdot632 m_{pg} + \cdot434 m_{pv} \\ \pm 160 \pm 20 \pm 17$$

In the seventh column of Table 1 the computed magnitudes are given; the last column contains the residuals $O - C$. It appears therefore that the colour response of the instrument was intermediary between

¹⁾ *Mitteilungen der Sternwarte Budapest-Svábhegy*, No. 17, 1943.

¹⁾ 'Magnitudes and Colors of Stars North of $+80^\circ$ '. F. H. SEARES, F. E. ROSS and M. C. JOYNER, Washington 1941.

photographic and photovisual. A similar colour sensitivity was found for other multiplier tubes. This result is at variance with KRON's, who found a photographic or even more violet response.

TABLE I

BD	α (1900)	δ (1900)	m_{pg}	m_{pv}	$m_{pe}(O)$	$m_{pe}(C)$	O-C
	h m	° '					
83 91	3 33.7	83 14	7.51	7.68	7.485	7.463	+ .022
80 55	1 38.8	80 23	7.00	7.10	6.866	6.889	- .023
80 57	1 39.8	80 53	7.47	7.47	7.310	7.347	- .037
80 65	1 57.9	81 0	7.00	6.84	6.784	6.776	+ .008
81 13	0 32.2	81 56	6.88	6.39	6.531	6.504	+ .027
82 76	2 54.3	82 31	7.93	7.04	7.476	7.451	+ .025
82 51	2 1.4	83 6	7.35	6.44	6.848	6.823	+ .025
80 58	1 44.6	80 25	8.26	7.02	7.630	7.651	- .021
80 86	2 33.4	81 2	7.07	5.82	6.362	6.377	- .015
83 56	2 20.3	83 23	7.98	6.62	7.290	7.300	- .010

Most of the observations were made while the author operated the telescope and Mrs WALRAVEN read the galvanometer deflections. At some nights the observations were made by Dr P. TH. OOSTERHOFF and by Mr H. G. VAN BUEREN. The total number of observations of RR Lyrae during 1947 is 3038. Each observation consists of four readings of the deflection while the star was centred on the diaphragm, preceded and followed by two readings of the sky brightness, and the same for a comparison star. In this way, working intensely, the variable could be observed every two minutes. The readings of star and sky were registered with opposite sign on a printing adding machine, which then directly gave the intensity of the star.

TABLE 2

Star	Name	α (1947)	δ (1947)	m_{vis}	Sp.
var.	RR Lyrae	h m 19 23.8	42° 41'	—	—
a	HD 183125	19 24.4	42 13	7.67	A2
b	HD 183383	19 25.7	42 7	7.38	B9
c	HD 182487	19 21.9	42 52	6.89	A0

Some data about the comparison stars are given in Table 2. In general two of the comparison stars, *a* and *b*, were used; when the variable was bright, *c* was also included. The reduction consisted in computing the difference in magnitude between variable and comparison star *a* in the following way. First, the mean of the difference between *a* and *b*, or *a* and *c*, was determined for each night, and this value was used to reduce the observed magnitude of star *b*, or of star *c*, to an indirect magnitude of star *a*.

Then the difference between variable and star *a* was computed, the indirect values for *a* being included. In deriving these differences an observed brightness was always compared to the mean of the

preceding and following values of the comparison stars, in order to take into account the fact that the observations of different stars could not be made simultaneously, but were spaced with equal intervals in time. A correction for differential extinction, amounting to a few thousandths of a magnitude, had to be applied only to the earlier observations; when

TABLE 3

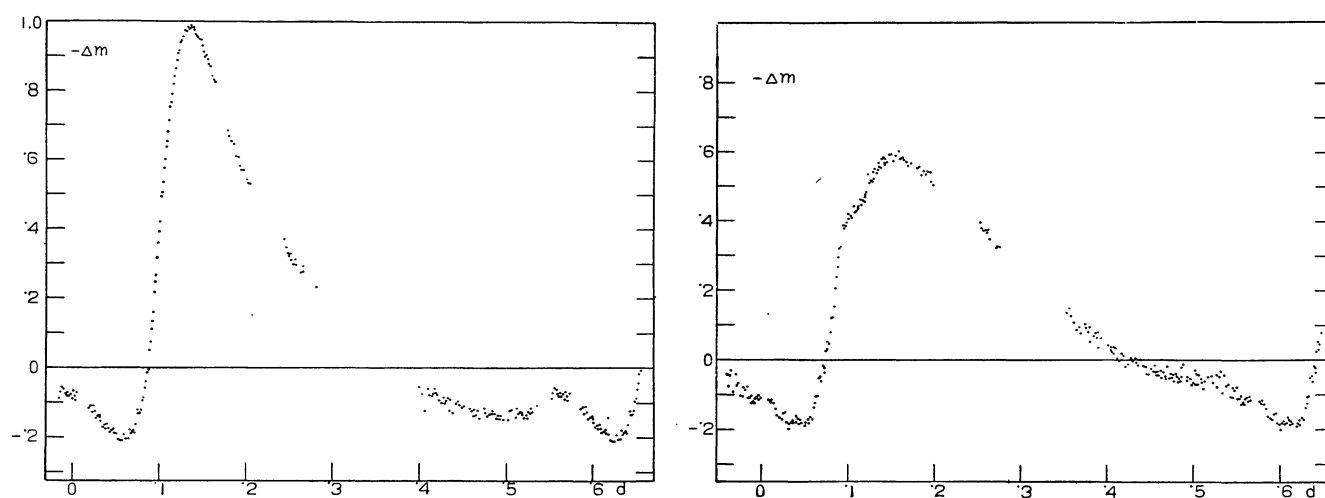
Jul. Day -2430000	$m_a - m_b$	$m_a - m_c$	mean error of one observation
2285.5			
2286.5			
2287.5	.625		m.021
2288.5		1.202	.016
2289.5			
2300.5	.645	1.228	.010
2302.5	.645	1.230	.009
2314.5	.620	1.260	.085
2319.5	.648	1.203	.033
2328.5	.648	1.235	.018
2330.5	.635	1.232	.016
2333.5	.625	1.215	.025
2334.5	.638	1.220	.007
2335.5	.630		.015
2336.5	.628		.013
2348.5	.634		.008
2354.5	.628		.022
2361.5	.632		.012
2362.5	.648		.033
2363.5	.634		.012
2364.5	.625	1.222	.022
2374.5	.642		.010
2376.5	.642		.010
2379.5	.640		.013
2380.5	.642		.025
2381.5	.622	1.202	.017
2382.5	.628		.018
2385.5	.628	1.212	.012
2386.5	.628		.014
2389.5	.628	1.210	.014
2391.5	.625		.011
2394.5	.625		.009
2397.5	.630	1.228	.013
2398.5	.620	1.198	.012
2401.5	.620		.012
2406.5	.622	1.200	.010
2408.5	.622		.014
2409.5	.628		.012
2410.5	.622		.011
2414.5	.622	1.205	.014
2415.5	.625		.014
2418.5	.622		.009
2419.5	.625		.014
2420.5	.625		.009
2423.5	.622		.010
2424.5	.618	1.198	.014
2426.5	.622	1.208	.007
2427.5	.618	1.192	.008
2431.5	.628		.014
2432.5	.618	1.200	.025
2433.5	.620		.009
2441.5	.615		.011
2444.5	.620	1.198	.010
2453.5	.612		.014
2461.5	.618		.012
2465.5	.610		.021
2478.5	.610	1.188	.010
2486.5	.620	1.190	.011

the season had advanced it was negligible. In Table 3 the magnitude differences of stars a and b , $m_a - m_b$, and of stars a and c , $m_a - m_c$, have been compiled. The internal mean error of one determination of magnitude difference as found from the residuals from the mean of the night has been given in the fourth column. This mean error may be supposed to hold also for the observations of the variable.

It appears from the table that the differences in magnitude gradually grow smaller. This is not shown by the difference between b and c . There is some reason for suspicion with respect to the constancy of star a , which is supported by the fact that this star,

HD 183125, has an abnormal spectrum, and its colour according to MÜNCH and TERRAZAS¹⁾, is redder than might be concluded from the spectral type. So it might have been better if another star had been used as a reference standard. The magnitude differences Δm between RR Lyrae and the reference star have been listed in Table 11 at the end of the article. In the first column of this table the heliocentric Julian Day is given. The last column will be discussed below. In order to give a visual impression of the accuracy of the observations, we reproduce two light-curves in Figure 1.

FIGURE 1



Examples of light-curves at different phases of the secondary period, directly composed of individual observations.

Our first aim will be to derive from our observations epochs which are necessary to find the phases of the primary period P of about $^d.57$ and of the secondary period P_k of 41^d . The most accurate epochs can be derived from the ascending branches, and usually the epoch is determined as the moment at which the median brightness between minimum and maximum is reached.

In the case of RR Lyrae, however, the magnitude at maximum varies strongly, as does, less pronounced, also the magnitude at minimum and hence the median magnitude is not constant. For several nights of observing the median magnitude was unknown because the adjacent maximum and minimum had not been observed. In the following discussion therefore the epochs were determined for a fixed magnitude, for which the value $\Delta m = -^m.300$ was chosen, which is near the average median magnitude. But even this procedure could not be strictly adhered to. Usually we first estimated which part of the ascending branch could be considered to be straight. The constants in the equation $\Delta m = a + b t$ were then solved by least

squares from the observations on this straight part of the rising branch. Finally the value of t was determined for which Δm equals $-^m.300$. Later in this article we shall see that the rising branch sometimes shows a flexure near the time of median brightness, where the increase in brightness is much slower than in the remaining parts of the rising branch or where the brightness may even be nearly constant for a short while. In such cases the least-squares solution has been made for observations on a straight part of the rising branch below the flexure and the epoch t , derived from an extrapolation of the linear equation does not coincide in this case with the time at which the variable actually reached brightness $\Delta m = -^m.300$. Although this procedure introduces some arbitrariness it probably is as good as any other.

In Table 4 the solutions have been collected. The first column of this table gives the Julian Days of the moment at which Δm equals $-^m.300$. The second column contains b , the units of time and magnitude

¹⁾ *Ap. J.* 103, 371, 1946.

TABLE 4

J.D. - 2430000	<i>b</i> units m'001 d'0001	m.e. of one observation	<i>E</i>	J.D. - 2430000	<i>b</i> units m'001 d'0001	m.e. of one observation	<i>E</i>
2330'45942	- 2'279	± '021 ^m	30827'2759	2423'44104	- 1'669	± '009 ^m	30991'3117
± 23	± 67		± 4	± 25	± 38		± 4
2335'56726	- 1'868	± '016	30836'2870	2424'57235	- 1'958	± '012	30993'3075
± 17	± 40		± 3	± 28	± 61		± 5
2364'46864	- 2'437	± '018	30887'2741	2427'40908	- 1'670	± '010	30998'3120
± 17	± 63		± 3	± 65	± 100		± 11
2381'48992	- 1'825	± '029	30917'3026	2431'37117	- 2'120	± '006	31005'3018
± 147	± 203		± 26	± 7	± 19		± 1
2385'45737	- 2'599	± '031	30924'3019	2432'50300	- 2'283	± '017	31007'2986
± 52	± 215		± 9	± 17	± 48		± 3
2389'42056	- 2'546	± '011	30931'2936	2441'55535	- 2'469	± '007	31023'2685
± 13	± 52		± 2	± 33	± 75		± 6
2394'51674	- 3'123	± '013	30940'2842	2444'38660	- 3'184	± '011	31028'2633
± 10	± 49		± 2	± 9	± 47		± 2
2398'47627	- 2'980	± '009	30947'2695	2453'45823	- 2'300	± '009	31044'2672
± 7	± 35		± 1	± 13	± 51		± 2
2406'40912	- 2'140	± '010	30961'2644	2461'40569	- 2'046	± '006	31058'2880
± 11	± 31		± 2	± 11	± 35		± 2
2410'38275	- 1'671	± '012	30968'2746	2465'37691	- 2'230	± '025	31065'2939
± 17	± 31		± 3	± 47	± 150		± 8
2415'49042	- 1'925	± '018	30977'2854	2478'40449	- 1'998	± '016	31088'2768
± 28	± 65		± 5	± 16	± 40		± 3
2419'46609	- 1'843	± '016	30984'2992	2486'33583	- 1'968	± '027	31102'2691
± 45	± 89		± 8	± 38	± 93		± 7

being d'0001 and m'001. The mean error of one observation, as found from the residuals, is given in the third column. These may be compared to that found from the comparison stars in Table 3. The last

column will be explained below. The observations which were used in the computation and their residuals (*O - C*) have been listed in Table 5.

TABLE 5

<i>t</i>	Δm	<i>O-C</i>	<i>t</i>	Δm	<i>O-C</i>	<i>t</i>	Δm	<i>O-C</i>	<i>t</i>	Δm	<i>O-C</i>
-2432330'4400			-2432335'5500			-2432364'4500			-2432385'4400		
89	-'072	-'012	98	-'158	+'003	125	-'185	-'035	136	-'177	+'025
106	-'108	-'010	105	-'175	-'001	135	-'158	+'016	149	-'276	-'040
124	-'110	+'030	111	-'208	-'023	145	-'195	+'004	171	-'316	-'023
145	-'175	+'013	117	-'170	+'026	158	-'205	+'025	184	-'342	-'016
158	-'270	-'053	123	-'200	+'008	168	-'258	-'003	196	-'352	+'006
172	-'260	-'011	130	-'198	+'022	177	-'260	+'017			
193	-'295	+'002	139	-'255	-'017	185	-'305	-'009	-2432389'4000		
207	-'310	+'019	145	-'262	-'014	196	-'350	-'026	98	-'015	+'011
224	-'332	+'036	152	-'260	+'002	206	-'355	-'007	106	-'035	+'011
238	-'398	+'002	163	-'285	-'003	217	-'395	-'021	126	-'098	'000
252	-'420	+'012	170	-'298	-'002	225	-'395	-'001	135	-'130	-'010
270	-'472	'000	176	-'352	-'046	236	-'418	+'003	153	-'182	-'016
283	-'500	+'002	183	-'322	-'002	248	-'438	+'012	176	-'220	+'005
297	-'542	-'008	190	-'342	-'009	255	-'472	-'005	190	-'257	+'003
311	-'582	-'014	197	-'350	-'004	263	-'468	+'018	205	-'310	-'012
336	-'645	-'022	203	-'348	+'009				219	-'332	+'002
349	-'640	+'012	211	-'368	+'004	-2432381'4600			233	-'382	-'012
			218	-'378	+'007	79	+'087	-'015	257	-'417	+'014
			225	-'408	-'010	146	+'008	+'028	260	-'447	-'008
-2432335'5500			234	-'412	+'003	153	-'005	+'028	282	-'482	+'013
15	-'010	-'004	259	-'470	-'008	188	-'142	-'045			
23	-'008	+'012	266	-'438	+'037	200	-'130	-'012	-2432394'5000		
30	-'028	+'006				236	-'170	+'014	58	+'015	-'027
40	-'080	+'028	-2432364'4500			247	-'205	-'001	70	+'007	+'003
48	-'062	+'006	64	-'012	-'010				85	-'052	-'010
55	-'075	+'005	76	-'012	+'019	-2432385'4400			96	-'075	+'001
63	-'090	+'006	86	-'032	+'023	49	-'008	-'032	108	-'110	+'004
70	-'112	-'004	95	-'088	-'011	73	-'040	-'002	118	-'135	+'011
77	-'098	+'024	104	-'090	+'009	91	-'080	+'005	130	-'160	+'023
84	-'142	-'008	114	-'148	-'024	122	-'109	+'057	139	-'215	-'004
91	-'138	+'010				127	-'160	+'018	152	-'247	+'005

TABLE 5 (continued)

<i>t</i>	Δm	<i>O-C</i>	<i>t</i>	Δm	<i>O-C</i>	<i>t</i>	Δm	<i>O-C</i>	<i>t</i>	Δm	<i>O-C</i>
-2432394'5000			-2432410'3600			-2432427'3900			-2432453'4400		
163	-.265	+.021	329	-.465	+.005	156	-.250	-.008	126	-.170	.000
174	-.317	+.003				168	-.260	+.002	148	-.202	+.019
185	-.360	-.008	-2432415'4700						160	-.270	-.001
197	-.392	.000	49	-.025	-.024	-2432431'3500			190	-.325	-.007
207	-.420	+.004	60	-.030	-.008	72	-.010	-.006	212	-.372	-.004
219	-.490	-.029	71	-.055	-.011	91	-.042	+.002	235	-.418	+.003
231	-.505	-.007	84	-.050	+.018	113	-.092	-.002	259	-.480	-.004
243	-.535	+.001	99	-.080	+.018	129	-.125	-.001			
254	-.575	-.005	113	-.122	+.002	144	-.145	+.011	-2432461'3900		
266	-.602	+.006	128	-.125	+.028	157	-.185	-.001	33	-.052	-.006
			140	-.157	+.019	172	-.207	+.009	48	-.078	-.001
-2432398'4600			154	-.205	-.002	184	-.240	+.001	62	-.100	+.006
66	+.002	+.014	170	-.242	-.008	197	-.265	+.003	79	-.128	+.012
79	-.062	-.012	183	-.270	-.011	208	-.305	-.013	97	-.180	-.003
94	-.092	+.003	196	-.297	-.013	221	-.322	-.002	110	-.212	-.008
106	-.137	-.006	208	-.322	-.015	232	-.347	-.005	124	-.230	+.002
119	-.162	+.008	223	-.330	+.006	243	-.365	+.001	142	-.272	-.002
130	-.195	+.007	234	-.390	-.033	255	-.392	.000	159	-.310	-.006
140	-.240	-.008	252	-.382	-.010	266	-.420	-.005	172	-.332	-.002
152	-.262	+.006	260	-.387	+.020	286	-.455	+.002	186	-.362	-.002
163	-.297	+.003				297	-.492	-.012	201	-.382	+.008
176	-.350	-.010	-2432419'4500			309	-.495	+.011			
188	-.380	-.005	02	.000	+.007	320	-.530	.000	-2432465'36		
200	-.415	-.004	15	-.028	+.003	331	-.550	-.002	43	-.038	-.020
212	-.460	-.014	29	-.055	+.001				58	-.045	+.007
226	-.488	.000	46	-.085	+.003	-2432432'4800			71	-.070	+.011
238	-.537	-.013	69	-.132	-.002	98	-.020	-.022	88	-.135	-.016
251	-.560	+.003	87	-.182	-.018	113	-.032	-.004	103	-.132	+.020
262	-.590	+.006	104	-.195	.000	127	-.070	-.006	119	-.160	+.028
274	-.615	+.017	123	-.227	+.003	142	-.085	+.014	132	-.220	-.003
			141	-.292	-.029	156	-.125	+.006	145	-.242	+.004
-2432406'3900			155	-.295	-.006	182	-.160	+.030	158	-.320	-.055
59	-.022	-.005	170	-.282	-.034	189	-.192	+.014	189	-.352	-.008
73	-.048	-.001				211	-.262	-.006	201	-.352	+.019
83	-.075	-.007	-2432423'2600			225	-.310	-.022			
94	-.097	-.006	26	+.005	+.003	237	-.325	-.009	-2432478'3800		
113	-.110	+.022	39	-.020	-.006	249	-.367	-.024	95	-.005	-.005
118	-.145	-.002	55	-.042	-.002	266	-.390	-.008	112	-.045	-.011
133	-.170	+.005	65	-.047	+.010	291	-.405	+.034	127	-.058	+.006
147	-.215	-.010	74	-.060	+.012	302	-.462	+.002	138	-.082	-.004
159	-.232	-.001	87	-.097	-.005	317	-.505	-.007	151	-.080	+.032
173	-.260	+.001	98	-.110	+.002	340	-.542	+.009	166	-.122	+.020
186	-.277	+.012	111	-.140	-.006	360	-.610	-.014	178	-.168	-.002
198	-.302	+.013	124	-.167	-.013	369	-.617	.000	189	-.205	-.017
210	-.345	-.005	137	-.172	-.006				203	-.215	+.001
223	-.367	+.001	149	-.187	+.012	-2432441'5600			214	-.242	-.004
238	-.415	-.015	161	-.222	-.004	11	-.440	+.002	226	-.265	-.003
251	-.445	+.017	173	-.255	-.017	28	-.478	+.006	237	-.279	+.005
266	-.460	.000	187	-.260	.000	45	-.538	-.012	251	-.322	-.010
283	-.490	-.006	200	-.275	+.008	64	-.568	+.005	266	-.342	.000
298	-.522	-.006	215	-.305	+.003	81	-.618	-.003	276	-.395	-.033
						98	-.658	-.001	286	-.412	-.030
-2432410'3600			-2432424'5500			113	-.690	+.004	297	-.412	-.008
41	+.008	+.003	72	+.002	+.005				308	-.430	-.004
61	-.035	-.013	84	-.032	-.005	-2432444'3700			323	-.452	+.004
82	-.072	-.016	95	-.048	.000	77	-.020	-.003	334	-.475	+.003
100	-.067	+.010	107	-.077	-.005	89	-.052	+.003	345	-.472	+.028
115	-.120	-.008	120	-.080	+.017	104	-.095	+.007	356	-.510	+.012
127	-.137	-.005	137	-.135	-.005	118	-.150	+.003	368	-.538	+.008
141	-.137	+.018	153	-.152	+.010	134	-.182	+.016			
153	-.165	+.011	167	-.195	-.006	143	-.248	-.021	-2432486'3200		
166	-.172	+.025	181	-.235	-.019	164	-.280	+.014	24	-.035	.000
179	-.217	+.001	195	-.255	-.011	175	-.338	-.010	45	-.062	+.014
195	-.262	-.016	209	-.282	-.010	186	-.382	-.018	64	-.087	+.027
207	-.260	+.006	223	-.282	+.017	214	-.440	+.012	82	-.142	+.008
219	-.285	+.001	236	-.315	+.009	228	-.505	-.007	99	-.165	+.018
233	-.315	-.006				240	-.540	-.004	120	-.242	-.018
245	-.335	-.006	-2432427'3900			251	-.572	-.002	138	-.292	-.032
257	-.352	-.003	52	-.065	+.003	264	-.610	+.002	160	-.332	-.029
270	-.375	-.004	65	-.085	+.005	276	-.640	+.010	180	-.360	-.018
288	-.415	-.014	80	-.130	-.015				203	-.425	-.037
301	-.427	-.005	97	-.152	-.009	-2432453'4400			239	-.438	+.020
315	-.437	+.009	109	-.150	+.013	70	-.052	-.010	258	-.500	-.004
			124	-.180	+.008	103	-.115	+.003	276	-.485	+.047

The variations in the period.

We adapt our discussion to the scheme of BALAZS and DETRE by using the formula of PRAGER,

$$\text{Julian Day of median magn.} = 2414856.408 + d.56683735 E \quad (1)$$

to compute E , of which the integer gives the cycle number and the decimal fraction the phase deviation $\Delta\phi$, called $(B - R)_{M_{gr}}$ in BALAZS and DETRE's article, expressed in the primary period P . In the fourth column of Table 4 the values of E computed for the epochs in the first column of that table, are given. The phase deviation $\Delta\phi$ is shown in Figure 2 (dots), as a function of the cycle number minus 30800¹⁾.

This figure clearly shows the secondary period of about 72 cycles, but also it is clear that the points of the successive secondary cycles cannot be combined into one curve. The amplitude is varying and also the length of the secondary period is variable. This phenomenon might have been found earlier by BALAZS and DETRE if their observations had been more numerous. Now it revealed itself only by a large scatter of their $(B - R)_{M_{gr}}$. A similar unexpected large scattering has been noticed by OOSTERHOFF in the case of RS Boo²⁾, another RR Lyrae-type variable with secondary period. It is very curious that in the case of the numerous and closely spaced observations of RR Lyrae by ZACHAROW³⁾, which reveal this phenomenon distinctly, it was ascribed by BALAZS and DETRE to systematic errors. An annoying consequence

of the effect is that it is now impossible to find the exact $\Delta\phi$ at the time of STRUVE's observations between J.D. 2432340 and J.D. 2432380, corresponding to our cycle numbers 30840 and 30915. It was tried therefore to find an interpolation formula representing $\Delta\phi$ for the whole interval covered by the observations. The secondary period had to be taken from BALAZS and DETRE's discussion.

Their formula, (9a):

$$P_k = 71^{P.83} \sin^{0.004168} (E - 9870)$$

gives for $E = 30800$, the secondary period $P_k = 72^{P.37}$ at the time of our observations.

The varying amplitude may be caused by another period. Its length was estimated as follows. We certainly had a large amplitude near $E = 31100$, and probably it was minimal near $E = 30900$ and $E = 31100$, i.e. the beat period P_b equals about 200 cycles. BALAZS and DETRE's figures show exceptionally large deviations for E equal to about 25130. Finally ZACHAROV's observations show a large amplitude for $E = 17540$ and $E = 16680$ (cf. BALAZS and DETRE's article, page 31). From these data it follows that the beat period may be close to 217 cycles. We assumed it to be exactly three times the secondary period P_k or $P_b = 217^{P.11}$. This beat period may be caused by interference of the secondary period P_k with a third period P_k' , being equal to $3/2 P_k$ or to $3/4 P_k$. It is directly seen from the run of $\Delta\phi$ that we must choose $P_k' = 3/2 P_k = 108^{P.55}$. We then made a least-squares solution of the following type:

$$\Delta\phi = a + bt + c \sin \frac{2\pi}{P_k} t + d \cos \frac{2\pi}{P_k} t + e \sin \frac{2\pi}{P_k'} t + f \cos \frac{2\pi}{P_k'} t,$$

the linear term $b t$ being introduced to account for the apparent decrease of the mean of $\Delta\phi$. The unit of t is

one cycle and its zero point is at $E = 30800.3$. The result obtained is:

$$\Delta\phi = \begin{matrix} P.2908 & - & P.000037 & t & - & P.0173 & \sin & \frac{2\pi}{P_k} & t & - & P.0060 & \cos & \frac{2\pi}{P_k} & t & - & P.0060 & \sin & \frac{2\pi}{P_k'} & t & + & P.0024 & \cos & \frac{2\pi}{P_k'} & t. \end{matrix} \quad (2)$$

± 12 ± 16 ± 6 ± 6 ± 6 ± 7

The phase deviations used in the computation are given in Table 6. Some of them are the mean of some observations having small weight, which is caused by the irregular shape of the ascending branch, at the time when the light-curve is most retarded. The other columns of the table contain the computed phase deviations and the residuals $O - C$. The solution is

represented by the full-drawn line in Figure 2. There also the line $(a + b t)$ is shown. It was not considered worth while to repeat the elaborate computations for other lengths of the periods, for the following reasons. The representation of the observed values by the solution is quite satisfactory if the residuals in the well observed regions are compared to those in the other regions. Secondly, if there is a second and third period, it is probable that also other periods may exist. Moreover it is not necessary that the variations are strictly sinusoidal.

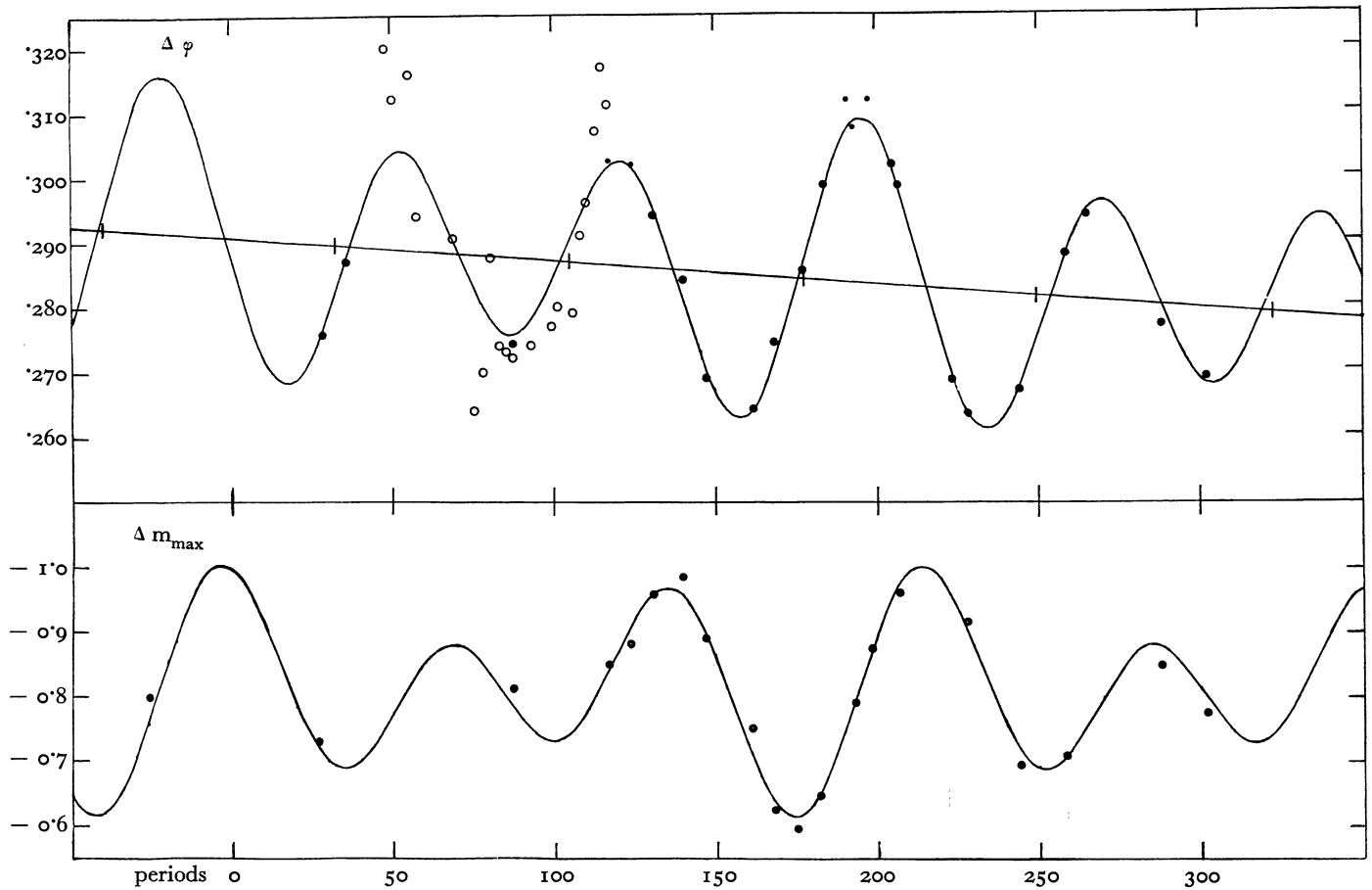
Let us now consider the constants of the solution. Constant a represents the present-day secular error

¹⁾ It should be noticed that the whole number subtracted by STRUVE and BLAAUW in order to get their cycle numbers is 30843; *Ap. J.* 108, 60, 1948.

²⁾ *B.A.N.* No. 369, 101, 1946, and private communication.

³⁾ The results of this author are given in BALAZS and DETRE's article.

FIGURE 2



Above: Variation of phase shift of the epoch of median brightness. Dots - values observed photoelectrically; full-drawn curve - computed interpolation formula (2); open circles - epochs of mean radial velocity, as found by STRUVE and BLAAUW.

Below: Variation of maximum magnitude. Dots - values observed photoelectrically; full-drawn curve - computed interpolation formula (3)

of PRAGER's formula and b its present rate of change. We may compare this quantity to the value predicted

$$\overline{(B - R)}_{M_{gr}} = 0.069 - 0.0000235 E + 0.116 \sin 0.00989 (E - 15500),$$

which becomes, after inserting $E = 30800.3 + t$, taking the first two terms of the Taylor development and expressing in periods instead of days:

$$\overline{(B - R)}_{M_{gr}} = 0.0923 - 0.0000351 t.$$

It appears that our a deviates much from the predicted value, whereas b agrees well. The large discrepancy is not disturbing, as BALAZS and DETRE's formula had to be extrapolated. Probably $\overline{(B - R)}_{M_{gr}}$ reached a higher value and began to decrease later than according to the formula. This result is confirmed by one observation by GORDON and KRON¹⁾ of an epoch at Julian Day 2432061.8023, from which

¹⁾ K. C. GORDON and G. E. KRON. *Ap.J.* 106, 318, 1947.

by BALAZS and DETRE, called by them $\overline{(B - R)}_{M_{gr}}$. These authors derived the formula:

follows $E = 30353.3179$ or $\Delta\phi = 0.318$, much larger than the predicted maximum of $\overline{(B - R)}_{M_{gr}}$, which is 0.217. Our interpolation formula (2) gives at the time of GORDON and KRON's observation $\Delta\phi = 0.326$.

Let us now consider the secondary period, which is represented by the third and fourth terms on the right-hand side of formula (2). These may be combined to $0.0183 \sin \frac{2\pi}{P_k} (t - 32^P.38)$. The amplitude 0.0183 is smaller than that of BALAZS and DETRE, who found 0.0265. For this effect a probable explanation will be given below. The moments at which the phase, ψ , of the secondary period is zero can be found as $E_{\psi=0} = 30832^P.68 + n \times 72^P.37$, where n denotes a number of secondary cycles. It should be noted that

these are not the moments at which $\Delta\phi$ reaches its mean value. The moments for which $\psi = 0$ are indicated in Figure 2 by vertical dashes.

For this quantity $E_{\psi=0}$ BALAZS and DETRE also give a formula:

$$E_{(B-R)_{Mgr}} = 171^{P \cdot 9} + 71^{P \cdot 83} e - 103^{P \cdot 1} \cos^{\circ} 30(e - 136).$$

TABLE 6

<i>t</i>	$\Delta\phi$ observed	$\Delta\phi$ computed	<i>O-C</i>
	P	P	P
27	.2759	.2757	+ .0002
36	.2870	.2888	- .0018
87	.2741	.2757	- .0016
122	.3021	.3021	.0000
131	.2936	.2949	- .0013
140	.2842	.2808	+ .0034
147	.2695	.2700	- .0005
161	.2644	.2639	+ .0005
168	.2746	.2711	+ .0035
177	.2854	.2869	- .0015
184	.2992	.2992	.0000
193	.3101	.3081	+ .0020
205	.3018	.3011	+ .0007
207	.2986	.2981	+ .0005
223	.2685	.2693	- .0008
228	.2633	.2634	- .0001
244	.2672	.2676	- .0004
258	.2880	.2879	+ .0001
265	.2939	.2946	- .0007
288	.2768	.2801	- .0033
302	.2691	.2680	+ .0011

Inserting $e = 427$, which is the number of secondary cycles elapsed at $E = 30832$, we find:

$$E_{(B-R)_{Mgr}} = 30838^{P \cdot 4},$$

deviating only about 6 primary cycles from our result. This is a rather good agreement, which is, however, accidental, as also in this case the extrapolation of the earlier observations is uncertain.

Finally the last two terms of (2) give the interfering third period P_k' which is 3/2 times the secondary period P_k . They may be combined to:

$$P \cdot 0064 \sin \frac{2\pi}{P_k'} (t - 60^{P \cdot 87}).$$

The moments at which the phase χ of the third period is zero can be found as $E_{\chi=0} = 30861^{P \cdot 17} + m \times 108^{P \cdot 55}$ where m denotes a number of cycles. Nothing more can be remarked about this period than that its reality seems assured. Its exact length and the question whether it is variable cannot be determined from the present observations. Long continuous series of observations will be necessary to study this, and still unknown periods, thoroughly.

The variations in the shape of the light-curve.

Together with the varying phase also the shape of the light-curve changes. This is shown most pronounced in the height of the maximum which varies within a wide range. The variations occur so quickly that the portions of light-curves observed within an interval of some days cannot be combined into one curve. Therefore the curves of Figure 1 do not represent real light-curves. When it was tried to combine observations of subsequent secondary periods it appeared that the influence of the third period manifested itself also in the shape of the light-curve. It turned out impossible to describe fully all variations of the light-curve during our observational period. The only thing we could do, was to obtain a system of mean light-curves, showing the variation in the period P_k . The real light-curves deviate more or less from these, depending on the phase of the beat period. The system of mean curves was obtained as follows. In order to distinguish clearly between phase shift and

TABLE 7

ϕ'	Δm	ϕ'	Δm	ϕ'	Δm	ϕ'	Δm	ϕ'	Δm	ϕ'	Δm	ϕ'	Δm
2285	6.83	2288	6.90	2300	7.19	2302	7.24	2330	7.93	2334	8.02	2335	8.04
.800 + .010		.060 - .618		.100 - .796		.800 + .107		.990 - .183		.150 - .615		.920 + .194	
		.080 - .613		.120 - .792		.820 + .120		.000 - .300		.200 - .512		.940 + .170	
2286	6.85	.100 - .606		.150 - .726		.840 + .140		.010 - .420		.250 - .420		.960 + .096	
		.150 - .556		.200 - .578				.020 - .570				.980 - .090	
.400 - .190		.200 - .443		.250 - .466		2314	7.54	.030 - .630		2335	8.04	.990 - .200	
.450 - .112				.300 - .375		.800 + .074		.040 - .656		.700 + .062		.000 - .300	
.500 - .054		2289	6.93					.060 - .700		.725 + .047		.010 - .406	
.550 - .016		.800 + .042		2302	7.24	2319	7.66	.080 - .722		.750 + .046			
.600 + .005		.840 + .075		.625 + .077		.800 + .080		.100 - .730		.775 + .057		2336	8.06
		.880 + .113		.650 + .090		.820 + .080		.120 - .703		.800 + .082		.500 - .090	
2287	6.88	.900 + .132		.675 + .110				.150 - .610		.820 + .107		.550 - .035	
		.920 + .146		.700 + .130		2328	7.87	2333	8.00	.840 + .128		.600 + .011	
.250 - .394		.940 + .120		.725 + .142				.860 + .150		.860 + .150		.625 + .030	
.300 - .294		.960 + .040		.750 + .130		.500 - .041		.880 + .170		.880 + .170		.650 + .046	
.350 - .227		.980 - .100		.775 + .107		.550 - .002		.900 + .188		.900 + .188		.675 + .055	
.400 - .178													

TABLE 7 (continued)

φ'	Δm	φ'	Δm	φ'	Δm	φ'	Δm	φ'	Δm	φ'	Δm	φ'	Δm
2336	8-06	2376	9-05	2386	9-29	2398	9-58	2415	0-00	2424	0-22	2444	0-70
'700 + '058		'150 - '695		'820 + '135		'000 - '300		'980 - '065		'020 - '353		'120 - '756	
'725 + '062		'200 - '585		'840 + '144		'010 - '480		'990 - '170		'030 - '383			
		'250 - '465		'860 + '162		'020 - '615		'000 - '300		'040 - '456		2453	0-92
2348	8-35			'880 + '180		'030 - '739		'010 - '386		'060 - '636		'900 + '165	
'650 + '108		2379	9-11	'900 + '203		'040 - '810		'020 - '410		'080 - '760		'920 + '185	
'675 + '127		'350 - '295		'920 + '218		'060 - '885		'030 - '430				'940 + '166	
'700 + '145		'400 - '212		'940 + '200		'080 - '888		'040 - '448		2426	0-26	'960 + '117	
'725 + '150		'450 - '142		'960 + '130		'100 - '837		'060 - '503		'120 - '814		'980 - '035	
'750 + '145		'500 - '077		'980 + '024		'120 - '771		'080 - '558		'150 - '725		'990 - '160	
'775 + '115		'550 - '018								'200 - '585		'000 - '300	
'800 + '095		'600 + '020		2389	9-36	2401	9-65	2418	0-07	'250 - '455		'010 - '435	
'820 + '103				'940 + '198		'940 + '150		'100 - '604				'020 - '527	
'840 + '130		2380	9-14	'960 + '126		'960 + '105		'120 - '644		2427	0-29	'030 - '575	
'860 + '159		'100 - '870		'980 - '022		'980 - '042		'150 - '625		'980 - '106		'040 - '616	
		'120 - '820		'990 - '155		'990 - '168		'200 - '550		'990 - '192		'060 - '666	
2354	8-51	'150 - '745		'000 - '300		'000 - '302		'250 - '453		'000 - '270		'080 - '688	
'250 - '416		'200 - '608		'010 - '450				'300 - '357		'010 - '340		'100 - '692	
'300 - '326		'250 - '470		'020 - '545		2406	9-78			'020 - '416		'120 - '671	
'350 - '236				'030 - '630		'000 - '300		2419	0-10	'030 - '500			
'400 - '150		2381	9-17	'040 - '727		'010 - '434		'880 + '180		'040 - '600		2461	1-12
'450 - '065		'840 + '134		'060 - '905		'020 - '522		'900 + '192		'060 - '790		'900 + '184	
'500 + '010		'860 + '165		'080 - '955		'030 - '590		'920 + '186		'080 - '874		'920 + '190	
		'880 + '186		2391	9-40	'040 - '649		'940 + '160		'100 - '853		'940 + '159	
2361	8-67	'900 + '202		'550 + '075		'060 - '730		'960 + '067		'120 - '802		'960 + '092	
'625 + '065		'920 + '202		'600 + '108		'080 - '749		'980 - '095				'980 - '070	
'650 + '073		'940 + '177		'625 + '120		'100 - '718		'990 - '195		2431	0-39	'990 - '180	
'675 + '078		'960 + '107		'650 + '130		'120 - '677		'000 - '290		'960 + '107		'000 - '300	
'700 + '070		'980 - '090		'675 + '136				'010 - '325		'980 - '063		'010 - '385	
'725 + '056		'990 - '187		'700 + '139		2408	9-82	'020 - '334		'990 - '166		'020 - '397	
'750 + '045		'000 - '262		'725 + '136		'675 + '010		'030 - '345		'000 - '300		'030 - '407	
'775 + '044		'010 - '328		'750 + '130		'700 + '013		'040 - '373		'010 - '416		'040 - '451	
'800 + '046		'020 - '375				'725 + '018		'060 - '462		'020 - '535		'060 - '568	
'820 + '059		'030 - '430		2394	9-49	'080 - '558		'080 - '558		2432	0-41	'080 - '678	
'840 + '072		'040 - '522		'820 + '074		'100 - '632		'100 - '632		'980 - '068		'100 - '706	
		'060 - '682		'840 + '085		'120 - '650		'120 - '650		'990 - '151		'120 - '702	
2362	8-70	'080 - '815		'860 + '105				2420	0-11	'000 - '300		2465	1-21
'400 - '150		'100 - '850		'880 + '140		'350 - '301		'650 + '044		'010 - '435		'920 + '180	
		'120 - '810		'900 + '170		'400 - '224		'675 + '059		'020 - '554		'940 + '175	
2363	8-73	'150 - '725		'920 + '200		'450 - '160		'700 + '077		'030 - '688		'960 + '100	
'150 - '604				'940 + '203		'500 - '105		'725 + '094		'040 - '829		'980 - '056	
'200 - '478		2382	9-18	'960 + '158		'550 - '055		'750 + '088		'060 - '954		'990 - '168	
'250 - '377		'625 + '070		'980 + '043		'600 - '015		'775 + '060		'080 - '945		'000 - '300	
		'650 + '086		'990 - '112				'800 + '073		'100 - '872		'010 - '365	
2364	8-76	'675 + '099		'000 - '300		2410	9-87	'820 + '094					
'900 + '150		'700 + '108		'010 - '480		'980 - '104				2433	0-43	2478	1-53
'920 + '159		'725 + '116		'020 - '581		'990 - '202		'000 - '300		'500 + '015		'960 + '098	
'940 + '150		'750 + '116		'030 - '775		'000 - '300		'010 - '402				'980 - '075	
'960 + '095		'775 + '106		'040 - '873		'010 - '402		'020 - '464		2440	0-61	'990 - '193	
'980 - '020		'800 + '106		'060 - '976		'020 - '464		'030 - '500		'860 + '055		'000 - '300	
'990 - '150		'820 + '127		'080 - '920		'030 - '500		'040 - '527		'880 + '085		'010 - '430	
'000 - '300		'840 + '153		'100 - '900		'060 - '580		'060 - '580		'900 + '210		'020 - '505	
'010 - '445		'860 + '190		'120 - '825		'080 - '620		'080 - '620		'920 + '209		'030 - '602	
'020 - '565				2397	9-56	'100 - '600		'100 - '620		'940 + '160		'040 - '695	
'030 - '640		2385	9-27	'100 - '830		'120 - '600		'120 - '600		'960 + '059		'060 - '954	
'040 - '715		'980 - '010		'120 - '760		'150 - '558		'150 - '558		'980 - '100		'080 - '945	
'060 - '802		'990 - '135		'150 - '663		'200 - '465		'200 - '465		'990 - '202		'100 - '872	
'080 - '800		'000 - '300		'200 - '502		2414	9-97	'000 - '282		'000 - '282		'010 - '714	
'100 - '755		'010 - '385		2398	9-58	'060 - '527		'010 - '322		'020 - '364		'040 - '824	
'120 - '695		'020 - '458		'840 + '066		'080 - '557		'020 - '364		'030 - '406			
'150 - '604		'030 - '533		'860 + '085		'100 - '585		'040 - '406		'040 - '406		2444	0-70
		'040 - '648		'880 + '112		'120 - '593		'060 - '455		'060 - '455		'960 + '140	
2374	8-99	'060 - '820		'900 + '140		'150 - '564		'080 - '597		'080 - '597		'980 + '009	
'625 + '014		'080 - '880		'920 + '167		'200 - '500						'990 - '178	
'650 + '022		'100 - '866		'940 + '168		2415	0-00	2424	0-22	'920 + '200		'000 - '300	
'675 + '025		'120 - '815		'960 + '134		'860 + '120		'940 + '164		'940 + '164		'010 - '493	
'700 + '030		'150 - '712		'980 + '021		'880 + '150		'960 + '085		'960 + '085		'020 - '641	
'725 + '037		'200 - '572				'900 + '174		'980 - '065		'980 - '065		'030 - '756	
'750 + '048				'990 - '140		'920 + '180		'990 - '185		'990 - '185		'040 - '834	
						'940 + '162		'000 - '290		'000 - '290		'060 - '770	
						'960 + '082		'010 - '328		'010 - '328		'080 - '772	
										'100 - '895		'100 - '738	
										'120 - '832		'120 - '682	

variation in shape, from all phases computed with (1), which are given in the last column of Table 11, the amount given by (2) was subtracted, with as result the reduced phase φ' . In this way the variation of the phase deviation is eliminated and the rising branches of all light-curves pass through the same point. At this point the reduced phase φ' is zero. Then at a number of other phases φ' , chosen with suitable intervals, the observed magnitudes Δm were read from the light-curves. These are collected in Table 7.

For each night at the top of the columns is given

the Julian Day of midnight minus 2430000.5 and the phase ψ of the secondary period, together with the last figure of its cycle number ϵ . Then for each reduced phase Δm is plotted against ψ , using different symbols for subsequent secondary cycles. In this way it is clearly demonstrated that most of the scatter is due to the change from cycle to cycle. Some of the graphs are shown in Figure 3. In the plots the mean curves are drawn, represented by dashed lines. The values of $-\Delta m$ at phase $\psi = 0, .1, .2$ etc., of these curves are given in Table 8.

TABLE 8

$\varphi' \backslash \psi$.1	.2	.3	.4	.5	.6	.7	.8	.9	1.0	mean
.01	-.347	-.341	-.376	-.433	-.468	-.478	-.459	-.432	-.401	-.372	-.411
.02	-.375	-.376	-.445	-.525	-.578	-.591	-.566	-.520	-.478	-.424	-.488
.03	-.383	-.426	-.527	-.631	-.714	-.717	-.654	-.582	-.505	-.434	-.557
.04	-.438	-.484	-.592	-.728	-.815	-.812	-.741	-.657	-.570	-.491	-.633
.06	-.550	-.637	-.759	-.879	-.939	-.908	-.831	-.743	-.657	-.580	-.748
.08	-.652	-.762	-.858	-.916	-.936	-.886	-.833	-.757	-.673	-.633	-.791
.10	-.713	-.804	-.849	-.867	-.859	-.826	-.782	-.724	-.673	-.670	-.777
.12	-.712	-.777	-.807	-.810	-.800	-.769	-.726	-.682	-.650	-.662	-.740
.15	-.672	-.711	-.725	-.715	-.684	-.668	-.636	-.602	-.590	-.616	-.662
.20	-.564	-.584	-.577	-.559	-.535	-.510	-.486	-.472	-.477	-.523	-.529
.25	-.463	-.464	-.452	-.439	-.424	-.408	-.394	-.389	-.401	-.430	-.426
.30	-.360	-.372	-.366	-.349	-.329	-.309	-.294	-.289	-.297	-.328	-.329
.35	-.292	-.295	-.286	-.260	-.236	-.223	-.214	-.220	-.238	-.266	-.253
.40	-.214	-.207	-.189	-.168	-.151	-.146	-.153	-.166	-.185	-.182	-.176
.45	-.140	-.122	-.096	-.076	-.068	-.070	-.084	-.101	-.121	-.133	-.101
.50	-.086	-.061	-.021	+.008	+.014	+.004	+.016	+.038	+.057	+.083	-.034
.55	-.025	+.009	+.053	+.074	+.067	+.050	+.028	+.003	-.018	-.029	+.021
.60	+.015	+.050	+.085	+.104	+.099	+.076	+.046	+.015	-.005	-.007	+.048
.62	+.039	+.071	+.099	+.115	+.108	+.084	+.058	+.034	+.017	+.017	+.064
.65	+.049	+.081	+.108	+.121	+.115	+.095	+.068	+.044	+.025	+.026	+.073
.67	+.062	+.099	+.123	+.131	+.118	+.091	+.059	+.030	+.012	+.026	+.075
.70	+.077	+.117	+.138	+.139	+.119	+.085	+.054	+.024	+.016	+.036	+.080
.72	+.081	+.125	+.147	+.140	+.114	+.079	+.048	+.021	+.016	+.037	+.081
.75	+.080	+.120	+.144	+.132	+.102	+.068	+.038	+.019	+.017	+.042	+.076
.77	+.068	+.103	+.118	+.109	+.088	+.063	+.040	+.025	+.025	+.042	+.068
.80	+.084	+.104	+.105	+.096	+.081	+.064	+.045	+.029	+.031	+.057	+.070
.82	+.107	+.120	+.120	+.109	+.089	+.070	+.056	+.053	+.065	+.086	+.088
.84	+.137	+.144	+.138	+.118	+.088	+.068	+.062	+.068	+.086	+.109	+.102
.86	+.159	+.171	+.165	+.141	+.105	+.073	+.063	+.073	+.100	+.130	+.118
.88	+.180	+.190	+.180	+.158	+.129	+.101	+.083	+.089	+.118	+.150	+.138
.90	+.195	+.207	+.204	+.187	+.164	+.141	+.126	+.127	+.146	+.171	+.167
.92	+.196	+.201	+.199	+.188	+.173	+.156	+.150	+.155	+.164	+.183	+.176
.94	+.168	+.172	+.175	+.175	+.171	+.166	+.156	+.153	+.154	+.161	+.165
.96	+.088	+.094	+.103	+.112	+.123	+.125	+.121	+.113	+.099	+.090	+.107
.98	-.081	-.076	-.057	-.038	-.016	-.006	-.015	-.030	-.054	-.072	-.044
.99	-.189	-.187	-.175	-.160	-.144	-.138	-.141	-.153	-.173	-.183	-.164
.00	-.294	-.287	-.281	-.300	-.300	-.300	-.300	-.300	-.300	-.300	-.296

The mean light-curve for each ψ was obtained by plotting this Δm against φ' . They are given in Figure 4. One of the most conspicuous features in these curves is the flexure on the rising branch which occurs near phase $\psi = .1$. While ψ is progressing, the maximum rises and the upper portion of the rising branch becomes steeper, the flexure also rises slowly and gradually fades out. In the mean curves of Figure 4 these effects are shown less sharply than in the real light-curves, as a consequence of smoothing out the variations with the third period. If, as in earlier discussions, the flexure is masked by the observational

errors, the epoch of median magnitude will be found later than by our method of using the lower portion of the rising branch. This may be the explanation of our amplitude of the secondary variation being smaller than BALAZS and DETRE'S. Another interesting feature of the light-curve is the secondary maximum just before minimum, which is most sharply defined near the phase $\psi = .5$, when also the primary maximum is highest. Near phase $\psi = 0$ this secondary maximum nearly disappears, leaving only a flat portion in the light-curve. During the secondary period the maximum, the minimum and the second-

FIGURE 3

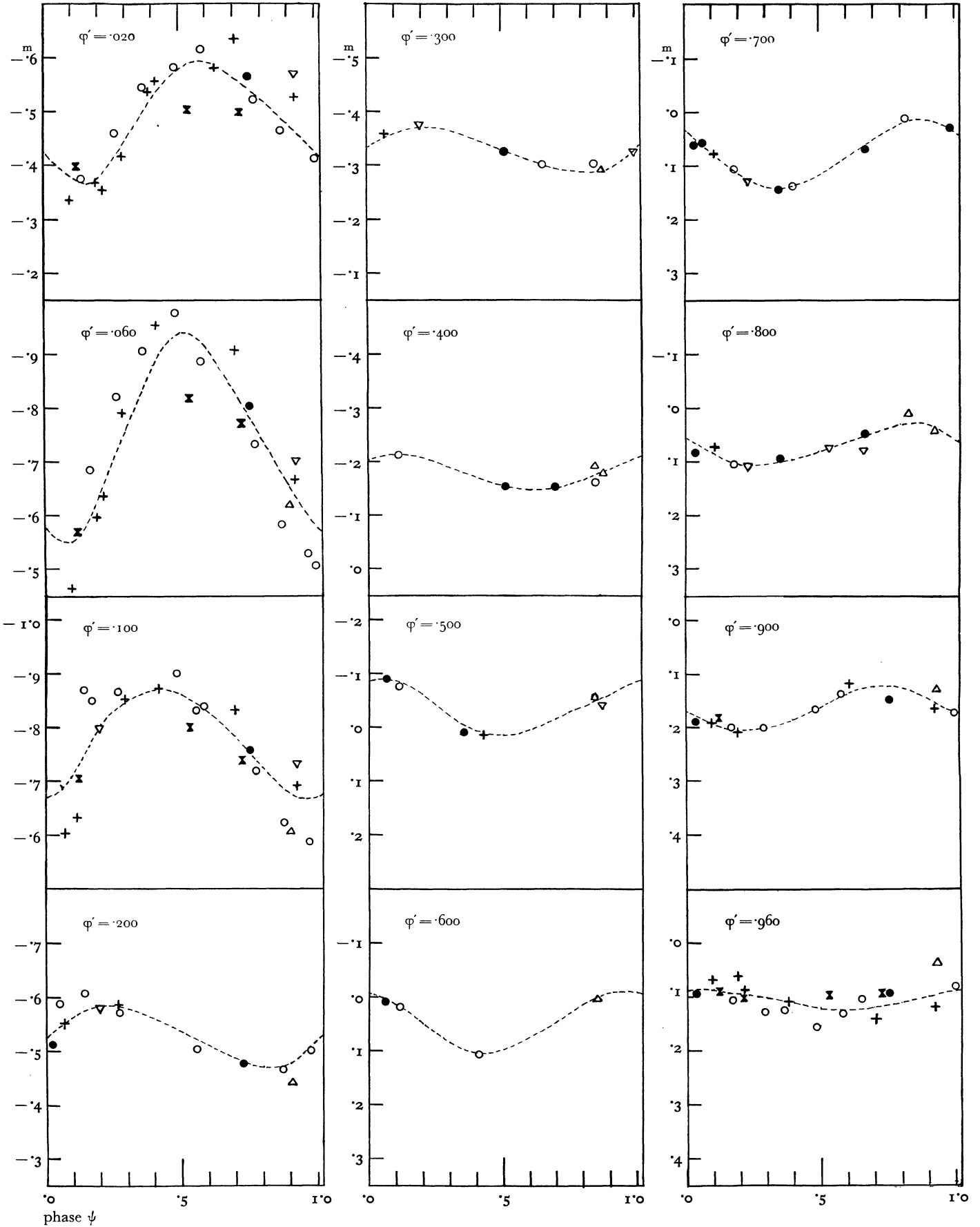
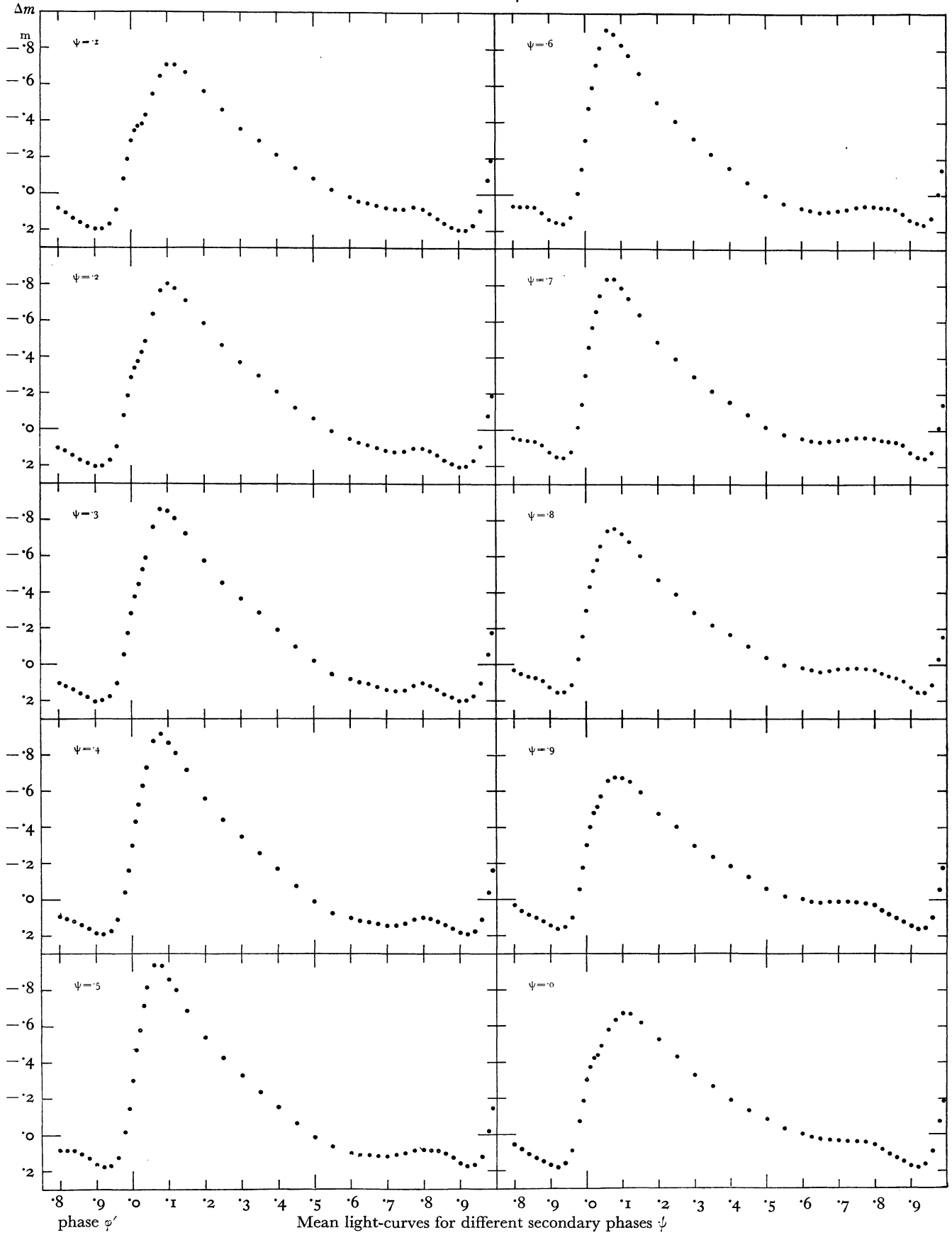


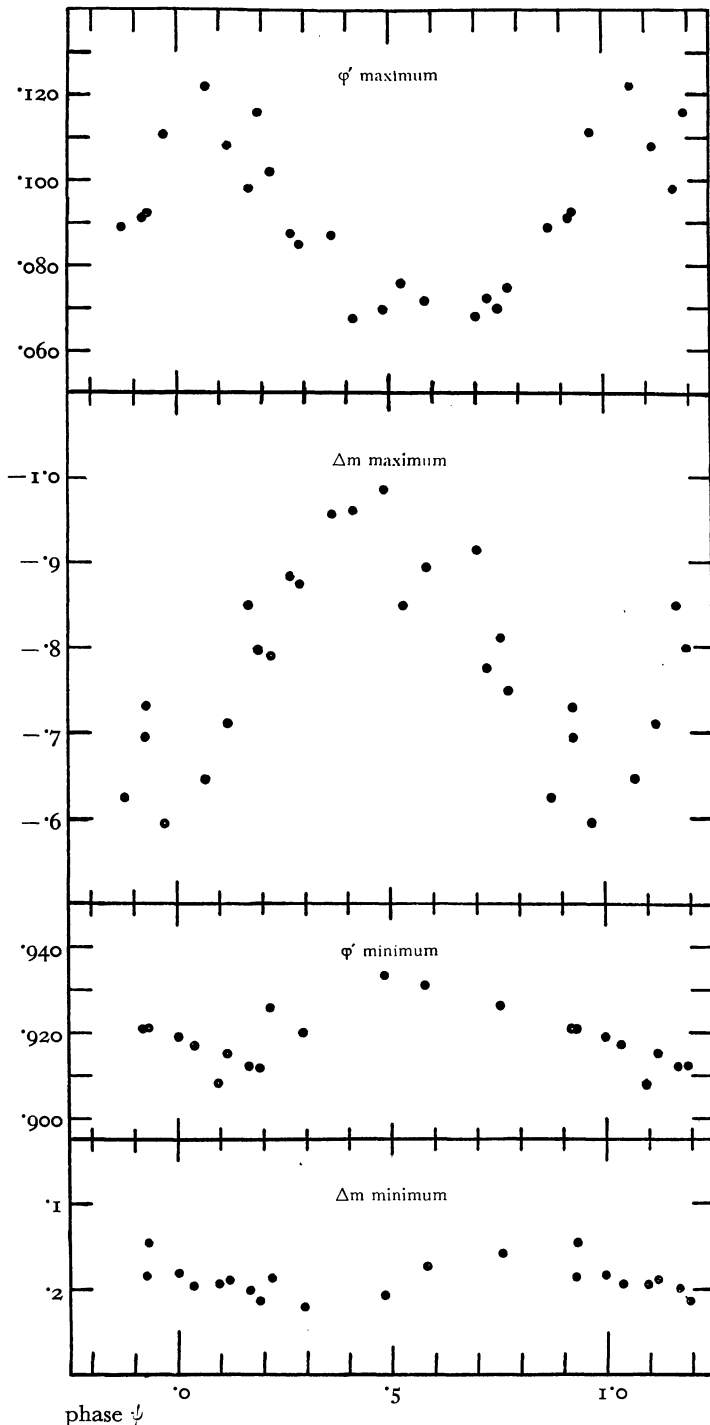
FIGURE 4



ary maximum of the mean light-curves are varying both in height and in phase.

The variations are large for the maximum and much less pronounced for the minimum. Moreover the variations do not occur in the same phase, as can be seen in Figure 4. This is more clearly demonstrated

FIGURE 5



Variation of phase and height of maximum and minimum. Successive secondary cycles have been combined into one.

in Figure 5, where the reduced phases and magnitudes of both maximum and minimum, as read from the observed light-curves, are plotted against ψ . It may be noted that in these graphs again much of the scattering is due to the third period. Figure 5 is based on the values given in Tables 9 and 10. The first columns of these tables contain the Julian Days of the observed maxima or minima. The reduced phases ϕ' were obtained by using the observed moments of median brightness in Table 4. If the adjacent moment of median brightness has not been observed, the value computed with the interpolation formula (2) was used.

Let us now consider the real light-curves. As has been stated already, these cannot be described in full detail. Nevertheless some idea could be obtained from the material by a careful study. It appeared thus that:

- a). The system of light-curves described during a secondary period never coincides with the system of mean curves given in Figure 4.
- b). The light-curves vary in shape most intensely when also the phase shift of the light-curve oscillates with its largest amplitude and vice versa.
- c). The time required to run through the system of curves varies in the same way as the period of oscillation of the phase shift $\Delta\phi$. For example, the time of most pronounced flexure always occurs just before maximum retardation of the light-curve.
- d). The variations are strongest about the maximum of the light-curve, much less pronounced for the minimum, and are not perceptible for a large portion of the descending branch. Some of the above-mentioned effects are very clearly demonstrated by

TABLE 9

J.D.	<i>E</i>	Δm maximum	Δm computed	<i>O-C</i>	ϕ' maximum
2300'505	30774'431	- '798	- '754	- '044	P '116
2330'514	827'372	- '729	- '719	- '010	'096
2364'508	887'344	- '810	- '784	- '026	'070
2381'544	917'398	- '850	- '839	- '011	'095
2385'506	924'388	- '882	- '910	+ '028	'086
2389'470	931'381	- '955	- '958	+ '003	'087
2394'556	940'353	- '985	- '957	- '028	'069
2398'517	947'341	- '892	- '900	+ '008	'072
2406'452	961'340	- '750	- '712	- '038	'076
2410'433	968'363	- '625	- '639	+ '014	'088
2414'421	975'399	- '593	- '615	+ '022	'111
2418'400	982'418	- '645	- '649	+ '004	'122
2424'630	993'409	- '790	- '794	+ '004	'102
2427'456	998'395	- '875	- '867	- '008	'083
2432'543	31007'369	- '960	- '973	+ '013	'067
2444'425	028'331	- '915	- '903	- '012	'068
2453'510	044'359	- '693	- '720	+ '027	'092
2461'467	058'396	- '708	- '706	- '002	'108
2478'447	088'352	- '848	- '877	+ '029	'075
2486'376	102'340	- '775	- '799	+ '024	'072

the observed heights of the maxima of the light-curves. In Table 9 these maxima are given as they are read from the observed light-curves.

TABLE IO

J.D. -2430000	φ' minimum	Δm minimum
2289'608	'921	'145
2335'520	'917	'195
2304'426	'926	'160
2381'438	'909	'200
2386'545	'920	'218
2394'479	'933	'208
2398'437	'931	'175
2415'444	'919	'182
2419'414	'908	'194
2423'390	'910	'214
2453'413	'921	'185
2461'358	'915	'190
2465'335	'926	'185

The second column of the table gives the phase computed with formula (1) at the moment when the maximum is reached. In Figure 2 the observed heights are plotted against cycle numbers. Introducing again the secondary period P_k and the third period $P_k' = 3/2 P_k$ we could find the least-squares solution representing the height of the maximum as a function of t , which is the time expressed in cycles with a zero-point at $E = 30800.4$:

$$\begin{aligned} \Delta m_{max} = & m.814 - m.060 \sin \frac{2\pi}{P_k} t + m.116 \cos \frac{2\pi}{P_k} t \\ & \pm .006 \pm .008 \quad \pm .008 \\ & + m.029 \sin \frac{2\pi}{P_k'} t + m.065 \cos \frac{2\pi}{P_k'} t. \quad (3) \\ & \pm .007 \quad \pm .010 \end{aligned}$$

The maximum as computed with this formula is given as the full-drawn line in Figure 2. The residuals of the observed values are given in the fifth column of Table 9. It may be noted here that the third period P_k' exhibits itself in the maxima with about the same degree of certainty as in the phase shifts, although these quantities are observed entirely independently of each other.

The observed relation between the height of maximum and phase shift will have to be explained by the theory of the pulsation of stars like RR Lyrae. One might expect that the phase shift $\Delta\varphi$ is the integral result of a variation in period due to some periodic disturbance exhibiting itself also in the height of the maximum, and therefore the maximum magnitude should be correlated with the derivative of $\Delta\varphi$ with respect to time. It is not possible to decide whether this is really the case, for, although the observations can be satisfied by such a relation, it is also possible, and with better result, to represent the phase shift as proportional to the derivative of the height of maximum.

Comparison with the radial-velocity curves.

Before closing the discussion a few remarks will be made concerning the radial-velocity programme of RR Lyrae by STRUVE and BLAAUW¹⁾. One of the results of that programme, the epochs of median radial velocity, may be directly compared with our values from the light-curves. This has been done in Figure 2, where STRUVE and BLAAUW's observations are represented by open circles. The agreement of phase is good, but the amplitude of the radial-velocity values is larger than that predicted by our formula for the light-curves. However, the amplitude depends very much on the method applied in determining the phase shift of the light-curve. The large deviations at that phase of the secondary period where the light-curve is most retarded, would disappear if, in determining the epoch of mean magnitude, not only the lower portion, but the whole of the ascending branch were taken into account, with neglect of the flexure.

It may be noted that at about the same phase of the secondary period hydrogen emission lines have been found by STRUVE during the increase of the star's brightness. Therefore, this moment is interesting in more than one respect, and future observations of colour and spectral-line intensities may prove of great value for the study of this star.

¹⁾ *Ap.J.* 108, 60, 1948.

TABLE II

J.D. Hel. -2430000	Δm	phase	J.D. Hel. -2430000	Δm	phase	J.D. Hel. -2430000	Δm	phase	J.D. Hel. -2430000	Δm	phase
d 2285'5475	m +'.004	P '0434	d 2285'5686	m +'.004	P '0807	d 2286'5351	m -'018	P '7858	d 2286'5542	m -'045	P '8194
'5503	+'.014	'0484				'5362	-'031	'7877	'5552	-'027	'8212
'5537	+'.004	'0544	2286'4728	-'179	'6758	'5372	-'031	'7895	'5569	-'017	'8242
'5548	+'.004	'0563	'4759	-'160	'6813	'5414	-'065	'7969	'5736	-'008	'8538
'5572	+'.009	'0606	'4860	-'185	'6991	'5424	-'032	'7986	'5750	+'.004	'8561
'5582	-'001	'0623	'4891	-'149	'7046	'5472	-'037	'8071	'5763	-'018	'8584
'5620	-'001	'0690	'5268	-'058	'7711	'5483	-'019	'8090			
'5645	+'.022	'0734	'5279	-'066	'7730	'5493	-'017	'8108	2287'5310	-'338	'5427
'5655	+'.021	'0752	'5292	-'061	'7753	'5531	-'017	'8175	'5320	-'368	'5445

TABLE II (continued)

J.D. Hel. -2430000	Δm	phase	J.D. Hel. -2430000	Δm	phase	J.D. Hel. -2430000	Δm	phase	J.D. Hel. -2430000	Δm	phase
d 2287'5331	m -366	P '5464	d 2289'6012	m +112	P '1949	d 2302'4971	m +084	P '9455	d 2319'5738	m +105	P '0718
'5452	-344	'5677	'6025	+130	'1972	'4999	+076	'9504	'5762	+040	'0760
'5459	-308	'5690	'6053	+220	'2021	'5019	+104	'9540	'5796	+032	'0820
'5559	-271	'5866	'6081	+134	'2071	'5040	+084	'9577	'5817	+112	'0857
'5570	-287	'5886	'6095	+127	'2095	'5068	+092	'9626	'5838	+112	'0894
'5580	-272	'5903	'6109	+170	'2120	'5096	+095	'9676	'5859	+092	'0931
'5635	-282	'6000	'6115	+161	'2131	'5116	+091	'9711	'5887	+080	'0981
'5649	-262	'6025	'6199	+046	'2279	'5137	+088	'9748			
'5660	-252	'6044	'6254	+119	'2376	'5165	+083	'9797	2328'4557	+085	'7410
'5975	-203	'6600	'6268	'000	'2401	'5192	+093	'9845	'4571	+082	'7435
'5985	-198	'6618	'6275	+119	'2413	'5248	+111	'9944	'4585	+040	'7460
'5996	-183	'6637	'6289	+049	'2438	'5269	+118	'9981	'4599	+038	'7484
'6054	-193	'6740	'6309	+061	'2473	'5289	+123	'0016	'4619	+090	'7519
'6061	-176	'6752	'6358	-064	'2559	'5317	+121	'0066	'4633	+042	'7544
'6072	-170	'6771	'6372	-083	'2584	'5352	+135	'0127	'4647	+045	'7569
'6142	-170	'6863	'6386	-074	'2609	'5379	+140	'0175	'4668	+060	'7606
'6134	-180	'6881	'6406	-008	'2644	'5407	+127	'0224	'4682	+068	'7631
			'6420	-165	'2669	'5428	+134	'0261	'4696	+048	'7655
2288'5450	-681	'3316				'5456	+147	'0311	'4710	+032	'7680
'5460	-662	'3333	2300'4955	-795	'4143	'5476	+132	'0346	'4731	+038	'7717
'5492	-597	'3390	'4983	-789	'4193	'5504	+150	'0395	'4772	-020	'7789
'5502	-597	'3407	'5003	-795	'4228	'5525	+137	'0432	'4786	+022	'7814
'5523	-565	'3444	'5024	-802	'4265	'5546	+137	'0470	'4800	+020	'7839
'5533	-595	'3462	'5052	-785	'4315	'5566	+132	'0505	'4814	-012	'7863
'5561	-671	'3512	'5073	-795	'4352	'5587	+160	'0542	'4835	+040	'7901
'5595	-635	'3572	'5100	-792	'4399	'5608	+130	'0579	'4849	+025	'7925
'5616	-567	'3609	'5121	-777	'4436	'5629	+124	'0616	'4869	+030	'7961
'5651	-645	'3670	'5149	-767	'4486	'5657	+142	'0665	'4890	+028	'7998
'5685	-635	'3730	'5170	-755	'4523	'5684	+104	'0713	'4904	+020	'8022
'5727	-616	'3804	'5190	-745	'4558	'5712	+114	'0762	'4925	-008	'8059
'5755	-620	'3854	'5218	-739	'4607	'5740	+120	'0812	'4939	+032	'8084
'5775	-620	'3889	'5239	-729	'4644	'5767	+103	'0859	'4960	+008	'8121
'5830	-563	'3938	'5260	-717	'4681	'5795	+106	'0909	'4974	+008	'8146
'5845	-610	'4013	'5287	-707	'4729	'5830	+116	'0971	'4994	+010	'8181
'5872	-588	'4060	'5315	-695	'4778	'5857	+111	'1018	'5015	+002	'8218
'5900	-583	'4110	'5329	-677	'4803	'5892	+091	'1080	'5029	'000	'8243
'5928	-576	'4159	'5350	-652	'4840	'5920	+121	'1129			
'5956	-536	'4208	'5371	-645	'4877	'5940	+116	'1165	2330'4489	-072	'2574
'5983	-580	'4256	'5426	-636	'4974	'5968	+116	'1214	'4506	-108	'2604
'6025	-558	'4330	'5447	-618	'5011	'5996	+113	'1263	'4524	-110	'2635
'6053	-566	'4380	'5474	-598	'5059	'6017	+103	'1300	'4545	-175	'2672
'6108	-598	'4477	'5495	-593	'5096	'6044	+103	'1348	'4558	-270	'2695
'6136	-529	'4526	'5523	-596	'5145	'6065	+133	'1385	'4572	-260	'2720
'6281	-431	'4782	'5544	-560	'5182	'6086	+126	'1422	'4593	-295	'2757
'6309	-421	'4831	'5571	-556	'5230	'6107	+116	'1459	'4607	-310	'2782
'6336	-447	'4879	'5592	-560	'5267	'6127	+149	'1494	'4624	-332	'2812
'6364	-394	'4928	'5613	-528	'5304	'6148	+133	'1532	'4638	-398	'2836
'6385	-409	'4965	'5641	-508	'5354	'6162	+149	'1556	'4652	-420	'2861
'6406	-399	'5002	'5661	-518	'5389				'4670	-472	'2893
'6433	-374	'5050	'5689	-506	'5438	2314'4590	+100	'0484	'4683	-500	'2916
			'5710	-498	'5475	'4618	+088	'0533	'4697	-542	'2941
2289'5319	+063	'0726	'5731	-496	'5512	'4666	+055	'0618	'4711	-582	'2965
'5347	+033	'0776	'5751	-478	'5548	'4687	+100	'0655	'4736	-645	'3009
'5367	+048	'0811	'5786	-490	'5609	'4708	+060	'0692	'4749	-640	'3032
'5399	+053	'0867	'5807	-459	'5646	'4743	+110	'0754	'4763	-628	'3057
'5437	+011	'0935	'5835	-471	'5696	'4771	+058	'0803	'4777	-672	'3082
'5503	+058	'1051	'5862	-439	'5743	'4791	+222	'0838	'4791	-652	'3106
'5534	+061	'1106	'5890	-439	'5793	'4812	-042	'0876	'4805	-638	'3131
'5568	+055	'1166	'5911	-441	'5830	'4833	-002	'0913	'4826	-638	'3161
'5596	+075	'1215	'5938	-444	'5878	'4847	+150	'0937	'4836	-655	'3186
'5624	+088	'1264	'5966	-421	'5927	'4896	-032	'1024	'4854	-652	'3218
'5651	+073	'1312	'6001	-389	'5989	'4916	+088	'1059	'4871	-692	'3248
'5686	+114	'1374	'6035	-389	'6049	'4937	+090	'1096	'4888	-700	'3278
'5852	+122	'1667	'6056	-354	'6086	'5021	+045	'1244	'4906	-672	'3309
'5894	+110	'1741	'6077	-387	'6123				'4920	-698	'3334
'5915	+052	'1778	'6112	-389	'6185	2319'5630	+122	'0527	'4937	-700	'3364
'5928	+124	'1801				'5651	+068	'0564	'4954	-720	'3394
'5935	+127	'1813	2302'4867	+074	'9272	'5671	+115	'0600	'4968	-692	'3419
'5956	+115	'1850	'4895	+076	'9321	'5692	+092	'0637	'4986	-722	'3450
'5984	+180	'1900	'4936	+086	'9393	'5713	+040	'0674	'4996	-715	'3468

TABLE I (continued)

J.D. Hel. -2430000	Δm	phase	J.D. Hel. -2430000	Δm	phase	J.D. Hel. -2430000	Δm	phase	J.D. Hel. -2430000	Δm	phase
2330 ^d 5010	-708	P3493	2333 ^d 4821	-338	P6085	2335 ^d 4367	+058	P0567	2335 ^d 5463	+090	P2501
5020	-705	3510	4842	-268	6122	4377	+042	0585	5475	+068	2522
5034	-732	3535				4391	+080	0609	5485	+090	2539
5041	-720	3547	2334 ^d 5155	-638	4316	4409	+048	0641	5495	+088	2557
5055	-720	3572	5172	-628	4346	4423	+032	0666	5506	+015	2577
5069	-738	3597	5190	-608	4377	4436	+098	0689	5515	-010	2592
5079	-712	3614	5204	-592	4402	4471	+045	0751	5523	-008	2607
5086	-722	3627	5217	-598	4425	4489	+075	0782	5530	-028	2619
5107	-695	3664	5231	-595	4450	4502	+070	0805	5540	-080	2637
5121	-725	3689	5249	-578	4481	4516	+070	0830	5548	-062	2651
5131	-715	3706	5263	-572	4506	4530	+108	0855	5555	-075	2663
5142	-750	3726	5277	-580	4531	4548	+108	0886	5563	-090	2677
5156	-730	3750	5294	-580	4561	4565	+082	0916	5570	-112	2689
5170	-705	3775	5308	-558	4585	4579	+088	0941	5570	-098	2702
5180	-748	3793	5329	-565	4623	4603	+080	0983	5584	-142	2714
5197	-698	3823	5336	-562	4635	4617	+112	1008	5591	-138	2726
5208	-722	3842	5349	-560	4658	4631	+110	1033	5598	-158	2739
5232	-722	3884	5370	-548	4695	4645	+105	1058	5605	-175	2751
5246	-712	3909	5391	-540	4732	4655	+128	1075	5611	-208	2762
5260	-635	3934	5408	-540	4762	4669	+125	1100	5617	-170	2772
5274	-682	3959	5426	-528	4794	4680	+128	1129	5623	-200	2783
5288	-715	3983	5447	-518	4831	4690	+115	1137	5630	-198	2795
5305	-655	4013	5461	-508	4855	4700	+110	1155	5639	-255	2811
5319	-725	4038	5474	-515	4878	4714	+108	1179	5645	-262	2822
5333	-740	4063	5488	-505	4903	4725	+120	1199	5652	-260	2834
5343	-648	4080	5502	-510	4928	4745	+108	1234	5663	-285	2853
5354	-688	4100	5516	-502	4952	4759	+110	1259	5670	-298	2866
5361	-680	4112	5530	-485	4977	4780	+142	1296	5676	-352	2876
5371	-640	4130	5544	-485	5002	4794	+112	1320	5683	-322	2889
5378	-635	4142	5558	-480	5027	4811	+140	1350	5690	-342	2901
5388	-720	4160	5572	-488	5051	4825	+155	1375	5697	-350	2913
5409	-648	4197	5586	-482	5076	4857	+150	1432	5703	-348	2924
5416	-595	4209	5599	-472	5099	4888	+122	1486	5711	-368	2938
5423	-688	4221	5613	-480	5124	4902	+165	1511	5718	-378	2951
5433	-625	4239	5627	-482	5148	4919	+155	1541	5725	-408	2963
5447	-615	4264	5655	-455	5198	4930	+160	1560	5734	-412	2979
5458	-535	4283	5669	-465	5222	4940	+182	1578	5759	-470	3023
5475	-630	4313	5683	-442	5247	4950	+162	1596	5766	-438	3035
			5697	-430	5272	4964	+178	1620			
2333 ^d 4241	-460	5061	5711	-418	5296	4975	+162	1640	2336 ^d 3982	-137	7530
4255	-495	5086	5731	-415	5332	4989	+162	1664	3999	-152	7560
4269	-448	5111	5738	-422	5344	4999	+155	1682	4020	-122	7597
4286	-450	5141				5009	+172	1700	4048	-105	7646
4303	-435	5171	2335 ^d 3933	+032	9801	5023	+175	1724	4076	-082	7695
4321	-428	5202	3950	+070	9831	5075	+192	1816	4114	-095	7763
4345	-430	5245	3964	+068	9856	5120	+188	1896	4135	-075	7800
4363	-428	5277	3975	+058	9876	5159	+185	1964	4190	-102	7897
4383	-408	5312	3995	+038	9911	5169	+178	1982	4204	-090	7921
4408	-405	5356	4009	+038	9936	5180	+218	2001	4218	-082	7946
4425	-408	5386	4020	+095	9955	5190	+178	2029	4232	-097	7971
4442	-392	5426	4034	+042	9980	5200	+235	2037	4246	-050	7995
4460	-400	5448	4048	+102	0004	5214	+185	2061	4284	-070	8062
4477	-378	5478	4068	+062	0040	5228	+190	2086	4298	-077	8087
4501	-375	5520	4079	+055	0059	5239	+185	2105	4315	-065	8117
4519	-352	5552	4093	+042	0084	5252	+208	2128	4333	-080	8149
4540	-378	5589	4107	-002	0108	5263	+190	2148	4350	-032	8179
4557	-362	5619	4186	+020	0248	5277	+195	2173	4367	-062	8209
4574	-345	5649	4200	+008	0273	5291	+180	2197	4444	-052	8345
4592	-352	5681	4214	+070	0297	5301	+198	2215	4458	-040	8369
4613	-368	5718	4225	+070	0317	5315	+158	2240	4472	-037	8394
4630	-352	5748	4235	+032	0334	5325	+175	2257	4485	-025	8417
4647	-370	5778	4245	+058	0352	5343	+160	2289	4499	-022	8442
4665	-368	5809	4256	+065	0371	5353	+162	2307	4513	-017	8466
4682	-312	5839	4270	+045	0396	5367	+140	2331	4527	-037	8491
4706	-315	5882	4284	+030	0421	5379	+148	2352	4538	-035	8511
4724	-318	5913	4298	+050	0445	5393	+118	2377	4558	-002	8546
4744	-268	5949	4311	+038	0468	5405	+115	2398	4583	+002	8590
4762	-282	5980	4325	+070	0493	5420	+108	2425	4610	-020	8638
4783	-256	6018	4339	+072	0528	5439	+085	2458	4628	-010	8669
4800	-310	6048	4357	+052	0549	5452	+080	2481	4649	+022	8706

TABLE I (continued)

J.D. Hel. -2430000	Δm	phase	J.D. Hel. -2430000	Δm	phase	J.D. Hel. -2430000	Δm	phase	J.D. Hel. -2430000	Δm	phase
d	m	P	d	m	P	d	m	P	d	m	P
2336'4687	+ '010	'8773	2348'4666	+ '162	'0437	2354'5158	- '098	'7156	2361'5478	+ '082	'1212
4718	- '008	'8828	4694	+ '150	'0487	'5182	- '085	'7198	'5502	+ '075	'1255
4742	+ '002	'8870	4711	+ '140	'0517	'5202	- '078	'7233	'5520	+ '060	'1287
4767	- '005	'8915	4732	+ '152	'0554	'5219	- '115	'7263			
4781	+ '008	'8939	4749	+ '120	'0584	'5240	- '098	'7300	2362'4115	- '185	'6450
4798	+ '015	'8969	4770	+ '150	'0621	'5257	- '062	'7330	'4138	- '180	'6490
4902	+ '042	'9153	4787	+ '145	'0651	'5307	- '050	'7419	'4166	- '192	'6540
4919	+ '042	'9183	4805	+ '130	'0683	'5326	- '088	'7452	'4190	- '135	'6582
4954	+ '040	'9244	4843	+ '120	'0750	'5342	- '060	'7480	'4209	- '155	'6616
4968	+ '025	'9269	4871	+ '112	'0799	'5360	- '035	'7512	'4230	- '182	'6653
4982	+ '035	'9294	4885	+ '110	'0824	'5379	- '060	'7546	'4264	- '188	'6713
4996	+ '035	'9319	4902	+ '088	'0854	'5399	- '028	'7581	'4282	- '160	'6744
5006	+ '045	'9336	4923	+ '115	'0891	'5420	- '022	'7618	'4310	- '165	'6794
5020	+ '065	'9361	4944	+ '100	'0928	'5439	- '035	'7651	'4320	- '208	'6811
5038	+ '042	'9393	4978	+ '092	'0988	'5460	- '008	'7680	'4339	- '120	'6845
5058	+ '030	'9428	4999	+ '102	'1025	'5481	- '018	'7726	'4357	- '120	'6877
5076	+ '052	'9460	5020	+ '095	'1062	'5498	- '002	'7756	'4395	- '092	'6944
5090	+ '090	'9484	5041	+ '152	'1099	'5519	- '022	'7793	'4454	- '078	'7048
5107	+ '050	'9514	5069	+ '090	'1148				'4471	- '092	'7078
5121	+ '055	'9539	5086	+ '100	'1178	2361'4129	+ '080	'8833			
5138	+ '057	'9567	5103	+ '095	'1208	'4148	+ '055	'8866	2363'4176	- '600	'4199
5156	+ '052	'9601	5128	+ '120	'1252	'4166	+ '065	'8898	'4202	- '610	'4245
5196	+ '040	'9624	5145	+ '108	'1282	'4181	+ '082	'8924	'4223	- '602	'4282
5183	+ '050	'9648	5187	+ '122	'1356	'4197	+ '072	'8953	'4242	- '585	'4315
5197	+ '062	'9673	5201	+ '132	'1381	'4221	+ '048	'8995	'4263	- '568	'4353
5215	+ '037	'9705	5228	+ '120	'1429	'4238	+ '058	'9025	'4282	- '558	'4386
5239	+ '047	'9747	5246	+ '120	'1461	'4254	+ '050	'9053	'4313	- '558	'4441
5256	+ '067	'9777	5263	+ '155	'1491	'4311	+ '040	'9154	'4336	- '548	'4481
5270	+ '055	'9802	5287	+ '168	'1533	'4330	+ '068	'9187	'4358	- '528	'4520
5284	+ '062	'9827	5308	+ '140	'1570	'4350	+ '050	'9223	'4377	- '518	'4554
5301	+ '050	'9857	5326	+ '158	'1602	'4391	+ '080	'9295	'4415	- '500	'4621
5347	+ '060	'9938	5346	+ '160	'1637	'4426	+ '072	'9357	'4435	- '478	'4656
5360	+ '047	'9961	5364	+ '155	'1669	'4456	+ '082	'9410	'4457	- '500	'4695
5374	+ '062	'9985	5385	+ '190	'1706	'4471	+ '062	'9436	'4480	- '480	'4735
5392	+ '055	'0017	5409	+ '168	'1748	'4494	+ '088	'9477	'4502	- '515	'4774
5409	+ '070	'0047				'4537	+ '078	'9552	'4523	- '450	'4811
5426	+ '067	'0077	2354'4184	- '400	'5437	'4561	+ '088	'9595	'4546	- '458	'4852
5444	+ '072	'0109	'4208	- '405	'5480	'4580	+ '068	'9628	'4567	- '448	'4889
5461	+ '040	'0148	'4224	- '418	'5508	'4605	+ '068	'9672	'4619	- '445	'4981
5479	+ '070	'0171	'4245	- '378	'5545	'4626	+ '082	'9709	'4640	- '432	'5018
5496	+ '075	'0201	'4283	- '345	'5612	'4636	+ '068	'9727	'4659	- '432	'5051
5517	+ '057	'0238	'4314	- '345	'5667	'4732	+ '072	'9896	'4678	- '430	'5085
5534	+ '067	'0268	'4349	- '352	'5729	'4751	+ '042	'9930	'4695	- '418	'5115
5555	+ '087	'0305	'4373	- '358	'5771	'4775	+ '130	'9970	'4716	- '390	'5152
5579	+ '065	'0347	'4401	- '358	'5820	'4796	+ '022	'0009	'4737	- '382	'5189
			'4434	- '332	'5878	'4818	+ '050	'0048	'4752	- '390	'5215
			'4476	- '332	'5953	'4837	+ '102	'0082	'4770	- '382	'5247
2348'4027	+ '075	'9310	'4512	- '300	'6016	'4864	+ '058	'0129	'4787	- '375	'5277
4053	+ '115	'9356	'4550	- '290	'6083	'4882	+ '032	'0161			
4081	+ '102	'9405	'4571	- '300	'6120	'4956	+ '045	'0292	2364'4036	+ '148	'1594
4121	+ '105	'9476	'4592	- '278	'6157	'4982	+ '050	'0337	'4052	+ '108	'1622
4179	+ '110	'9525	'4620	- '270	'6207	'5006	+ '045	'0380	'4066	+ '110	'1647
4185	+ '095	'9589	'4646	- '208	'6252	'5028	+ '038	'0419	'4078	+ '132	'1668
4218	+ '122	'9647	'4670	- '245	'6295	'5051	+ '050	'0459	'4092	+ '165	'1693
4256	+ '122	'9714	'4703	- '240	'6353	'5070	+ '050	'0493	'4104	+ '168	'1714
4280	+ '118	'9756	'4726	- '238	'6394	'5093	+ '045	'0533	'4118	+ '142	'1738
4301	+ '128	'9793	'4752	- '238	'6439	'5114	+ '035	'0570	'4131	+ '208	'1761
4326	+ '132	'9837	'4780	- '218	'6489	'5132	+ '048	'0602	'4145	+ '195	'1786
4346	+ '135	'9873	'4839	- '202	'6593	'5150	+ '040	'0634	'4158	+ '180	'1809
4371	+ '152	'9917	'4865	- '200	'6639	'5245	+ '072	'0801	'4175	+ '128	'1839
4402	+ '148	'9972	'4884	- '205	'6672	'5266	+ '068	'0838	'4194	+ '135	'1873
4426	+ '155	'0014	'4903	- '210	'6706	'5287	+ '035	'0876	'4211	+ '182	'1903
4444	+ '142	'0046	'4924	- '172	'6743	'5306	+ '035	'0909	'4225	+ '168	'1927
4464	+ '155	'0081	'4943	- '178	'6776	'5327	+ '058	'0946	'4241	+ '130	'1955
4485	+ '135	'0118	'4986	- '118	'6852	'5350	+ '050	'0987	'4255	+ '162	'1980
4517	+ '150	'0174	'5009	- '165	'6893	'5370	+ '045	'1022	'4274	+ '168	'2014
4534	+ '145	'0204	'5030	- '162	'6930	'5391	+ '062	'1059	'4288	+ '165	'2038
4555	+ '152	'0241	'5049	- '158	'6963	'5416	+ '065	'1103	'4312	+ '145	'2081
4572	+ '138	'0271	'5116	- '118	'7082	'5436	+ '080	'1138	'4326	+ '162	'2105
46031	+ '140	'0376	'5137	- '135	'7119	'5457	+ '110	'1175	'4343	+ '125	'2135
4649	+ '165	'0407									

TABLE II (continued)

J.D. Hel. -2430000	Δm	phase	J.D. Hel. -2430000	Δm	phase	J.D. Hel. -2430000	Δm	phase	J.D. Hel. -2430000	Δm	phase
d	m	P	d	m	P	d	m	P	d	m	P
2364'4357	+130	'2160	2364'5456	-665	'4099	2379'5596	-005	'8972	2381'5068	-437	'3324
4371	+158	'2185	5475	-648	'4132				5079	-447	'3343
4388	+170	'2215	5493	-635	'4164	2380'4135	-860	'4036	5090	-460	'3363
4406	+152	'2247	5506	-635	'4187	4159	-812	'4079	5102	-492	'3384
4420	+132	'2271	5524	-625	'4219	4182	-807	'4119	5113	-495	'3403
4437	+130	'2301	5538	-620	'4244	4230	-820	'4204	5125	-530	'3425
4447	+120	'2319	5555	-610	'4274	4255	-830	'4248	5132	-582	'3437
4468	+098	'2356	5569	-588	'4298	4274	-847	'4282	5167	-600	'3499
4486	+082	'2388				4303	-810	'4333	5180	-577	'3522
4503	+065	'2418	2374'4563	-005	'8941	4380	-760	'4469	5193	-612	'3542
4520	+040	'2448	4594	-002	'8996	4399	-740	'4502	5205	-650	'3566
4543	-018	'2488	4632	+017	'9063	4507	-722	'4693	5220	-667	'3592
4552	+020	'2504	4664	+017	'9119	4519	-672	'4714	5230	-672	'3610
4559	+008	'2516	4761	-015	'9290	4572	-722	'4728	5241	-700	'3629
4564	-012	'2525	4789	-035	'9340	4541	-680	'4753	5255	-732	'3654
4576	-012	'2546	4865	-035	'9474	4555	-665	'4777	5264	-747	'3670
4586	-032	'2564	4903	-017	'9514	4632	-637	'4913	5277	-750	'3693
4595	-088	'2580	4985	-042	'9685	4651	-595	'4947	5289	-757	'3714
4604	-090	'2596	5004	-042	'9719	4666	-642	'4973	5300	-792	'3733
4614	-148	'2613	5070	-020	'9835	4689	-607	'5014	5319	-802	'3767
4625	-185	'2633	5086	-012	'9864	4711	-652	'5053	5325	-792	'3777
4635	-158	'2651	5223	-032	'0105	4864	-530	'5322	5340	-815	'3804
4645	-195	'2668	5242	-040	'0139	4888	-510	'5365	5355	-825	'3830
4658	-205	'2691	5261	-042	'0172	4902	-495	'5389	5369	-812	'3855
4668	-258	'2709	5400	-048	'0389	4928	-502	'5435	5394	-827	'3899
4677	-260	'2725	5419	-048	'0451	4941	-480	'5458	5407	-845	'3922
4685	-305	'2739	5428	-065	'0467	4956	-467	'5485	5418	-872	'3942
4696	-350	'2758				4979	-462	'5525	5430	-880	'3963
4706	-355	'2776	2376'4637	-722	'4355	5005	-432	'5571	5443	-842	'3986
4717	-395	'2795	4656	-697	'4389				5455	-852	'4007
4725	-395	'2809	4675	-695	'4422	2381'3993	+060	'1428	5469	-845	'4032
4736	-418	'2829	4693	-695	'4454	4012	+120	'1461	5481	-847	'4053
4748	-438	'2850	4710	-695	'4484	4028	+185	'1489	5500	-832	'4086
4755	-472	'2862	4734	-687	'4526	4047	+150	'1523	5515	-830	'4113
4763	-468	'2876	4752	-672	'4558	4128	+160	'1666	5602	-772	'4266
4772	-502	'2892	4772	-665	'4593	4151	+170	'1706	5633	-782	'4321
4781	-518	'2908	4790	-662	'4625	4168	+180	'1736	5646	-790	'4344
4791	-530	'2926	4877	-602	'4778	4184	+195	'1765	5691	-768	'4423
4800	-560	'2942	4894	-585	'4808	4283	+187	'1939	5701	-752	'4441
4809	-580	'2957	4918	-617	'4851	4302	+220	'1973	5718	-732	'4471
4817	-580	'2972	4939	-605	'4888	4332	+197	'2026	5734	-720	'4499
4826	-585	'2987	4962	-595	'4928	4342	+207	'2043	5750	-732	'4527
4835	-612	'3003	4984	-565	'4967	4439	+202	'2214	5773	-720	'4568
4847	-622	'3025	5081	-567	'5138	4462	+195	'2255	5788	-687	'4594
4859	-635	'3046	5102	-505	'5175	4483	+192	'2292	5804	-697	'4623
4871	-655	'3067	5123	-510	'5212	4510	+220	'2340			
4878	-660	'3079	5144	-510	'5249	4618	+140	'2530	2382'4114	+075	'9283
4890	-682	'3100	5165	-497	'5286	4641	+142	'2571	4135	+067	'9320
4916	-718	'3146	5184	-547	'5320	4660	+142	'2604	4157	+082	'9359
4930	-720	'3171				4679	+087	'2638	4180	+092	'9399
4944	-740	'3196	2379'4294	-265	'6675	4746	+008	'2756	4230	+095	'9487
4951	-750	'3208	4320	-245	'6721	4753	-005	'2768	4251	+102	'9524
4965	-752	'3233	4337	-237	'6751	4788	-142	'2830	4270	+087	'9558
4975	-775	'3250	4355	-235	'6783	4800	-130	'2851	4291	+050	'9595
4986	-788	'3270	4431	-240	'6917	4836	-170	'2915	4347	+102	'9694
4996	-788	'3287	5058	-080	'8023	4847	-205	'2934	4367	+092	'9729
5010	-778	'3312	5075	-065	'8953	4889	-267	'3008	4378	+107	'9749
5020	-708	'3330	5101	-082	'8099	4908	-267	'3042	4406	+110	'9798
5036	-788	'3358	5120	-082	'8132	4921	-287	'3065	4529	+090	'0015
5286	-735	'3799	5221	-030	'8311	4926	-295	'3074	4548	+095	'0048
5298	-735	'3820	5242	-007	'8348	4940	-335	'3098	4567	+130	'0082
5312	-715	'3845	5263	-027	'8385	4953	-327	'3121	4588	+105	'0119
5331	-710	'3878	5280	-017	'8415	4964	-352	'3141	4661	+117	'0248
5343	-670	'3900	5376	-012	'8584	4977	-352	'3164	4678	+122	'0278
5359	-672	'3928	5393	-015	'8614	4991	-357	'3188	4699	+122	'0315
5373	-680	'3952	5416	-002	'8655	5005	-390	'3213	4716	+112	'0345
5388	-678	'3979	5433	-005	'8685	5027	-395	'3252	4767	+135	'0435
5406	-682	'4011	5547	-017	'8886	5032	-407	'3261	4779	+100	'0456
5428	-650	'4050	5561	-025	'8910	5046	-387	'3285	4791	+110	'0477
5444	-658	'4078	5577	-020	'8939	5057	-412	'3305	4808	+142	'0507

TABLE II (continued)

J.D. Hel. -2430000	Δm	phase	J.D. Hel. -2430000	Δm	phase	J.D. Hel. -2430000	Δm	phase	J.D. Hel. -2430000	Δm	phase
2382 ^d 4850	+102	P	2385 ^d 4784	-612	P	2386 ^d 5064	+137	P	2389 ^d 4683	-950	P
4861	+095	'0581	4794	-658	'3390	5144	+185	'1526	4701	-952	'3779
4874	+140	'0624	4812	-665	'3408	5168	+167	'1667	4720	-952	'3811
4888	+100	'0648	4815	-680	'3439	5245	+180	'1709			'3844
4942	+122	'0744	4826	-700	'3445	5272	+180	'1845	2391 ^d 4194	+058	'8200
4956	+132	'0768	4839	-732	'3464	5307	+225	'1893	4219	+078	'8244
4972	+105	'0796	4850	-748	'3487	5335	+195	'1954	4248	+125	'8295
4984	+075	'0818	4860	-778	'3506	5408	+225	'2004	4284	+060	'8358
4998	+110	'0842	4872	-782	'3524	5432	+220	'2133	4306	+080	'8397
5017	+127	'0827	4885	-785	'3545	5460	+215	'2175	4324	+080	'8429
5036	+100	'0909	4895	-802	'3568	5481	+217	'2224	4342	+075	'8461
5051	+112	'0906	4907	-808	'3586	5529	+272	'2261	4363	+002	'8498
5097	+100	'1017	4918	-820	'3607	5550	+202	'2364	4380	+072	'8528
5121	+102	'1059	4928	-832	'3626	5571	+185	'2383	4395	+080	'8554
5137	+135	'1088	4942	-860	'3644	5620	+190	'2420	4412	+095	'8584
5152	+092	'1114	4952	-865	'3669	5634	+172	'2507	4452	+102	'8655
5225	+145	'1243	4963	-852	'3686	5654	+150	'2531	4468	+088	'8683
5239	+170	'1268	4982	-865	'3706	5668	+122	'2567	4482	+102	'8708
5249	+105	'1285	4992	-882	'3739	5689	+102	'2591	4498	+095	'8736
5269	+142	'1320	5004	-878	'3757	5710	+130	'2628	4518	+090	'8771
5315	+140	'1402	5017	-870	'3778	5731	+070	'2665	4539	+125	'8808
5322	+127	'1414	5032	-892	'3801	5752	+058	'2702	4555	+092	'8837
5333	+157	'1433	5046	-880	'3828	5776	+030	'2740	4573	+130	'8868
5345	+167	'1455	5065	-872	'3852	5793	+007	'2782	4602	+105	'8951
5364	+180	'1488	5076	-885	'3886	5811	+038	'2812	4638	+098	'8983
5374	+160	'1506	5088	-882	'3905	5832	-070	'2844	4658	+110	'9018
			5107	-855	'3926			'2881	4677	+115	'9052
			5121	-868	'3960	2389 ^d 3824	+207	'2263	4700	+112	'9092
2385 ^d 3961	+138	'1938	5131	-868	'3985	3841	+215	'2293	4775	+118	'9225
3985	+218	'1980	5140	-872	'4002	3860	+182	'2327	4793	+122	'9256
4449	-008	'2799	5152	-862	'4018	3897	+170	'2392	4809	+120	'9285
4473	-040	'2841	5164	-860	'4039	3916	+182	'2426	4826	+138	'9315
4491	-080	'2873	5176	-848	'4060	3940	+195	'2468	4844	+135	'9346
4517	-090	'2919	5187	-832	'4082	3973	+167	'2526	4861	+122	'9376
4522	-118	'2928	5199	-842	'4101	3973	+092	'2579	4880	+145	'9410
4523	-118	'2930	5209	-832	'4122	4003	+055	'2630	4939	+118	'9514
4525	-142	'2933	5234	-822	'4140	4032	+012	'2724	4957	+128	'9546
4527	-152	'2937	5249	-820	'4184	4085	-015	'2747	4975	+140	'9577
4529	-186	'2940	5261	-802	'4210	4098	-035	'2761	4999	+135	'9620
4534	-162	'2949	5272	-810	'4222	4106	-098	'2796	5018	+132	'9653
4536	-182	'2953	5286	-788	'4251	4126	-130	'2812	5034	+125	'9682
4537	-188	'2954	5301	-772	'4276	4135	-182	'2844	5050	+130	'9710
4546	-248	'2970	5313	-768	'4302	4153	-220	'2884	5082	+145	'9766
4548	-270	'2974	5324	-765	'4323	4176	-257	'2909	5099	+135	'9796
4550	-280	'2977	5338	-762	'4343	4190	-310	'2936	5114	+148	'9823
4551	-305	'2979	5346	-762	'4382	4219	-332	'2960	5135	+138	'9860
4567	-312	'3007	5359	-762	'4404	4233	-382	'2985	5152	+154	'9890
4569	-322	'3011	5364	-750	'4413	4257	-417	'3027	5216	+150	'0003
4576	-315	'3023	5374	-740	'4431	4260	-447	'3033	5239	+122	'0043
4584	-342	'3037	5385	-712	'4450	4282	-482	'3071	5255	+122	'0071
4596	-352	'3058	5412	-715	'4498	4314	-515	'3128	5299	+148	'0149
4614	-372	'3090	5428	-755	'4526	4328	-542	'3151	5317	+118	'0181
4629	-370	'3117	5433	-708	'4535	4340	-565	'3174	5334	+132	'0211
4631	-410	'3120	5445	-705	'4556	4363	-615	'3214	5350	+128	'0239
4643	-410	'3141	5456	-695	'4576	4382	-637	'3248	5365	+128	'0265
4645	-418	'3145	5466	-680	'4593	4395	-665	'3271	5382	+135	'0295
4647	-405	'3148	5484	-688	'4625	4415	-690	'3306	5413	+142	'0350
4648	-420	'3150	5496	-672	'4646	4439	-710	'3348	5428	+140	'0377
4652	-430	'3157	5506	-670	'4664	4449	-762	'3366	5441	+145	'0400
4662	-438	'3175	5517	-652	'4683	4477	-805	'3415	5456	+128	'0426
4671	-445	'3191	5529	-638	'4704	4490	-842	'3438	5472	+128	'0454
4683	-450	'3212	5541	-645	'4726	4506	-870	'3467	5486	+118	'0479
4692	-450	'3228	5551	-645	'4743	4525	-877	'3500	5500	+130	'0504
4713	-488	'3265	5563	-630	'4764	4545	-900	'3535			
4716	-498	'3270				4562	-912	'3565	2394 ^d 4026	+020	'0828
4716	-498	'3270				4581	-930	'3599	4040	+090	'0853
4725	-500	'3286	2386 ^d 4835	+122	'1122	4602	-952	'3636	4054	+070	'0878
4735	-538	'3304	4859	+142	'1164	4623	-960	'3673	4070	+058	'0906
4747	-538	'3325	4887	+132	'1213	4640	-927	'3703	4094	+062	'0948
4760	-580	'3348	4915	+155	'1263	4660	-962	'3738	4111	+075	'0978
4765	-592	'3357	5002	+152	'1416						
4773	-608	'3371									

TABLE II (continued)

J.D. Hel. -2430000	Δm	phase	J.D. Hel. -2430000	Δm	phase	J.D. Hel. -2430000	Δm	phase	J.D. Hel. -2430000	Δm	phase
2394 ^d 4126	+082	P1005	2394 ^d 5290	-652	P3058	2398 ^d 3976	+075	P1307	2398 ^d 5082	-872	P3258
4139	+072	1028	5303	-680	3081	3993	+080	1337	5096	-900	3283
4154	+080	1054	5314	-712	3101	4011	+097	1369	5112	-882	3311
4175	+077	1091	5325	-750	3120	4030	+092	1403	5126	-888	3336
4191	+090	1120	5338	-767	3143	4051	+105	1440	5139	-885	3359
4205	+067	1144	5349	-790	3162	4067	+115	1468	5155	-888	3387
4220	+082	1171	5363	-820	3187	4085	+115	1500	5169	-888	3412
4236	+095	1199	5375	-840	3208	4101	+127	1528	5182	-897	3435
4251	+072	1225	5389	-865	3233	4118	+130	1558	5207	-897	3479
4385	+117	1462	5402	-885	3256	4138	+125	1593	5223	-900	3507
4401	+112	1490	5416	-907	3281	4160	+132	1632	5239	-878	3535
4418	+132	1520	5430	-917	3305	4186	+122	1678	5253	-882	3560
4436	+110	1552	5443	-940	3328	4219	+152	1736	5268	-860	3587
4456	+125	1587	5458	-947	3355	4236	+145	1766	5282	-860	3611
4470	+147	1612	5472	-955	3379	4252	+150	1794	5297	-832	3638
4489	+142	1645	5484	-972	3401	4271	+167	1828	5315	-840	3669
4504	+140	1672	5498	-977	3425	4345	+175	1958	5330	-840	3696
4516	+145	1693	5513	-975	3452	4353	+190	1972	5354	-830	3738
4528	+157	1714	5526	-985	3475	4369	+160	2001	5369	-817	3765
4550	+172	1753	5540	-982	3499	4386	+162	2030	5384	-807	3791
4565	+165	1779	5552	-982	3521	4397	+180	2049	5408	-788	3834
4582	+177	1809	5566	-990	3545	4421	+172	2092	5422	-795	3858
4597	+162	1836	5582	-982	3574	4437	+197	2121	5430	-785	3872
4617	+175	1871	5595	-980	3596	4446	+160	2136	5447	-765	3902
4630	+185	1894	5608	-972	3619	4468	+155	2175			
4645	+182	1921	5624	-960	3648	4484	+162	2203	2401 ^d 4641	-370	5406
4664	+177	1954	5637	-957	3671	4499	+142	2230	4672	-347	5460
4688	+190	1996	5650	-952	3694	4520	+150	2267	4683	-327	5480
4710	+190	2035	5664	-947	3718	4536	+142	2295	4648	-322	5506
4728	+207	2067	5678	-945	3743	4553	+115	2325	4712	-325	5531
4744	+210	2095	5693	-927	3769	4568	+100	2352	4724	-310	5552
4759	+210	2122	5707	-912	3794	4583	+110	2378	4753	-295	5603
4779	+210	2157	5727	-897	3829	4596	+088	2401	4767	-310	5628
4796	+192	2187	5741	-905	3854	4610	+080	2426	4782	-295	5654
4821	+205	2231	5756	-890	3881	4624	+062	2450	4841	-272	5759
4838	+205	2261	5771	-875	3907	4640	+042	2479	4856	-292	5785
4854	+177	2289	5788	-867	3937	4653	+017	2502	4871	-275	5811
4873	+192	2323	5812	-842	3979	4666	+002	2525			
4889	+187	2351	5826	-832	4004	4679	-062	2547	2406 ^d 3653	+172	1871
4903	+182	2376	5846	-822	4039	4694	-092	2574	3674	+157	1908
4917	+187	2400				4706	-137	2595	3695	+152	1945
4931	+162	2425	2397 ^d 3939	-885	3600	4719	-162	2618	3719	+170	1988
4947	+122	2453	3962	-890	3641	4730	-195	2637	3740	+135	2025
4960	+132	2476	3982	-870	3676	4740	-240	2655	3764	+150	2067
4974	+132	2501	4008	-857	3722	4752	-262	2676	3788	+147	2110
4986	+122	2522	4033	-845	3766	4763	-297	2696	3809	+120	2147
5007	+097	2559	4067	-842	3826	4776	-350	2719	3829	+117	2182
5020	+085	2582	4315	-685	4264	4788	-380	2739	3842	+120	2205
5033	+060	2605	4344	-665	4315	4800	-415	2761	3855	+112	2228
5045	+040	2628	4373	-655	4366	4812	-460	2782	3868	+105	2251
5058	+015	2649	4401	-645	4415	4826	-488	2807	3886	+062	2282
5070	+007	2670	4420	-610	4449	4838	-537	2828	3909	+045	2323
5085	-052	2697	4444	-610	4491	4851	-560	2851	3918	+042	2339
5096	-075	2716	4467	-580	4532	4862	-590	2870	3931	+022	2362
5108	-110	2737	4486	-570	4565	4874	-615	2891	3944	+020	2385
5118	-135	2755	4512	-570	4611	4885	-657	2911	3959	-022	2411
5130	-160	2776	4548	-542	4674	4898	-675	2934	3973	-048	2436
5139	-215	2792	4571	-535	4715	4912	-705	2958	3983	-075	2454
5152	-247	2815	4595	-530	4758	4923	-712	2978	3994	-097	2473
5163	-265	2834				4937	-738	3003	4013	-110	2507
5174	-317	2854	2398 ^d 3773	+065	0949	4950	-765	3026	4018	-145	2515
5185	-360	2873	3798	+062	0993	4962	-782	3047	4033	-170	2542
5197	-392	2894	3825	+090	1041	4974	-775	3068	4047	-215	2566
5207	-420	2912	3849	+065	1083	4987	-795	3091	4059	-232	2588
5219	-490	2933	3874	+065	1127	5003	-825	3119	4073	-260	2612
5231	-505	2954	3898	+047	1170	5016	-837	3142	4086	-277	2635
5243	-535	2975	3915	+092	1200	5029	-852	3165	4098	-302	2656
5254	-575	2995	3930	+087	1226	5042	-860	3188	4110	-345	2678
5266	-602	3016	3945	+087	1253	5057	-862	3214	4123	-367	2700
5279	-635	3039	3960	+097	1279	5070	-862	3237	4138	-415	2727

TABLE II (continued)

J.D. Hel. -2430000	Δm	phase	J.D. Hel. -2430000	Δm	phase	J.D. Hel. -2430000	Δm	phase	J.D. Hel. -2430000	Δm	phase
d	m	P	d	m	P	d	m	P	d	m	P
2406'4151	-445	'2750	2409'4356	-225	'6037	2410'4071	-527	'3176	2414'4356	-562	'4246
'4166	-460	'2776	'4371	-237	'6063	'4084	-525	'3199	'4380	-567	'4288
'4183	-490	'2806	'4396	-240	'6107	'4102	-560	'3230	'4456	-557	'4422
'4198	-522	'2833	'4409	-235	'6130	'4120	-567	'3262	'4474	-557	'4454
'4214	-542	'2861	'4426	-210	'6160	'4134	-552	'3287	'4510	-535	'4517
'4228	-555	'2886	'4440	-210	'6185	'4148	-580	'3312	'4531	-550	'4554
'4242	-562	'2910	'4459	-225	'6219	'4162	-585	'3336	'4557	-540	'4600
'4256	-588	'2935	'4483	-185	'6261	'4175	-585	'3359	'4574	-547	'4630
'4273	-595	'2965	'4499	-207	'6289	'4201	-595	'3405	'4602	-545	'4680
'4292	-627	'2999	'4513	-205	'6314	'4215	-595	'3430	'4626	-512	'4722
'4305	-660	'3022	'4529	-212	'6342	'4235	-605	'3465	'4647	-500	'4759
'4316	-645	'3041	'4542	-202	'6365	'4251	-620	'3493			
'4330	-655	'3066	'4557	-200	'6394	'4269	-617	'3525	2415'4088	+117	'1415
'4343	-682	'3089	'4574	-195	'6421	'4284	-625	'3552	'4102	+120	'1439
'4356	-682	'3112	'4589	-190	'6448	'4299	-622	'3578	'4120	+115	'1471
'4369	-692	'3134	'4609	-180	'6483	'4313	-625	'3603	'4150	+125	'1524
'4383	-712	'3159	'4624	-187	'6510	'4326	-625	'3606	'4168	+140	'1556
'4405	-717	'3198	'4638	-172	'6534	'4340	-617	'3650	'4185	+160	'1586
'4418	-732	'3221	'5273	-052	'7655	'4359	-625	'3684	'4209	+160	'1628
'4432	-745	'3246	'5288	-060	'7681	'4374	-632	'3710	'4226	+165	'1658
'4445	-732	'3269	'5302	-062	'7706	'4388	-630	'3735	'4243	+170	'1688
'4460	-757	'3295	'5317	-040	'7732	'4399	-612	'3754	'4259	+155	'1716
'4476	-740	'3323	'5335	-037	'7764	'4413	-607	'3779	'4277	+150	'1747
'4491	-747	'3350	'5353	-037	'7796	'4428	-602	'3806	'4296	+180	'1781
'4505	-752	'3374	'5366	-052	'7819	'4441	-612	'3829	'4316	+182	'1817
'4519	-732	'3399	'5380	-040	'7843	'4457	-615	'3857	'4329	+202	'1840
'4535	-750	'3427	'5395	-030	'7870	'4474	-597	'3887	'4350	+180	'1877
'4549	-755	'3452	'5417	-020	'7909	'4505	-600	'3941	'4363	+172	'1900
'4564	-752	'3479	'5430	-035	'7932	'4523	-592	'3973	'4377	+180	'1924
'4586	-747	'3517	'5446	-027	'7960	'4610	-567	'4127	'4395	+180	'1956
'4605	-732	'3551	'5460	-035	'7984	'4627	-577	'4157	'4411	+162	'1984
'4618	-722	'3574	'5474	-005	'8009	'4642	-562	'4183	'4426	+170	'2011
'4634	-732	'3602	'5494	-038	'8044	'4657	-562	'4210	'4440	+185	'2036
'4655	-725	'3639	'5521	-030	'8092	'4673	-555	'4238	'4455	+175	'2062
'4670	-692	'3666	'5534	-027	'8115	'4691	-555	'4270	'4472	+180	'2092
'4688	-700	'3697	'5556	-038	'8154	'4707	-545	'4298	'4509	+190	'2157
'4702	-705	'3722	'5571	-002	'8180	'4723	-542	'4326	'4524	+180	'2184
'4719	-687	'3752	'5587	-015	'8209	'4738	-552	'4353	'4539	+180	'2210
'4736	-692	'3782	'5598:	-018	'8228	'4751	-537	'4375	'4555	+170	'2258
'4753	-667	'3812				'4764	-540	'4398	'4572	+165	'2268
'4772	-670	'3846	2410'3618	+052	'2377	'4778	-530	'4423	'4590	+170	'2300
'4794	-677	'3884	'3641	+008	'2417	'4791	-517	'4446	'4607	+137	'2330
'4808	-657	'3909	'3661	-035	'2452	'4804	-535	'4469	'4621	+122	'2335
'4827	-637	'3942	'3682	-072	'2490	'4819	-525	'4495	'4635	+105	'2380
			'3700	-067	'2521	'4834	-517	'4522	'4652	+102	'2410
2408'4869	+012	'9300	'3715	-120	'2548	'4847	-515	'4545	'4666	+050	'2434
'4894	+003	'9344	'3727	-137	'2569	'4862	-495	'4571	'4681	+045	'2461
'4915	+017	'9381	'3741	-137	'2594	'4878	-497	'4599	'4694	+062	'2484
'4948	+007	'9439	'3753	-165	'2615	'4892	-495	'4624	'4715	+015	'2521
'4967	+037	'9473	'3766	-172	'2638	'4905	-480	'4647	'4726	+020	'2540
'4987	+005	'9508	'3779	-217	'2661				'4736	+038	'2558
'5000	+010	'9531	'3795	-262	'2689	2414'3873	-540	'3393	'4749	-025	'2581
'5046	+012	'9612	'3807	-260	'2710	'3892	-510	'3427	'4760	-030	'2600
'5063	+032	'9642	'3819	-285	'2731	'3913	-512	'3464	'4771	-055	'2619
'5089	+035	'9688	'3833	-315	'2756	'3935	-545	'3503	'4784	-050	'2642
'5106	+010	'9718	'3845	-335	'2777	'3956	-555	'3540	'4799	-080	'2669
'5120	+002	'9743	'3857	-352	'2798	'3981	-542	'3584	'4813	-122	'2694
'5139	+005	'9776	'3870	-375	'2821	'4043	-585	'3693	'4828	-125	'2720
'5154	+020	'9803	'3888	-415	'2853	'4066	-590	'3734	'4840	-157	'2741
'5228	+020	'9933	'3901	-427	'2876	'4185	-580	'3767	'4854	-205	'2765
'5246	+032	'9965	'3915	-437	'2901	'4113	-572	'3817	'4870	-242	'2794
			'3929	-465	'2925	'4137	-595	'3859	'4883	-270	'2817
2409'4173	-297	'5714	'3947	-465	'2957	'4157	-597	'3895	'4896	-297	'2840
'4197	-310	'5746	'3965	-502	'2989	'4190	-577	'3953	'4908	-322	'2861
'4220	-282	'5797	'3980	-495	'3015	'4217	-595	'4000	'4923	-330	'2888
'4240	-277	'5832	'3995	-497	'3042	'4240	-607	'4040	'4934	-390	'2907
'4264	-257	'5875	'4014	-510	'3075	'4267	-585	'4089	'4952	-382	'2939
'4296	-260	'5931	'4028	-515	'3100	'4287	-587	'4124	'4960	-387	'2953
'4310	-252	'5956	'4041	-522	'3123	'4305	-580	'4156	'4973	-387	'2976
'4328	-245	'5987	'4055	-537	'3148	'4335	-572	'4209	'4986	-397	'2999

TABLE II (continued)

J.D. Hel. -2430000	Δm	phase	J.D. Hel. -2430000	Δm	phase	J.D. Hel. -2430000	Δm	phase	J.D. Hel. -2430000	Δm	phase
d	m	P	d	m	P	d	m	P	d	m	P
2415 ^d 5002	-422	3027	2418 ^d 4652	-475	5335	2419 ^d 4901	-352	3416	2423 ^d 3477	+122	1471
5018	-410	3055	4707	-450	5432	4918	-382	3446	3493	+130	1499
5032	-415	3080	4730	-445	5472	4931	-422	3469	3508	+130	1525
5046	-410	3105	4747	-437	5502	4945	-407	3493	3527	+142	1559
5065	-447	3138	4779	-432	5559	4969	-430	3536	3541	+142	1583
5087	-425	3177	4799	-425	5594	4982	-472	3559	3560	+170	1617
5099	-430	3198	4826	-425	5642	4994	-447	3580	3587	+182	1665
5113	-440	3223	4848	-422	5681	5006	-452	3601	3604	+157	1695
5128	-447	3249	4879	-395	5735	5018	-480	3622	3728	+200	1913
5145	-467	3279	4902	-382	5776	5030	-497	3643	3747	+190	1947
5160	-452	3306	4924	-377	5815	5046	-515	3672	3768	+200	1984
5173	-465	3329	4942	-377	5846	5059	-525	3695	3784	+192	2012
5188	-460	3355	4966	-365	5889	5074	-532	3721	3798	+197	2037
5200	-475	3376	4983	-375	5919	5089	-537	3747	3813	+187	2063
5206	-480	3387	5004	-350	5956	5113	-560	3790	3828	+207	2090
5228	-490	3426	5077	-322	6085	5127	-572	3814	3845	+202	2120
5244	-515	3454	5096	-330	6118	5143	-600	3843	3862	+232	2150
5261	-520	3484	5117	-327	6155	5158	-580	3869	3878	+205	2178
5279	-520	3516				5172	-592	3894	3892	+225	2203
5294	-525	3542	2419 ^d 3915	+220	1676	5187	-622	3920	3910	+215	2234
5311	-547	3572	3957	+060	1750	5196	-622	3936	3930	+200	2270
5325	-555	3597	3981	+170	1793	5221	-627	3980	3948	+220	2301
5339	-575	3622	4009	+185	1842	5234	-647	4003	3966	+215	2333
5353	-555	3646	4050	+157	1914	5332	-630	4176	3983	+210	2363
5366	-560	3669	4068	+210	1946	5342	-652	4194	3998	+177	2390
5384	-557	3701	4092	+202	1989	5354	-675	4215	4011	+197	2413
5400	-550	3729	4120	+190	2038	5370	-645	4243	4053	+187	2487
5412	-565	3750	4138	+175	2070				4077	+142	2529
5425	-570	3773	4193	+072	2167	2420 ^d 4075	+045	9600	4090	+155	2552
			4234	+180	2239	4089	+055	9625	4101	+135	2571
2418 ^d 3830	-555	3885	4250	+175	2267	4103	+052	9650	4119	+125	2603
3850	-610	3920	4266	+185	2296	4117	+057	9674	4133	+107	2628
3869	-600	3953	4287	+165	2333	4134	+070	9704	4137	+087	2635
3884	-610	3980	4311	+165	2375	4151	+067	9734	4149	+087	2656
3891	-632	3992	4328	+150	2405	4198	+057	9817	4160	+060	2676
3915	-640	4035	4352	+157	2447	4214	+065	9846	4170	+065	2693
3932	-632	4065	4368	+135	2475	4230	+075	9874	4184	+055	2718
3945	-630	4087	4384	+132	2504	4243	+062	9897	4195	+055	2737
3960	-645	4114	4405	+085	2541	4259	+060	9925	4204	+035	2753
3972	-645	4135	4420	+067	2567	4276	+060	9955	4215	+022	2773
3990	-647	4167	4434	+060	2592	4318	+097	0029	4226	+005	2792
4004	-640	4192	4445	+067	2611	4330	+085	0050	4239	-020	2815
4025	-650	4229	4458	+010	2634	4346	+065	0078	4255	-042	2843
4037	-637	4250	4471	+008	2657	4360	+072	0103	4265	-047	2861
4051	-642	4274	4494	+002	2698	4374	+080	0128	4274	-060	2877
4068	-640	4304	4502	000	2712	4387	+087	0151	4287	-097	2900
4082	-620	4329	4515	-028	2735	4401	+080	0175	4298	-110	2919
4096	-632	4354	4529	-055	2760	4417	+100	0204	4311	-140	2942
4111	-625	4380	4546	-085	2789	4431	+095	0228	4324	-167	2965
4123	-635	4402	4569	-132	2830	4446	+102	0255	4337	-172	2988
4137	-625	4426	4587	-182	2862	4551	+102	0440	4349	-187	3009
4164	-630	4474	4604	-195	2892	4572	+095	0477	4361	-222	3030
4182	-625	4506	4623	-227	2925	4599	+085	0525	4373	-255	3051
4204	-612	4544	4641	-292	2957	4634	+085	0586	4387	-260	3076
4223	-610	4578	4655	-295	2982	4655	+060	0624	4400	-275	3099
4251	-605	4627	4670	-282	3008	4683	+065	0673	4415	-305	3125
4272	-602	4664	4690	-310	3044	4710	+047	0721	4426	-295	3145
4299	-590	4712	4705	-327	3070	4728	+067	0752	4439	-295	3168
4317	-587	4744	4721	-327	3098	4749	+065	0789	4452	-290	3191
4338	-587	4781	4734	-322	3121	4766	+040	0819	4464	-330	3212
4442	-547	4964	4752	-340	3153	4783	+062	0849	4478	-325	3237
4458	-537	4992	4769	-352	3183	4818	+080	0911	4491	-335	3259
4480	-537	5031	4790	-335	3220	4839	+070	0948	4505	-340	3284
4503	-525	5072	4807	-330	3250	4860	+070	0985	4522	-365	3314
4531	-512	5121	4824	-335	3280	4887	+075	1033	4535	-382	3337
4549	-505	5153	4838	-357	3305	4901	+075	1058	4548	-395	3360
4570	-500	5190	4849	-365	3324	4933	+090	1114	4560	-400	3381
4588	-490	5222	4861	-355	3345	4953	+100	1149	4576	-420	3409
4608	-492	5257	4872	-392	3365	4978	+095	1193	4600	-415	3452
4633	-485	5301	4886	-392	3389	5026	+094	1278	4611	-437	3471

TABLE II (continued)

J.D. Hel. -2430000	Δm	phase	J.D. Hel. -2430000	Δm	phase	J.D. Hel. -2430000	Δm	phase	J.D. Hel. -2430000	Δm	phase
d 2423'4623	m -450	P '3492	d 2424'6005	m -537	P '3572	d 2427'4402	m -762	P '3669	d 2432'4927	m -070	P '2804
'4634	-455	'3512	'6018	-567	'3595	'4413	-760	'3689	'4942	-085	'2831
'4646	-457	'3533	'6032	-600	'3620	'4425	-785	'3710	'4956	-125	'2855
'4656	-470	'3551	'6048	-615	'3648	'4436	-800	'3729	'4982	-160	'2901
'4669	-492	'3573	'6061	-620	'3671	'4447	-817	'3749	'4989	-192	'2914
'4682	-510	'3596	'6075	-652	'3696	'4463	-822	'3777	'5011	-262	'2953
'4693	-532	'3616	'6091	-692	'3724	'4475	-845	'3798	'5025	-310	'2977
'4703	-547	'3639	'6103	-705	'3745	'4488	-845	'3821	'5037	-325	'2998
'4719	-555	'3662	'6117	-697	'3770	'4499	-865	'3841	'5049	-397	'3020
'4730	-587	'3681	'6130	-707	'3793	'4513	-870	'3865	'5066	-390	'3050
'4743	-582	'3704	'6143	-732	'3816	'4524	-887	'3885	'5091	-405	'3094
'4754	-602	'3723	'6158	-745	'3842	'4537	-875	'3908	'5102	-462	'3113
'4769	-650	'3750	'6174	-765	'3870	'4550	-860	'3931	'5117	-505	'3140
'4793	-672	'3792	'6187	-765	'3893	'4561	-862	'3950	'5140	-542	'3180
'4805	-660	'3813	'6201	-780	'3918	'4572	-870	'3969	'5160	-610	'3215
			'6213	-782	'3939	'4584	-875	'3990	'5169	-617	'3231
2424'5222	+135	'2191	'6225	-787	'3960	'4595	-870	'4010	'5183	-645	'3256
'5245	+195	'2231	'6245	-785	'3996	'4607	-870	'4031	'5197	-687	'3281
'5261	+207	'2260	'6257	-782	'4017	'4618	-865	'4050	'5212	-730	'3307
'5279	+202	'2291				'4631	-857	'4073	'5246	-820	'3367
'5292	+190	'2314	2426'3395	-820	'4251	'4642	-862	'4093	'5259	-830	'3390
'5305	+180	'2337	'3418	-802	'4292	'4660	-842	'4125	'5272	-850	'3413
'5346	+195	'2410	'3442	-807	'4334	'4664	-845	'4132	'5286	-900	'3438
'5367	+170	'2447	'3471	-780	'4385	'4677	-840	'4155	'5299	-897	'3461
'5381	+160	'2471	'3493	-770	'4424	'4689	-822	'4176	'5312	-917	'3484
'5398	+140	'2501	'3522	-755	'4475	'4699	-815	'4193	'5327	-925	'3510
'5418	+175	'2537	'3552	-742	'4528	'4713	-817	'4218	'5341	-900	'3535
'5424	+150	'2547	'3574	-735	'4567	'4724	-812	'4237	'5355	-952	'3559
'5438	+122	'2572	'3595	-720	'4604	'4736	-832	'4259	'5385	-955	'3612
'5467	+105	'2623	'4143	-455	'5571	'4751	-815	'4285	'5398	-957	'3635
'5481	+100	'2648	'4165	-435	'5610	'4762	-827	'4305	'5405	-990	'3648
'5495	+080	'2672	'4187	-440	'5648	'4775	-820	'4327	'5427	-957	'3686
'5499	+082	'2679	'4211	-420	'5691	'4790	-790	'4354	'5441	-952	'3711
'5511	+065	'2701	'4235	-430	'5733	'4808	-797	'4386	'5453	-950	'3732
'5522	+052	'2720	'4256	-402	'5770	'4821	-765	'4409	'5468	-962	'3759
'5534	+052	'2741							'5483	-925	'3785
'5548	+045	'2766	2427'3952	-065	'2876	2431'3450	+137	'2557	'5497	-935	'3810
'5559	+022	'2785	'3965	-085	'2898	'3467	+122	'2587	'5511	-935	'3835
'5572	+002	'2808	'3980	-130	'2925	'3488	+105	'2624	'5525	-925	'3850
'5584	-032	'2829	'3997	-152	'2955	'3506	+075	'2656	'5539	-912	'3884
'5595	-048	'2849	'4009	-150	'2976	'3530	+062	'2698	'5599	-807	'3990
'5607	-077	'2870	'4024	-180	'3003	'3554	+055	'2740	'5612	-855	'4013
'5620	-080	'2893	'4056	-250	'3059	'3572	-010	'2772	'5625	-860	'4036
'5637	-135	'2923	'4068	-260	'3080	'3591	-042	'2806	'5638	-832	'4059
'5653	-152	'2951	'4082	-260	'3105	'3613	-092	'2844	'5651	-802	'4082
'5667	-195	'2976	'4093	-260	'3124	'3629	-125	'2873	'5664	-845	'4105
'5681	-235	'3001	'4108	-292	'3151	'3644	-145	'2899			
'5695	-255	'3025	'4119	-325	'3170	'3657	-185	'2922	2433'3422	-047	'7791
'5709	-282	'3050	'4130	-312	'3190	'3672	-207	'2949	'3446	-002	'7833
'5723	-282	'3075	'4142	-325	'3211	'3684	-240	'2970	'3467	+007	'7870
'5736	-315	'3098	'4155	-365	'3234	'3697	-265	'2993	'3488	+005	'7907
'5749	-320	'3121	'4169	-377	'3258	'3708	-305	'3012	'3505	+022	'7937
'5764	-312	'3147	'4182	-400	'3281	'3721	-322	'3035	'3523	+022	'7969
'5778	-330	'3172	'4194	-410	'3302	'3732	-347	'3054	'3540	+017	'7999
'5795	-335	'3202	'4205	-415	'3322	'3743	-365	'3074	'3561	+027	'8036
'5811	-337	'3230	'4217	-455	'3343	'3755	-392	'3095	'3582	+042	'8073
'5823	-362	'3251	'4229	-465	'3364	'3766	-420	'3114	'3603	+045	'8110
'5837	-352	'3276	'4241	-475	'3385	'3786	-455	'3150	'3620	+042	'8140
'5850	-387	'3299	'4253	-480	'3407	'3797	-492	'3169	'3641	+052	'8177
'5865	-362	'3325	'4258	-495	'3415	'3809	-495	'3190	'3662	+047	'8214
'5878	-370	'3348	'4278	-532	'3451	'3820	-530	'3210	'3682	+042	'8250
'5890	-392	'3369	'4294	-565	'3479	'3831	-550	'3229	'3703	+078	'8287
'5903	-425	'3392	'4306	-592	'3500	'3841	-565	'3247			
'5915	-407	'3412	'4315	-615	'3516	'3856	-605	'3273	2440'3365	+062	'1183
'5928	-437	'3436	'4328	-640	'3539				'3380	+042	'1209
'5941	-460	'3459	'4340	-665	'3560	2432'4848	+080	'2665	'3398	+018	'1241
'5953	-462	'3480	'4352	-662	'3581	'4865	+040	'2695	'3418	+052	'1276
'5966	-495	'3503	'4365	-680	'3604	'4881	+025	'2723	'3432	+050	'1301
'5979	-517	'3526	'4377	-715	'3625	'4898	-020	'2753	'3448	+105	'1329
'5992	-515	'3549	'4390	-745	'3648	'4913	-032	'2780	'3615	+100	'1624

TABLE II (continued)

J.D. Hel. -2430000	Δm	phase	J.D. Hel. -2430000	Δm	phase	J.D. Hel. -2430000	Δm	phase	J.D. Hel. -2430000	Δm	phase
d 2440'3630	m +100	P '1650	d 2444'4333	m -882	P '3457	d 2453'5113	m -700	P '3609	d 2461'4534	m -690	P '3722
'3645	+095	'1677	'4358	-885	'3501	'5136	-675	'3650	'4545	-702	'3741
'3674	+100	'1728	'4369	-885	'3521	'5183	-692	'3733	'4558	-692	'3764
'3691	+145	'1758	'4375	-872	'3531	'5203	-685	'3768	'4571	-685	'3786
'3706	+140	'1784	'4385	-855	'3549	'5226	-685	'3808	'4584	-705	'3810
			'4411	-852	'3595	'5246	-688	'3844	'4597	-698	'3833
2441'5611	-440	'2787	'4422	-852	'3614	'5293	-690	'3927	'4624	-710	'3880
'5628	-478	'2817	'4434	-848	'3636	'5314	-658	'3964	'4639	-712	'3907
'5645	-538	'2847	'4445	-818	'3655	'5334	-648	'3999	'4652	-708	'3930
'5664	-568	'2880	'4463	-802	'3687				'4664	-715	'3951
'5681	-618	'2910	'4477	-800	'3711	2461'3418	+150	'1752	'4676	-705	'3972
'5698	-658	'2940	'4491	-800	'3736	'3442	+180	'1795	'4692	-715	'4000
'5713	-690	'2967	'4503	-780	'3757	'3458	+160	'1823	'4704	-715	'4022
'5730	-712	'2997	'4516	-780	'3780	'3474	+180	'1852	'4714	-688	'4039
'5744	-745	'3021	'4529	-782	'3803	'3491	+182	'1882	'4730	-660	'4067
'5766	-812	'3060	'4541	-762	'3824	'3509	+198	'1913	'4747	-708	'4097
'5782	-825	'3088	'4554	-755	'3847	'3526	+182	'1943	'4762	-718	'4124
'5798	-845	'3117	'4565	-748	'3867	'3548	+205	'1982			
			'4581	-718	'3895	'3573	+208	'2026	2465'3299	+122	'2106
2444'3596	+152	'2157	'4594	-718	'3918	'3600	+195	'2074	'3317	+182	'2142
'3604	+148	'2171	'4613	-718	'3951	'3623	+188	'2114	'3332	+180	'2168
'3632	+140	'2221	'4626	-710	'3974	'3646	+185	'2155	'3349	+182	'2198
'3649	+142	'2251	'4638	-710	'3995	'3676	+142	'2208	'3366	+202	'2228
'3679	+112	'2304	'4653	-715	'4022	'3705	+138	'2259	'3386	+155	'2263
'3693	+050	'2328				'3738	+138	'2317	'3393	+165	'2276
'3704	+110	'2348	2453'3953	+112	'1563	'3763	+125	'2361	'3405	+202	'2297
'3716	+092	'2369	'3973	+172	'1598	'3784	+128	'2398	'3420	+162	'2323
'3730	+052	'2394	'3996	+148	'1639	'3799	+132	'2425	'3440	+188	'2359
'3744	+028	'2418	'4016	+158	'1674	'3830	+115	'2480	'3455	+165	'2385
'3763	+005	'2452	'4053	+188	'1739	'3849	+062	'2513	'3470	+155	'2412
'3777	-020	'2476	'4076	+182	'1780	'3865	+060	'2541	'3485	+142	'2438
'3784	-052	'2498	'4099	+200	'1820	'3888	+022	'2582	'3502	+128	'2468
'3804	-095	'2524	'4117	+188	'1852	'3919	-018	'2637	'3524	+120	'2507
'3818	-150	'2549	'4138	+160	'1889	'3933	-052	'2661	'3539	+105	'2533
'3834	-182	'2577	'4161	+200	'1930	'3948	-078	'2688	'3553	+068	'2558
'3843	-248	'2593	'4188	+182	'1977	'3962	-100	'2713	'3567	+052	'2583
'3864	-280	'2630	'4213	+178	'2021	'3979	-128	'2742	'3580	+070	'2606
'3875	-338	'2649	'4238	+148	'2065	'3997	-180	'2774	'3594	+022	'2630
'3886	-382	'2669	'4261	+155	'2106	'4010	-212	'2797	'3610	+018	'2658
'3914	-470	'2718	'4284	+165	'2147	'4024	-230	'2822	'3627	-005	'2688
'3928	-550	'2743	'4311	+138	'2194	'4042	-272	'2854	'3643	-038	'2717
'3940	-540	'2764	'4335	+118	'2237	'4059	-310	'2884	'3658	-045	'2743
'3951	-572	'2783	'4360	+115	'2281	'4072	-332	'2907	'3671	-070	'2766
'3964	-610	'2806	'4393	+080	'2339	'4086	-362	'2931	'3688	-135	'2796
'3976	-640	'2828	'4413	+060	'2374	'4101	-382	'2958	'3703	-132	'2823
'3987	-655	'2847	'4436	+045	'2432	'4121	-392	'2993	'3719	-160	'2851
'3999	-685	'2868	'4459	+010	'2455	'4140	-395	'3027	'3722	-220	'2874
'4011	-700	'2889	'4470	-052	'2475	'4159	-392	'3060	'3745	-242	'2897
'4029	-748	'2921	'4503	-115	'2533	'4178	-405	'3094	'3758	-320	'2920
'4040	-782	'2940	'4526	-170	'2574	'4197	-398	'3127	'3789	-352	'2974
'4054	-795	'2965	'4548	-202	'2612	'4212	-400	'3154	'3801	-352	'2995
'4066	-808	'2986	'4569	-270	'2649	'4227	-395	'3180	'3813	-362	'3017
'4077	-818	'3006	'4590	-325	'2686	'4253	-420	'3226	'3827	-362	'3041
'4097	-842	'3041	'4612	-372	'2725	'4267	-435	'3251	'3841	-350	'3066
'4112	-852	'3067	'4635	-418	'2766	'4281	-452	'3275			
'4125	-855	'3090	'4659	-480	'2810	'4301	-485	'3311	2478'3722	+145	'2199
'4136	-850	'3110	'4680	-532	'2845	'4317	-492	'3338	'3775	+135	'2292
'4153	-880	'3140	'4708	-530	'2895	'4330	-510	'3362	'3809	+098	'2352
'4167	-895	'3164	'4729	-570	'2932	'4347	-518	'3392	'3827	+080	'2384
'4182	-892	'3191	'4751	-570	'2970	'4367	-548	'3427	'3848	+050	'2421
'4193	-895	'3210	'4779	-588	'3020	'4382	-552	'3453	'3868	+025	'2456
'4206	-898	'3233	'4801	-588	'3059	'4399	-575	'3483	'3890	-005	'2495
'4217	-908	'3253	'4822	-630	'3096	'4408	-590	'3499	'3907	-045	'2525
'4245	-918	'3302	'4847	-645	'3140	'4422	-590	'3524	'3922	-058	'2552
'4259	-922	'3327	'4870	-650	'3180	'4435	-608	'3547	'3933	-082	'2571
'4274	-912	'3353	'4892	-655	'3219	'4448	-635	'3570	'3946	-080	'2594
'4284	-910	'3371	'4913	-665	'3256	'4461	-645	'3593	'3961	-122	'2620
'4296	-890	'3392	'4943	-688	'3309	'4476	-660	'3619	'3973	-168	'2642
'4306	-898	'3410	'4976	-665	'3367	'4506	-675	'3672	'3984	-205	'2661
'4319	-890	'3433	'4998	-692	'3406	'4520	-700	'3696	'3998	-215	'2686

TABLE II (continued)

J.D. Hel. -2430000	Δm	phase	J.D. Hel. -2430000	Δm	phase	J.D. Hel. -2430000	Δm	phase	J.D. Hel. -2430000	Δm	phase
d 2478'4009	m -242	P '2705	d 2478'4320	m -765	P '3254	d 2486'3052	m +142	P '2151	d 2486'3607	m -692	P '3130
'4021	-265	'2726	'4331	-762	'3273	'3073	+125	'2188	'3629	-740	'3169
'4032	-279	'2746	'4345	-788	'3298	'3092	+140	'2221	'3646	-758	'3199
'4046	-322	'2770	'4356	-812	'3317	'3124	+105	'2277	'3666	-760	'3234
'4061	-342	'2796	'4366	-815	'3335	'3144	+075	'2313	'3683	-762	'3264
'4071	-395	'2814	'4378	-828	'3356	'3165	+062	'2350	'3700	-780	'3294
'4081	-412	'2832	'4396	-832	'3388	'3187	+012	'2389	'3720	-768	'3329
'4092	-412	'2852	'4406	-812	'3405	'3203	+000	'2417	'3739	-772	'3363
'4103	-430	'2871	'4410	-850	'3413	'3224	-035	'2454	'3761	-772	'3402
'4118	-452	'2897	'4429	-852	'3446	'3245	-062	'2491	'3779	-788	'3433
'4129	-475	'2917	'4440	-862	'3465	'3264	-087	'2525	'3799	-772	'3469
'4140	-472	'2936	'4453	-855	'3488	'3282	-142	'2556	'3814	-772	'3495
'4151	-510	'2956	'4464	-845	'3508	'3299	-165	'2586	'3837	-765	'3536
'4163	-538	'2977	'4475	-828	'3527	'3320	-242	'2624	'3857	-758	'3571
'4186	-555	'3017	'4485	-828	'3545	'3338	-292	'2655	'3873	-755	'3599
'4197	-585	'3037	'4497	-828	'3566	'3360	-332	'2694	'3889	-755	'3627
'4208	-600	'3056	'4507	-822	'3584	'3380	-360	'2729	'3908	-747	'3661
'4218	-630	'3074	'4518	-835	'3603	'3403	-425	'2770	'3924	-732	'3689
'4229	-652	'3093	'4529	-835	'3622	'3439	-438	'2833	'3940	-747	'3717
'4239	-662	'3111	'4543	-832	'3638	'3458	-500	'2867	'3958	-732	'3749
'4249	-662	'3128	'4554	-825	'3658	'3476	-485	'2899	'3974	-708	'3777
'4259	-682	'3146	'4567	-835	'3681	'3500	-550	'2941	'3992	-708	'3809
'4269	-692	'3163	'4578	-815	'3700	'3521	-580	'2978	'4020	-682	'3858
'4280	-705	'3183	'4588	-808	'3717	'3536	-612	'3005	'4036	-678	'3887
'4290	-725	'3201	'4594	-788	'3737	'3556	-622	'3040	'4054	-672	'3918
'4300	-742	'3218	'4610	-798	'3757	'3573	-658	'3070	'4076	-670	'3957
'4310	-752	'3236				'3589	-680	'3098	'4091	-662	'3984

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