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COMMUNICATION FROM THE OBSERVATORY AT LEIDEN.

The Secular Perturbations of Pallas by Jupiter, by R. T. A. Innes.*)

Our knowledge of the motion of this minor planet is succinctly given by A. O. LEUSCHNER in *Bulletin* N°. 25 of the U. S. Am. National Research Council (1922).

As is well known GAUSS gave much attention to this planet and he believed that commensurability with Jupiter existed in the relation

$$18 n_i - 7 n = 0.$$

GAUSS's work was published after a lapse of about a century, and has been used by G. STRUVE in his Inaugural Dissertation "Die Darstellung der Pallasbahn durch die GAUSS'sche Theorie für den Zeitraum 1803 bis 1910." (Berlin 1911). In *B. A. N.* 28 J. WOLTJER points out that in case of commensurability the integers must add up to zero. In other words, in place of $18 n_i - 7 n = 0$ we must have some such form as

$$18 n_i - 7 n - j_i \frac{d\omega_i}{dt} - j \frac{d\omega}{dt} - i \frac{d\Omega}{dt} = 0$$

in which

$$j_i + j + i = 18 - 7 = 11.$$

The most remarkable case of commensurability is that connecting the longitudes of three of Jupiter's satellites, in which

$$n - 3 n_i + 2 n_2 = 0.$$

The satellites of Saturn furnish several examples, the most striking being that of Titan and Hyperion, namely

$$4 l - 3 l_i - \omega = 180^\circ + \text{librational terms.}$$

In all these cases the factors j_i , j and i are zero or ± 1 .

In the case of Pallas and Jupiter, the only admissible values would appear to be

$$\begin{array}{ccc} j_i & j & i \\ 0 & +11 & 0 \\ 0 & +10 & +1 \\ +1 & +10 & 0 \end{array}$$

and the very size of the j almost prohibits a real librational effect.

It is not easy to determine the mean motion of Pallas. LE VERRIER used

$$n_i = 109256'', \quad n = 280711'',$$

consequently

$$18 n_i - 7 n = 1631''.$$

We may consider Jupiter's mean motion n_i as known exactly. Its daily value is $299^\circ 1283$. If the relation $18 n_i - 7 n = 0$ holds, then $n = 769^\circ 187$. In the table given by LEUSCHNER, the value of n varies from

$$768^\circ 45 \text{ to } 770^\circ 75.$$

These are osculating values; GAUSS's mean value was $769^\circ 1507$, whilst G. STRUVE finds $769^\circ 13850$.

It is evident that the difference $18 n_i - 7 n$ is very small. If we accept G. STRUVE's mean motion then

$$18 n_i - 7 n = +0^\circ 3412 \text{ in a day,} \\ \text{or} \quad = 124'' 6 \text{ in a Julian year.}$$

Can we now find some likely combination, such that

$$j_i \frac{d\omega_i}{dt} + j \frac{d\omega}{dt} + i \frac{d\Omega}{dt} = +124'' 6.$$

We know $\frac{d\omega_i}{dt}$, the motion of the perihelion of Jupiter, with great precision; it is $+7'' 70$. This motion is too small to be of any importance so we turn to the motions of ω and Ω .

GAUSS gave values for these, which reduced by G. STRUVE to a more modern value of the mass of Jupiter, are

*) The investigation by Dr. INNES contained in this communication arose out of a conversation which he had with Dr. WOLTJER and myself during his visit to Leiden in December 1924. It is with reference to these circumstances that Dr. INNES graciously considers it as a work of the Leiden Observatory. This explains why this paper is published as a communication from Leiden in the *B. A. N.*

W. DE SITTER

$$\frac{d\omega}{dt} = -11''.0301 \quad \frac{d\Omega}{dt} = -36''.0642$$

N. B. This value of $\frac{d\omega}{dt}$ corresponds to $-10''.8260$ and not to $-10''.8960$ as printed on page 35 of STRUVE's paper.

We notice that the motion of the perihelion of Pallas is negative and this is unusual. Thus the action of Jupiter on the four interior planets (NEWCOMB, *A. P. V.*) gives

Planet	$e \frac{d\omega}{dt}$
Mercury	+ 0''.317
Venus	+ 0.046
Earth	+ 0.117
Mars	+ 1.164

In the cases of Ceres and Iris C. J. MERFIELD found $\frac{d\omega}{dt} = +55''.9$ and $+31''.94$ respectively (*M. N. LXVII* p. 560 and *Ast. Nach.* 4337). If in the case of Pallas $\frac{d\omega}{dt}$ was positive, it would fit in well as $11 \frac{d\omega}{dt} = 121''.3$, almost exactly equal to $18 n_1 - 7 n$. Was it possible that GAUSS had made an error of sign? It was to settle this doubt that I determined to compute the secular perturbations of Pallas through the action of Jupiter by GAUSS's Elliptical Ring method. It was only when my calculation was practically finished that I found out that P. BRUCK had made the computation in 1895 (*Bull. Astr.*, XII p. 289) and found $\frac{d\omega}{dt} = -9''.76$. The osculating values of ω given in LEUSCHNER's table also indicated that the motion of the perihelion was negative and might even be as large as $-21''$. My surmise that the sign given by GAUSS was in error thus falls to the ground.

Thus it is fully proved that the possible values of

$$j_i \frac{d\omega_i}{dt} + j \frac{d\omega}{dt} + i \frac{d\Omega}{dt}$$

$$\begin{aligned} \sin \pi \sin J &= -\sin i \cos i_i \sin \omega + \cos i \sin i_i \cos (\Omega_i - \Omega) \sin \omega - \sin i_i \sin (\Omega_i - \Omega) \cos \omega \\ \cos \pi \sin J &= -\sin i \cos i_i \cos \omega + \cos i \sin i_i \cos (\Omega_i - \Omega) \cos \omega + \sin i_i \sin (\Omega_i - \Omega) \sin \omega \\ \sin \pi_i \sin J &= \cos i \sin i_i \sin \omega_i - \sin i \cos i_i \cos (\Omega_i - \Omega) \sin \omega_i - \sin i_i \sin (\Omega_i - \Omega) \cos \omega_i \\ \cos \pi_i \sin J &= \cos i \sin i_i \cos \omega_i - \sin i \cos i_i \cos (\Omega_i - \Omega) \cos \omega_i + \sin i_i \sin (\Omega_i - \Omega) \sin \omega_i \end{aligned}$$

The introduction of auxiliary angles lengthens the work.

We get

We now compute

$$\begin{aligned} a_c &= \alpha (\cos \pi_i \cos \pi + \sin \pi_i \sin \pi \cos J) \\ a_s &= \alpha (\cos \pi_i \sin \pi - \sin \pi_i \cos \pi \cos J) \end{aligned}$$

and get

$$\begin{array}{lll} a_c = -0.1966065 & e a_c = -0.0467916 & \cos \varphi a_c = -0.1909572 \\ a_s = +0.4862153 & e a_s = +0.1157174 & \cos \varphi a_s = +0.4722444 \\ b_c = -0.1202819 & e b_c = -0.0286266 & \cos \varphi b_c = -0.1168257 \\ b_s = +0.4324572 & e b_s = +0.1029232 & \cos \varphi b_s = +0.4200310 \end{array}$$

are adverse to any near approach to $18 n_1 - 7 n$. By far the most probable argument is

$$18 n_1 - 7 n - 11 \frac{d\omega}{dt} = 0.$$

If we now take $\frac{d\omega}{dt} = -10''$, and adopt

$$18 n_1 - 11 \frac{d\omega}{dt} = 5494'' = 7 n,$$

we get

$$n = 785'',$$

which is a quite inadmissible value. The idea of a libration may therefore be dismissed.

It may nevertheless be worth while to give the results of my computation and the steps by which they were reached. In the *Monthly Notices* for May 1907, I gave a process for GAUSS's method based on the HALPHEN-ARNDT investigation, which evades the solution of a cubic equation, but the process was intended mainly for logarithmic work and made use of the true anomaly of the disturbed planet. This solution has been partly revised so as to eliminate the true anomaly and to make more use of the calculating machine.

The elements adopted are from G. STRUVE's paper

Pallas	Jupiter
$\Omega = 172^\circ 52' 52''$	$\Omega_1 = 99^\circ 26' 36''$
$i = 34^\circ 42' 53.8''$	$i_1 = 1^\circ 18' 31.4''$
$\omega = 309^\circ 15' 39.6''$	$\omega_1 = 273^\circ 16' 39.2''$
$e = 0.2379962$	$e_1 = 0.0483348$
$\log \alpha = 0.442645$	$\log \alpha_1 = 0.716217$
$n = 769''.1385$	$\log \alpha = 9.7264278$

Putting

J = mutual inclination of orbits.

π and π_1 = angular distances of the perihelia from the ascending node of the disturbing planet on the orbit of the disturbed, and solving directly, we have

$$J = 34^\circ 21' 42''$$

$$\pi = 127^\circ 2' 17.3''$$

$$\pi_1 = 18^\circ 0' 30.8''$$

At this stage it is necessary to decide on the number of divisions of the circumference to be used, and 16 was chosen. For each of these, we now compute

$$\begin{aligned} r_o &= \alpha - e \alpha \cos E \\ &= 0.5326327 - 1.267646 \cos E \\ r_o^2 &= 0.2917322 - 1.350379 \cos E + 0.0080346 \cos 2E \\ r_o A_c &= a_c \cos E - \cos \varphi a_s \sin E - ea_c \\ r_o B_c &= -a_s \cos E - \cos \varphi a_c \sin E + ea_s \\ r_o A_s &= b_s \cos E + \cos \varphi b_c \sin E - eb_s \\ r_o B_s &= b_c \cos E - \cos \varphi b_s \sin E - eb_c \\ D &= r_o A_c \cos^2 \varphi_i - e_i r_o^2 = +0.0325815 \\ &- 1.896201 \cos E - 4.711411 \sin E - 0.0003884 \cos 2E \end{aligned}$$

In computing these, it is best, in spite of some repetition, to make a table giving the 16 values of $\cos E$, $\sin E$, etc. This table is reproduced.

The sums of the even and of the odd divisions for these quantities must equal 8 times the constant quantities and this affords a check. This holds good until we come to the quantities involving the angle ι , and even then, if the number of divisions of the circumference is large enough, the two sums ought to approach equality. In the tables these sums are indicated by Σ and Σ' .

Then

$$\begin{aligned} P_1 &= \frac{2}{3} (1 - e_i^2 + r_o^2 + 2e_i r_o A_c) \\ P_2 &= \frac{2}{3} (r_o^2 A_c^2 + r_o^2 A_s^2 + 2e_i D + e_i^2 r_o^2) \\ P_3 &= 4e_i^2 (r_o A_s)^2 \\ \text{N.B. } \sqrt{P_3} &= 2e_i r_o A_s \text{ is also wanted.} \\ G_2 &= P_1^2 - 2P_2 \quad G_3 = P_1^3 - 3P_1 P_2 - P_3 \\ \lambda &= \frac{2}{4} G_2 \quad \cos \iota = G_3 / G_2^{\frac{3}{2}} \\ \Phi_R &= (r_o A_c D + r_o A_s r_o A_s) \frac{1}{r_o} - r_o (P_1 - e_i r_o A_c) \\ \Phi_S &= (r_o B_c D + r_o B_s r_o A_s) \frac{1}{r_o} \end{aligned}$$

$$\begin{aligned} \Phi_W &= \sin \pi_i D + \cos \pi_i \cos \varphi_i r_o A_s \\ \chi_R - \frac{1}{4} G_2 r_o &= \frac{1}{2} (P_1 \Phi_R + P_2 r_o) \\ \chi_S &= \frac{1}{2} (P_1 \Phi_S - \sqrt{P_3} r_o \cos \varphi_i \cos J) \\ \chi_W &= \frac{1}{2} (P_1 \Phi_W - \sqrt{P_3} (r_o A_c \cos \varphi_i \cos \pi_i - r_o A_s \sin \pi_i)) \end{aligned}$$

We must now find the values of the two series

$$F\left(\frac{1}{6}, \frac{5}{6}; 2; \sin^2 \frac{\iota}{2}\right)$$

and

$$F\left(-\frac{1}{6}, \frac{7}{6}; 2; \sin^2 \frac{\iota}{2}\right)$$

Their logarithms are tabulated for each degree of ι at the end of this paper. From $\iota = 0^\circ$ to 90° the table is taken from FRANK ROBBINS's paper in the *Monthly Notices*, 1907 May; and from 90° to 180° from C. J. MERFIELD's in the *Monthly Notices*, 1908 June, with the kind permissions of the authors. The

properties of these series are given in the *Proceedings of the R. S. Edinburgh*, XXVII part IV, pp. 360–361.

Putting

$$F_+ = \frac{15}{8} F\left(\frac{1}{6}, \frac{5}{6}; 2; \sin^2 \frac{\iota}{2}\right) / \left(\lambda^{\frac{7}{4}} \cos^2 \frac{\iota}{2}\right)$$

and

$$F_- = \frac{7}{8} F\left(-\frac{1}{6}, \frac{7}{6}; 2; \sin^2 \frac{\iota}{2}\right) / \left(\lambda^{\frac{5}{4}} \cos^2 \frac{\iota}{2}\right)$$

we have

$$\begin{aligned} \frac{1}{\alpha^2} \frac{a}{r} R_o &= F_- \Phi_R + F_+ (\chi_R - \frac{1}{4} G_2 r_o) \\ \frac{1}{\alpha^2} \frac{a}{r} S_o &= F_- \Phi_S + F_+ \chi_S \\ \frac{1}{\alpha \sin J} \times \frac{a}{r} W_o &= [F_- \Phi_W + F_+ \chi_W] r_o. \end{aligned}$$

Having the 16 values of each of these quantities, which we may designate as

$$R_o, R_1, \dots, R_{15}; S_o, S_1, \dots, S_{15} \text{ and } W_o, W_1, \dots, W_{15}$$

respectively, we compute

$$\begin{aligned} A_{c,o} &= \frac{1}{r_o} [R_o + R_1 + \dots + R_{15}] \\ \frac{1}{2} A_{c,1} &= \frac{1}{r_o} [R_o + R_1 \cos 22\frac{1}{2}^\circ + \dots + R_{15} \cos 337\frac{1}{2}^\circ] \\ \frac{1}{2} A_{c,2} &= \frac{1}{r_o} [R_o + R_1 \cos 45^\circ + \dots + R_{15} \cos 315^\circ] \\ \frac{1}{2} A_{s,1} \text{ and } \frac{1}{2} A_{s,2} &: \text{Replace cos by sin in } \frac{1}{2} A_{c,1} \text{ and } \frac{1}{2} A_{c,2} \text{ respectively.} \end{aligned}$$

The expressions for $B_{c,o}, \frac{1}{2} B_{c,1}, \dots, C_{c,o}, \frac{1}{2} C_{c,1}$ etc. are similar.

N.B. $\frac{1}{2} A_{s,2}$ is not required.

The above formulae can be consolidated, but this is not advisable as it complicates the check by the addition of even and odd divisions.

The equation

$$\sin \varphi \frac{1}{2} A_{s,1} + \cos \varphi B_{c,o} = 0$$

affords a useful check. In the present case, the first five significant figures agree.

The final equations are

$$\begin{aligned} e \frac{d\varphi}{dt} &= m_i n \alpha^2 \left[-\left(1 + \frac{e^2}{2}\right) B_{c,o} + 2e \frac{1}{2} B_{c,1} - \frac{e^2}{2} \frac{1}{2} B_{c,2} \right] \\ e \frac{d\chi}{dt} &= m_i n \alpha^2 \left[e \cos \varphi A_{c,o} - \cos \varphi \frac{1}{2} A_{c,1} \right. \\ &\quad \left. + (2 - e^2) \frac{1}{2} B_{s,1} - \frac{e}{2} \frac{1}{2} B_{s,2} \right] \end{aligned}$$

$$\begin{aligned} \frac{di}{dt} &= \frac{m_i n \alpha \sin J}{\cos \varphi} \left[(\frac{1}{2} C_{c,1} - e C_{c,o}) \cos \omega - \frac{1}{2} C_{s,1} \sin \omega \right] \\ \sin i \frac{d\Omega}{dt} &= \frac{m_i n \alpha \sin J}{\cos \varphi} \left[(\frac{1}{2} C_{c,1} - e C_{c,o}) \sin \omega + \frac{1}{2} C_{s,1} \cos \omega \right] \\ -2 \frac{r}{a} R_o &= \alpha^2 \left[-(2 + e^2) A_{c,o} + 4e \frac{1}{2} A_{c,1} - e^2 \frac{1}{2} A_{c,2} \right] \end{aligned}$$

Taking the values of the A , B and C from the tables which follow and using

$$\begin{aligned} m_1 n \alpha^2 &= 76.095 \\ m_1 n \alpha \sin J &= 80.634 \end{aligned}$$

we obtain the secular perturbations due to the first order of Jupiter's mass. With our results we include for comparison BRUCK's and the GAUSS-STRUVE figures.

GAUSS was able to extract from his work the secular variations and these are given by G. STRUVE (p. 17). STRUVE adds that he attempted to recompute the secular variations by means of the Lund Tables (1900) but that the attempt was unsuccessful because e and i are not sufficiently small quantities and that he did not go further. On page 35 he repeats GAUSS's values reduced to the mass of Jupiter adopted ($1/1047.35$) and these are given below.

BRUCK's figures are reduced to the values of α and $m_1 n$ used by STRUVE. It should be remarked that BRUCK used 32 divisions and that the lack of equality between Σ and Σ' from ι onwards in my results shows that 16 divisions as used by me are really insufficient although the resulting error may be very small.

The comparison is as follows:

	This calculation	GAUSS G. STRUVE p. 35	BRUCK
$\frac{de}{dt}$	- 10.591		- 10.531
$\frac{d\phi}{dt}$	- 10.904	- 10.998	
$\frac{d\omega}{dt}$	- 9.871	- 11.030	- 9.756
$\frac{di}{dt}$	+ 5.094	+ 5.054	+ 4.926
$\frac{d\Omega}{dt}$	- 35.354	- 36.064	- 35.647
$- 2 \frac{r}{a} R_o$	- 0.06094		- 0.05940
$\frac{d\chi}{dt}$	- 3.5781		
$\frac{d\varepsilon}{dt}$	- 22.7408	- 22.7264	- 22.3871

With this value of $d\varepsilon/dt$ we are now prepared to calculate the semi-axis major with accuracy. If this is determined by the Keplerian relation

$$a^3 n^2 = k^2 (1 + m) \quad \log k = 3.5500066$$

it requires the correction

$$+ \frac{1}{6} \frac{a}{n} \frac{d\varepsilon}{dt}$$

LE VERRIER indicates a correction four times larger (see for example, *Annales de l'Obs. de Paris*, Mem.

X. p 189) but this has ultimately to be reduced by the inclusion of the constant terms in the perturbations of the radius-vector. If therefore the perturbations are going to be developed analytically and by powers of the masses it is best to start with the semi-axis major

$$a (1 + \frac{d\varepsilon}{dt} / 6 n). \quad (1)$$

If however the perturbations of the radius-vector are determined by mechanical integrations so that the non-periodical parts are included in the integrations, the equation leading to the semi-axis major should be

$$a (1 + 2 \frac{d\varepsilon}{dt} / 3 n). \quad (2)$$

In computing the secular perturbations form (1) should be used. Actually the value given by form (2) was used.

G. STRUVE's mean motion $n = 769.1385$ gives the Keplerian value

$$\log a = 0.4426680.$$

The correction to this by (1) is

$$[8.85963] \frac{d\varepsilon}{dt} / n = - 0.00000587$$

The effect due to the action of the other planets may be estimated at $-1/33$ of Jupiter's; and accepting this, the correction is

$$- 0.00000567 \quad \text{by (1)}$$

and

$$- 0.00002268 \quad \text{" (2)}$$

giving

$$\log a = 0.4426623 \quad \text{or} \quad \log a = 0.4426453$$

the latter being the value given by G. STRUVE.

The first value may be called the mean value because it only suffers strictly periodic variations.

References.

A good list is given by ERIC DOOLITTLE in his Memoir published in the *Transactions of the American Philosophical Society*, XXII part 2, (Philadelphia 1912). Others are:

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E	N°.	$\cos E$	$\sin E$	$\cos 2E$	$\sin 2E$	r_0	r_0^2	$r_0 A_c$	$r_0 B_c$	$r_0 A_s$
0°	0	1.0000000	0.0000000	1.0000000	0.0000000	0.4058681	0.1647289	-0.1498150	-0.3704979	+0.3295339
22½	1	0.9238795	0.3826834	0.7071068	0.7071068	.4155174	.1726548	-3155692	-2604108	+2519078
45	2	0.7071068	0.7071068	0.0000000	1.0000000	.4429966	.1962460	-4261574	-0930616	+1202620
67½	3	0.3826834	0.9238795	-0.7071068	0.7071068	.4841220	.2343738	-4647432	+1060723	+0453619
90	4	0.0000000	1.0000000	-1.0000000	0.0000000	.5326327	.2836976	-4254527	.3066746	-2197489
112½	5	-0.3826834	0.9238795	-0.7071068	-0.7071068	.5811434	.3377274	-3142671	.4782054	-3763502
135	6	-0.7071068	0.7071068	0.0000000	-1.0000000	.6222688	.3872184	-1481136	.5945507	+4913248
157½	7	-0.9238795	0.3826834	0.7071068	-0.7071068	.6497480	.4221727	+0477123	.6379979	+5471688
180	8	-1.0000000	0.0000000	1.0000000	0.0000000	.6593973	.4348047	.2433983	.6019327	+5353804
202½	9	-0.9238795	-0.3826834	0.7071068	0.7071068	.6497480	.4221727	.4091525	.4918456	-4577542
225	10	-0.7071068	-0.7071068	0.0000000	1.0000000	.6222688	.3872184	.5197407	.3244964	-3261084
247½	11	-0.3826834	-0.9238795	-0.7071068	0.7071068	.5811434	.3377274	.5583264	+1253625	-1604846
270	12	0.0000000	-1.0000000	-1.0000000	0.0000000	.5326327	.2836976	.5190359	-0752398	+0139025
292½	13	0.3826834	-0.9238795	-0.7071068	-0.7071068	.4841220	.2343738	.4078504	.2467706	+1705038
315	14	0.7071068	-0.7071068	0.0000000	-1.0000000	.4429966	.1962460	.2416668	.3631159	+2854785
337½	15	0.9238795	-0.3826834	0.7071068	-0.7071068	.4155174	.1726548	.0458709	-4065030	.3413224
	Σ					4.2610616	2.3338576	+3743330	+9257392	-8233856
	Σ'					4.2610616	2.3338574	+3743330	+9257393	-8233857

N°.	$r_0 B_s$	P_1	P_2	P_3	D	Φ_R	Φ_S	Φ_W	$\chi_{R-\frac{1}{4}G_2} r_0$
0	-0.0916553	+0.7652734	+0.0774691	+0.0010148	-0.1574271	+0.0121275	+0.0692903	+0.2643539	+0.0203587
I	-2432383	'7598751	.0881356	.0005930	-3231774	.0760807	.0550764	.1393737	.0472169
2	-3534323	'7684755	.1030095	.0001352	.4346474	.1012164	.0046402	.0201386	.0617076
3	-4054613	'7914075	.1151165	.0000192	.4749858	.0662104	.0660790	.1899357	.0540649
4	-3914044	.8268220	.1250696	.0004513	.4381711	.0106840	.0908042	.3442039	.0288912
5	-3134015	.8700075	.1395368	.0013236	.3298569	.0923233	.0684697	.4594729	.0003843
6	-1833280	.9137093	.1654323	.0022559	.1664837	.1454653	.0143176	.5181788	.0149848
7	-0.0209864	.9496322	.2035236	.0027978	+0.0271952	.1527417	.0443765	.5113472	.0064047
8	+1489085	.9706651	.2455556	.0026786	.2218134	.1157320	.0815801	.4399814	.0247908
9	.3004917	.9729257	.2769457	.0019581	.3877910	.0526188	.0818501	.3149308	.0643753
10	.4106857	.9567501	.2837984	.0009938	.4998103	.0086373	.0454121	.1552488	.0924314
11	.4627145	.9262430	.2603613	.0002407	.5406681	.0411905	.0111422	.0147180	.0947298
12	.4486576	.8876909	.2126577	.0000018	.5041108	.0321544	.0595003	.1669567	.0709058
13	.3706547	.8476432	.1561337	.0002717	.3955691	.0075201	.0710910	.2842552	.0346067
14	.2405810	.8115163	.1085113	.0007616	.2310465	.0439686	.0348396	.3427914	.0061945
15	.0782394	.7831685	.0817505	.0010887	.0374184	.0399925	.0276570	.3357900	.0013239
Σ	+0.2290128	+6.9009026	+1.3215035	+0.0082930	+0.2606517	-1617143	.0078194	.7015495	+2902952
Σ'	+0.2290128	+6.9009027	+1.3215037	+0.0082928	+0.2606517	-1617148	.0078219	.7015497	+2902971

N°.	χ_S	χ_W	G_2	G_2	$(\log 1/\lambda^{\frac{1}{4}})$	ι	$\log F(\frac{1}{8}, \frac{5}{8}; 2; \sin^2 \frac{\iota}{2})$	$\log F(-\frac{1}{8}, \frac{7}{8}; 2; \sin^2 \frac{\iota}{2})$
0	+0.0211828	+0.1050409	+0.4307051	+0.2693073	0.0034093	17° 41' 1" 4'	0.0007180	9.9989941
I	+0.167541	+0.0575518	.4011388	.2372499	0.0111306	20 57 42' 6"	.0010088	'9985864
2	-0.0030061	-0.0051688	.3845355	.2162107	0.0157203	24 56 19' 8"	.0014277	'9979986
3	-0.0252725	-0.0760954	.3960924	.2223476	0.0125050	26 52 56' 8"	.0016587	'9976743
4	-0.0328749	-0.1458686	.4334953	.2545619	0.0027083	26 53 12' 7"	.0016592	'9976735
5	-0.0210681	-0.2031863	.4778393	.2930022	9.9921339	27 29 43' 0"	.0017351	'9975670
6	+0.0056435	-0.2364663	.5040001	.3070966	9.9863467	30 52 33' 3"	.0021876	'99669312
7	+0.0352394	-0.2371234	.4947544	.2737645	9.9883570	38 7 28' 8"	.0033336	'9953186
8	+0.0536629	-0.2032711	.4510795	.1968163	9.9983910	49 29 4' 0"	.0056098	'9921055
9	+0.0516704	-0.1414718	.3926934	.1106560	0.0134409	63 16 39' 0"	.0091539	'9870756
10	+0.0298113	-0.0648661	.3477744	.0602152	0.0266304	72 55 34' 2"	.0121332	'9828216
11	-0.0014433	-0.0113150	.3372037	.0709340	0.0299812	68 45 40' 2"	.0107972	'9847320
12	-0.0267041	-0.0747666	.3626797	.1331714	0.0220735	52 25 52' 1"	.0062953	'9911352
13	-0.0334196	-0.1177151	.4062311	.2117216	0.0097611	35 8 33' 4"	.0028331	'9960232
14	-0.0191769	-0.1371402	.4415356	.2694935	0.0007129	23 17 9' 2"	.0012448	'9982553
15	+0.0051778	-0.1325122	.4498521	.2871970	9.9986869	17 50 58' 5"	.0007315	9.9989752
Σ	+0.0276385	-0.3387832	3.3558052	1.7068729		298 30 46' 7"	.0312756	9.9559150
Σ'	+0.0276382	-0.3387828	3.3558052	1.7068728		298 29 42' 3"	.0312519	9.9559523

Nº.	F_+	$\log F_+$	F_-	$\log F_-$	$\frac{I}{\alpha^2} \frac{\alpha}{r} R_0$	$\frac{I}{\alpha^2} \frac{\alpha}{r} S_0$	$\frac{I}{\alpha} \frac{\alpha}{\sin J} \frac{\alpha}{r_0} W_0$
0	2.0322087	0.3079683	0.9298922	9.9684326	+ 0.0526504	+ 0.1074804	+ 0.1859502
1	2.3256212	.3665389	1.0253262	0.0108620	.1878161	+ .0954350	+ .1149933
2	2.5422258	.4052145	1.0948413	0.0393508	.2676906	- .0150105	- .0155886
3	2.4339966	.3863198	1.0625088	0.0263318	.2019429	- .1317227	- .1873670
4	2.0785000	.3177500	0.9491929	9.9773545	+ .0499092	- .1545213	- .3355974
5	1.7576016	.2449204	0.8423475	9.9254913	- .0770929	- .0947047	- .4324615
6	1.6275510	.2115346	0.7990824	9.9025916	- .1406274	- .0022559	- .4971483
7	1.7531512	.2438194	0.8474171	9.9280972	- .1406643	+ .0993854	- .5516604
8	2.2438094	.3509858	1.0226014	0.0097063	.0627219	.2038333	.5974318
9	3.2809731	.5160025	1.3678840	0.1360493	+ .1392372	.2814905	.5814944
10	4.5790320	.6607746	1.7668830	0.2472093	.4385085	+ .2167453	.3556074
11	4.5754969	.6604382	1.7515300	0.2434174	.5055822	- .0261197	+ .0450681
12	3.3735944	.5280926	1.3733850	0.1377923	.2833677	- .1718055	+ .2579058
13	2.43093258	.3856645	1.0674295	0.0283392	.0760784	- .1571051	+ .2853940
14	1.9828730	.2972949	0.9159809	9.9618864	- .0279915	- .0699377	+ .2595615
15	1.8841741	.2751218	0.8810458	9.9449985	- .0327407	+ .0341230	+ .2206742
Σ	20.4597943		8.8518591		+ .8607856	+ .1145281	- .0978660
Σ'	20.4413405		8.8454889		+ .8601589	+ .1007817	- .0808537

$$A_{c,0} = + 0.1075590$$

$$\frac{1}{2} A_{c,1} = + 0.0100774$$

$$\frac{1}{2} A_{s,1} = - 0.0549149$$

$$\frac{1}{2} A_{c,2} = - 0.0458926$$

$$B_{c,0} = + 0.0134569$$

$$\frac{1}{2} B_{c,1} = - 0.0377854$$

$$\frac{1}{2} B_{s,1} = - 0.0115546$$

$$\frac{1}{2} B_{c,2} = + 0.0805150$$

$$\frac{1}{2} B_{s,2} = + 0.0320310$$

$$C_{c,0} = - 0.1361700$$

$$\frac{1}{2} C_{c,1} = + .1942004$$

$$\frac{1}{2} C_{s,1} = - .1091055$$

$$\sin \varphi \frac{1}{2} A_{s,1} = - 0.0130695$$

$$\cos \varphi B_{c,0} = + .0130702$$

$$\Sigma = + .0000007$$

The following tables of $F(\frac{1}{6}, \frac{5}{6}; 2; \sin^2 t)$ and $F(-\frac{1}{6}, \frac{7}{6}; 2; \sin^2 \frac{t}{2})$ can be checked by the equation

$$F_1(t) F_2(180^\circ - t) + F_1(180^\circ - t) F_2(t) = \frac{216}{35\pi} = 1.964427,$$

where we have put $F_1(t) = F(\frac{1}{6}, \frac{5}{6}; 2; \sin^2 t)$, and $F_2(t) = F(-\frac{1}{6}, \frac{7}{6}; 2; \sin^2 \frac{t}{2})$.

t	$\log F(\frac{1}{\delta}, \frac{5}{\delta}; 2; \sin^2 \frac{\ell}{2})$	Δ_1	Δ_2	t	$\log F(-\frac{1}{\delta}, \frac{7}{\delta}; 2; \sin^2 \frac{\ell}{2})$	Δ_1	Δ_2	t	$\log F(\frac{1}{\delta}, \frac{5}{\delta}; 2; \sin^2 \frac{\ell}{2})$	Δ_1	Δ_2	t	$\log F(-\frac{1}{\delta}, \frac{7}{\delta}; 2; \sin^2 \frac{\ell}{2})$	Δ_1	Δ_2
0°	0.0000000	+ 23	+ 46	0°	0.0000000	- 32	- 64	68°	0.0105613	+ 3105	+ 43	9°	9850690	- 4435	- 65
1	0.0000023	+ 69	+ 46	9°	9999968	- 97	- 65	69	0.0108718	+ 3105	+ 45	9°	9846255	- 4500	- 65
2	0.0000092	+ 115	+ 46	9°	99999871	- 160	- 63	70	0.0111868	+ 3150	+ 42	9°	9841755	- 4565	- 65
3	0.0000207	+ 160	+ 45	9°	99999711	- 225	- 65	71	0.0111560	+ 3192	+ 44	9°	9837190	- 4629	- 64
4	0.0000367	+ 207	+ 47	9°	99999486	- 290	- 64	72	0.0118296	+ 3236	+ 43	9°	9832561	- 4694	- 65
5	0.0000574	+ 253	+ 46	9°	99999196	- 354	- 64	73	0.0121575	+ 3279	+ 44	9°	9827867	- 4759	- 64
6	0.0000827	+ 299	+ 46	9°	99998842	- 418	- 64	74	0.0124898	+ 3323	+ 43	9°	9823108	- 4823	- 66
7	0.0001126	+ 344	+ 45	9°	99998424	- 482	- 65	75	0.0128264	+ 3408	+ 42	9°	9818285	- 4889	- 63
8	0.0001470	+ 390	+ 46	9°	99997942	- 547	- 64	76	0.0131672	+ 3451	+ 43	9°	9813396	- 4952	- 64
9	0.0001860	+ 437	+ 47	9°	99997395	- 611	- 64	77	0.0135123	+ 3494	+ 43	9°	9808444	- 5016	- 65
10	0.0002297	+ 482	+ 45	9°	99996784	- 675	- 64	78	0.0138617	+ 3536	+ 42	9°	9803428	- 5081	- 65
11	0.0002779	+ 528	+ 46	9°	99996109	- 740	- 65	79	0.0142153	+ 3578	+ 42	9°	9798347	- 5145	- 64
12	0.0003307	+ 574	+ 46	9°	99995369	- 804	- 64	80	0.0145731	+ 3621	+ 43	9°	9793202	- 5209	- 64
13	0.0003881	+ 620	+ 46	9°	99994565	- 869	- 65	81	0.0149352	+ 3662	+ 41	9°	9787993	- 5273	- 64
14	0.0004501	+ 666	+ 46	9°	99993696	- 933	- 64	82	0.0153014	+ 3704	+ 42	9°	9782720	- 5336	- 63
15	0.0005167	+ 711	+ 45	9°	99992763	- 997	- 65	83	0.0156718	+ 3746	+ 41	9°	9777384	- 5400	- 64
16	0.0005878	+ 758	+ 47	9°	99991766	- 1062	- 65	84	0.0160464	+ 3787	+ 41	9°	9771984	- 5464	- 64
17	0.0006636	+ 803	+ 45	9°	99990704	- 1126	- 64	85	0.0164251	+ 3829	+ 42	9°	9766520	- 5526	- 62
18	0.0007439	+ 849	+ 46	9°	99989578	- 1191	- 65	86	0.0168080	+ 3869	+ 40	9°	9760994	- 5590	- 62
19	0.0008288	+ 896	+ 47	9°	99988387	- 1255	- 64	87	0.0171949	+ 3909	+ 40	9°	9755404	- 5652	- 62
20	0.0009184	+ 941	+ 45	9°	99987132	- 1320	- 64	88	0.0175858	+ 3951	+ 42	9°	9749752	- 5716	- 62
21	0.0010125	+ 987	+ 46	9°	99985812	- 1384	- 64	89	0.0178089	+ 3991	+ 40	9°	9744036	- 5778	- 62
22	0.0011112	+ 1032	+ 45	9°	99984428	- 1449	- 65	90	0.0183800	+ 4032	+ 41	9°	9738258	- 5840	- 62
23	0.0012144	+ 1079	+ 47	9°	99982979	- 1513	- 64	91	0.0187832	+ 4072	+ 40	9°	9732418	- 5902	- 62
24	0.0013223	+ 1124	+ 45	9°	99981466	- 1578	- 65	92	0.0191904	+ 4110	+ 38	9°	9726516	- 5964	- 61
25	0.0014347	+ 1170	+ 46	9°	99979888	- 1642	- 64	93	0.0196014	+ 4149	+ 39	9°	9720552	- 6025	- 61
26	0.0015517	+ 1215	+ 45	9°	99978246	- 1707	- 65	94	0.0200163	+ 4188	+ 38	9°	9714527	- 6086	- 61
27	0.0016732	+ 1261	+ 46	9°	99976539	- 1771	- 64	95	0.0204351	+ 4226	+ 39	9°	9708441	- 6146	- 60
28	0.0017993	+ 1307	+ 46	9°	99974768	- 1837	- 66	96	0.0208577	+ 4265	+ 38	9°	9702295	- 6208	- 60
29	0.0019300	+ 1357	+ 46	9°	99972931	- 1901	- 64	97	0.0212842	+ 4303	+ 38	9°	9696087	- 6268	- 60
30	0.0020653	+ 1353	+ 46	9°	99971030	- 1965	- 66	98	0.0217145	+ 4342	+ 39	9°	968819	- 6328	- 59
31	0.0022052	+ 1399	+ 45	9°	99969065	- 2031	- 64	99	0.0221487	+ 4379	+ 37	9°	9683491	- 6387	- 59
32	0.0023496	+ 1444	+ 46	9°	99967034	- 2095	- 64	100	0.0225866	+ 4416	+ 37	9°	9677104	- 6447	- 60
33	0.0024986	+ 1490	+ 45	9°	99964939	- 2160	- 65	101	0.0230282	+ 4452	+ 36	9°	9670657	- 6505	- 58
34	0.0026521	+ 1535	+ 46	9°	99962779	- 2224	- 64	102	0.0234734	+ 4488	+ 36	9°	9664152	- 6563	- 58
35	0.0028102	+ 1581	+ 46	9°	99960555	- 2290	- 66	103	0.0239222	+ 4523	+ 35	9°	9657589	- 6620	- 57
36	0.0029729	+ 1627	+ 45	9°	99958265	- 2354	- 64	104	0.0243745	+ 4559	+ 36	9°	9650969	- 6678	- 58
37	0.0031401	+ 1672	+ 46	9°	99955911	- 2419	- 65	105	0.0248304	+ 4593	+ 34	9°	9644291	- 6734	- 56
38	0.0033119	+ 1718	+ 45	9°	99953492	- 2484	- 65	106	0.0252897	+ 4627	+ 34	9°	9637557	- 6790	- 56
39	0.0034882	+ 1763	+ 45	9°	99951008	- 2549	- 65	107	0.0257524	+ 4662	+ 35	9°	9630767	- 6845	- 56
40	0.0036690	+ 1808	+ 46	9°	99948459	- 2613	- 64	108	0.0262186	+ 4696	+ 34	9°	9623922	- 6901	- 56
41	0.0038544	+ 1854	+ 46	9°	99945846	- 2679	- 66	109	0.0266882	+ 4739	+ 33	9°	9617021	- 6955	- 54
42	0.0040444	+ 1900	+ 45	9°	99943167	- 2744	- 65	110	0.0271611	+ 4729	+ 33	9°	9610066	- 7008	- 53
43	0.0042389	+ 1945	+ 45	9°	99940423	- 2808	- 64	111	0.0276373	+ 4762	+ 31	9°	9603058	- 7061	- 53
44	0.0044379	+ 1990	+ 45	9°	99937615	- 2874	- 66	112	0.0281166	+ 4793	+ 32	9°	9595997	- 7113	- 52
45	0.0046414	+ 2035	+ 46	9°	99934741	- 2938	- 64	113	0.0285991	+ 4825	+ 31	9°	9588884	- 7165	- 52
46	0.0048495	+ 2081	+ 44	9°	99931803	- 3004	- 64	114	0.0290847	+ 4856	+ 30	9°	9581719	- 7215	- 50
47	0.0050620	+ 2125	+ 46	9°	99928799	- 3068	- 64	115	0.0295733	+ 4886	+ 28	9°	9574504	- 7263	- 48
48	0.0052791	+ 2171	+ 46	9°	99925731	- 3134	- 65	116	0.0300647	+ 4914	+ 29	9°	9567241	- 7312	- 49
49	0.0055008	+ 2217	+ 44	9°	99922597	- 3199	- 65	117	0.0305590	+ 4943	+ 29	9°	9559929	- 7360	- 48
50	0.0057269	+ 2261	+ 45	9°	99919398	- 3264	- 64	118	0.0310562	+ 4972	+ 27	9°	9552569	- 7405	- 46
51	0.0059575	+ 2351	+ 45	9°	99916134	- 3328	- 66	119	0.0315561	+ 4999	+ 26	9°	9545164	- 7451	- 44
52	0.0061926	+ 2396	+ 45	9°	99912806	- 3394	- 65	120	0.0320586	+ 5025	+ 26	9°	9537713	- 7495	- 44
53	0.0064322	+ 2441	+ 45	9°	99909412	- 3459	- 66	121	0.0325637	+ 5051	+ 24	9°	9530218	- 7539	- 44
54	0.0066763	+ 2486	+ 45	9°	99905953	- 3525	- 64	122	0.0330712	+ 5075	+ 24	9°	9522679	- 7580	- 41
55	0.0069249	+ 2531	+ 45	9°	99902428	- 3589	- 66	123	0.0335811	+ 5099	+ 22	9°	9515099	- 7621	- 41
56	0.0071780	+ 2575	+ 44	9°	99898839	- 3655	- 64	124	0.0340932	+ 5121	+ 23	9°	9507478	- 7660	- 39
57	0.0074355	+ 2620	+ 45	9°	99895184	- 3719	- 66	125	0.0346076	+ 5144	+ 21	9°	9499818	- 7697	- 37
58	0.0076975	+ 2665	+ 45	9°	99891465	- 3785	- 65	126	0.0351241	+ 5165	+ 20	9°	94942121	- 7733	- 36
59	0.0079640	+ 2709	+ 44	9°	99887680	- 3850	- 65	127	0.0356426	+ 5185	+ 19	9°	94848388	- 7767	- 34
60	0.0082349	+ 2753	+ 44	9°	99883830	- 3915	- 65	128	0.0361630	+ 5204	+ 18	9°	9476621	- 7800	- 33
61	0.0085102	+ 2798	+ 45	9°	99879915	- 3980	- 65	129	0.0366852	+ 5222	+ 16	9°	9468821	- 7830	- 30
62	0.0087900	+ 2842	+ 44	9°	99875935	- 4045	- 65	130	0.0372090	+ 5238	+ 15	9°	9460991	- 7859	- 29
63	0.0090742	+ 2886	+ 44	9°	99871890	- 4110	- 65	131	0.0377343	+ 5253	+ 13	9°	9453132	- 7885	- 26
64	0.0093628	+ 2886	+ 44	9°	99867780	- 4175	- 65	132	0.0382609	+ 5266	+ 13	9°	94445247	- 7910	- 25
65	0.0096558	+ 2930	+ 44	9°	99863605	- 4240	- 65	133	0.0387888	+ 5279	+ 11	9°	9437337	- 7934	- 24
66	0.0099532	+ 2974	+ 44	9°	99859365	- 4305									

t	log $F(\frac{1}{\delta}, \frac{5}{\delta}; 2; \sin^2 \frac{t}{2})$	Δ_1	Δ_2	log $F(-\frac{1}{\delta}, \frac{7}{\delta}; 2; \sin^2 \frac{t}{2})$	Δ_1	Δ_2	t	log $F(\frac{1}{\delta}, \frac{5}{\delta}; 2; \sin^2 \frac{t}{2})$	Δ_1	Δ_2	log $F(-\frac{1}{\delta}, \frac{7}{\delta}; 2; \sin^2 \frac{t}{2})$	Δ_1	Δ_2
136°	0.0403785	+ 5314	+ 7	9.9413478	- 7986	- 15	159°	0.0522934	+ 4735	- 68	9.9233425	- 7173	+ 107
137	0.0409099	+ 5319	+ 5	9.9405492	- 7999	- 13	160	0.0527669	+ 4659	- 76	9.9226252	- 7057	+ 116
138	0.0414418	+ 5323	+ 4	9.9397493	- 8008	- 9	161	0.0532328	+ 4576	- 83	9.9219195	- 6929	+ 128
139	0.0419741	+ 5323	+ 0	9.9389485	- 8015	- 7	162	0.0536904	+ 4487	- 89	9.9212266	- 6792	+ 137
140	0.0425064	+ 5323	- 1	9.9381470	- 8018	- 3	163	0.0541391	+ 4389	- 98	9.9205474	- 6641	+ 151
141	0.0430386	+ 5322	- 4	9.9373452	- 8018	0	164	0.0545780	+ 4283	- 106	9.9198833	- 6476	+ 165
142	0.0435704	+ 5318	- 5	9.9365434	- 8014	+ 4	165	0.0550063	+ 4168	- 115	9.9192357	- 6296	+ 180
143	0.0441017	+ 5313	- 8	9.9357420	- 8008	+ 6	166	0.0554231	+ 4042	- 126	9.9186001	- 6102	+ 194
144	0.0446322	+ 5305	- 10	9.9349412	- 7997	+ 11	167	0.0558273	+ 3906	- 136	9.9179959	- 5891	+ 211
145	0.0451617	+ 5295	- 12	9.9341415	- 7983	+ 14	168	0.0562179	+ 3758	- 148	9.9174068	- 5660	+ 231
146	0.0456900	+ 5283	- 16	9.9333432	- 7963	+ 20	169	0.0565937	+ 3595	- 163	9.9168408	- 5407	+ 253
147	0.0462167	+ 5267	- 19	9.9325469	- 7938	+ 25	170	0.0569532	+ 3418	- 177	9.9163001	- 5133	+ 274
148	0.0467415	+ 5248	- 21	9.9317531	- 7908	+ 30	171	0.0572950	+ 3224	- 194	9.9157868	- 4833	+ 300
149	0.0472642	+ 5227	- 25	9.9309623	- 7874	+ 34	172	0.0576174	+ 3011	- 213	9.9153035	- 4502	+ 331
150	0.0477844	+ 5202	- 28	9.9301749	- 7834	+ 40	173	0.0579185	+ 2773	- 238	9.9148533	- 4140	+ 362
151	0.0483018	+ 5174	- 31	9.9293915	- 7789	+ 45	174	0.0581958	+ 2510	- 263	9.9144393	- 3737	+ 403
152	0.0488161	+ 5143	- 35	9.9286126	- 7737	+ 52	175	0.0584468	+ 2216	- 294	9.9140656	- 3289	+ 448
153	0.0493269	+ 5108	- 40	9.9278389	- 7682	+ 55	176	0.0586684	+ 1882	- 334	9.9137367	- 2782	+ 507
154	0.0498337	+ 5068	- 43	9.9270707	- 7617	+ 65	177	0.0588566	+ 1497	- 385	9.9134585	- 2201	+ 581
155	0.0503362	+ 5025	- 48	9.9263090	- 7544	+ 73	178	0.0590063	+ 1035	- 462	9.9132384	- 1514	+ 687
156	0.0508339	+ 4977	- 52	9.9255546	- 7465	+ 79	179	0.0591098	+ 428	- 607	9.9130870	- 624	+ 890
157	0.0513264	+ 4925	- 58	9.9248081	- 7376	+ 89	180	0.0591526			9.9130246		
158	0.0518131	+ 4867	- 64	9.9240705	- 7280	+ 96							