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**Photographic observations of the eclipsing variable Castor C = YY
Geminorum from 1926 Oct. 2 to 1928 Jan. 13**

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COMMUNICATION FROM THE OBSERVATORY AT LEIDEN.

Photographic observations of the eclipsing variable Castor C = YY Geminorum from 1926 Oct. 2 to 1928 Jan. 13, by *H. van Gent*.

1. Between the publication of the note on Castor C in *B. A. N.* 97 and my departure from Leiden to Johannesburg, I took a number of additional plates of this variable, mainly during the minima. These plates have been measured by C. KOOREMAN in the Schilt-photometer. Two later epochs of minimum were determined by P. TH. OOSTERHOFF.

The 14 epochs of minimum used for a least square solution of the period are given in Table 1. The first of these epochs has been taken from *B. A. N.* 97. The apparent period (half the period of revolution) is found to be $^d.4071411 \pm ^d.0000005$ (m. e.). The mean error of a single epoch is $\pm ^d.0015$. No evidence of the orbit being excentric can be found in Table 1 from the O—C's of the odd and even minima.

TABLE I.

J. D.	epoch	O—C
$^d.2424595^4105$	0	— .0010
4791.6548	482	+ 13
4848.6537	622	+ 5
4875.5268	688	+ 23
4916.6466	789	+ 9
4920.3112	798	+ 12
4921.5306	801	— 8
4922.3441	803	— 17
4961.4304	899	— 9
5230.5519	1560	+ 4
5234.6211	1570	— 18
5242.3568	1589	— 18
5687.3656	2682	+ 18
5698.3561	2709	— 4

The phases were then computed from the formula:

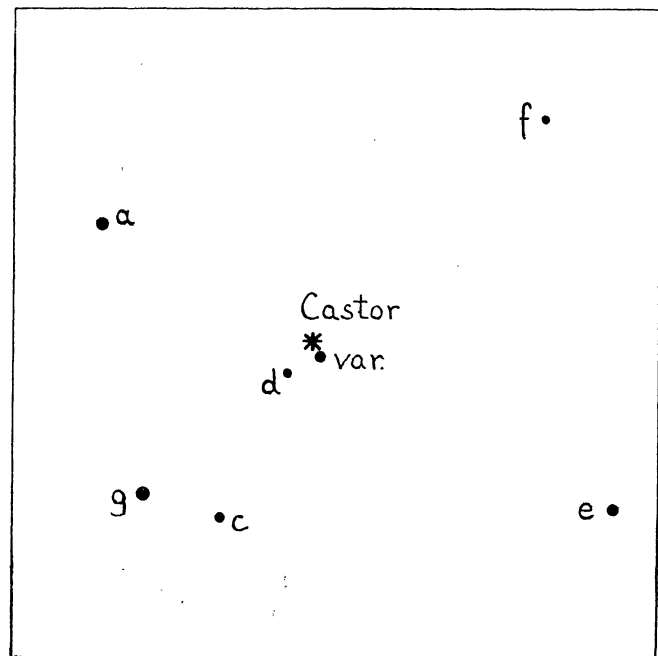
$$\text{phase} = 2.456151 \left(\text{J. D. hel. M. astr. T. Grw.} - 2424595.4105 \right)$$

Altogether 1165 exposures on 34 plates from 21 nights have been used. These are given in Table 2 together with an additional plate containing 11 expo-

sure (near maximum of the variable) taken with a grating placed in front of the objective for the determination of the magnitude scale. The adopted difference in magnitude between the central image and the spectra of the first order is $^m.923$, according to former measures made by SCHILT and HERTZSPRUNG (*B. A. N.* 35, 56 and 68).

Six comparison stars, the positions of which are indicated on Figure 1, were used. The galvanometer

FIGURE 1.



Size of square 5' x 5'

readings of the Schilt photometer were converted into provisional magnitudes by the aid of a table, which had been prepared from other material to represent an average plate. These provisional magnitudes, counted

TABLE 2.

plate no.	date	epoch	number of exposures	middle of first and last exposure						reduction factor for gradation	observed differential magnitude of comparison stars						reduction to max to m.00
				h m s			h m s				<i>g</i>	<i>a</i>	<i>e</i>	<i>c</i>	<i>d</i>	<i>f</i>	
1200	1926 Oct. 2	482	78	2	13	46	5	31	16	.908	— ^m .730	— ^m .655	— ^m .361	.336	.590	.817	— ^m .01
1202	— Nov. 28	622	61	6	36	9	9	21	9	.947	— ^m .660	— ^m .682	— ^m .405	.304	.672	.773	— ^m .20
1203	¹⁾ — Dec. 1		(11)	7	37	24	9	36	10	1.024	— ^m .738	— ^m .631	— ^m .374	.323	.627	.794	.00
1209	— — 25	688	73	5	56	13	8	56	13	1.242	— ^m .686	— ^m .634	— ^m .437	.319	.714	.726	— ^m .32
1217	1927 Febr. 2	784	20	10	6	40	10	56	40	1.018	— ^m .715	— ^m .616	— ^m .432	.349	.638	.774	— ^m .07
1221	— — 4	789	54	11	26	40	13	46	40	.974	— ^m .702	— ^m .630	— ^m .428	.343	.615	.802	— ^m .06
1223	— — 7	796	38	7	16	41	8	51	41	1.030	— ^m .694	— ^m .661	— ^m .398	.336	.650	.769	— ^m .19
1224	— — 8	798	68	4	16	48	7	11	41	1.080	— ^m .694	— ^m .608	— ^m .457	.315	.676	.767	— ^m .19
1228	— — 9	801	84	8	41	41	12	11	41	1.048	— ^m .730	— ^m .648	— ^m .372	.337	.708	.706	²⁾
1229	— — 10	803	62	5	11	42	7	46	42	1.001	— ^m .712	— ^m .639	— ^m .404	.334	.710	.713	— ^m .29
1230	— — 12	808	21	5	41	43	6	31	43	1.346	— ^m .660	— ^m .592	— ^m .556	.409	.773	.626	— ^m .27
1231	— — —	808	21	6	41	43	7	31	43	1.098	— ^m .713	— ^m .684	— ^m .339	.299	.714	.721	— ^m .24
1232	— — —	808	21	7	41	43	8	36	43	1.208	— ^m .681	— ^m .681	— ^m .397	.348	.715	.698	— ^m .28
1234	— March 3	854	1	10	1	42				.656	— ^m .663	— ^m .637	— ^m .453	.295	.656	.801	— ^m .20
1238	— — 16	887	11	11	36	40	12	1	40	1.130	— ^m .700	— ^m .622	— ^m .424	.285	.733	.727	— ^m .26
1239	— — —	887	11	12	9	10	12	34	10	1.134	— ^m .704	— ^m .609	— ^m .438	.302	.696	.754	— ^m .22
1240	— — —	887	11	12	39	28	13	4	10	.964	— ^m .675	— ^m .623	— ^m .479	.357	.704	.715	— ^m .22
1241	— — —	887	11	13	11	40	13	36	40	1.028	— ^m .658	— ^m .665	— ^m .433	.312	.702	.742	— ^m .22
1242	— — 17	889	11	7	11	41	7	36	40	1.100	— ^m .729	— ^m .595	— ^m .439	.343	.699	.722	— ^m .18
1243	— — —	889	11	7	46	40	8	11	40	1.050	— ^m .663	— ^m .598	— ^m .520	.343	.717	.718	— ^m .20
1244	— — —	889	11	8	21	40	8	49	10	1.059	— ^m .686	— ^m .627	— ^m .448	.328	.690	.744	— ^m .20
1245	— — —	889	11	8	56	40	9	21	40	1.062	— ^m .697	— ^m .599	— ^m .462	.310	.717	.733	— ^m .20
1246	— — —	889	16	9	31	40	10	9	10	1.078	— ^m .688	— ^m .647	— ^m .428	.331	.689	.738	— ^m .26
1248	— — 21	899	76	8	56	42	12	4	12	.957	— ^m .669	— ^m .619	— ^m .480	.324	.697	.745	— ^m .15
1254	— May 6	1012	11	12	16	44	12	41	44	1.114	— ^m .690	— ^m .661	— ^m .389	.281	.697	.759	— ^m .23
1255	— — —	1012	11	12	49	14	13	16	44	1.086	— ^m .712	— ^m .629	— ^m .417	.331	.693	.732	— ^m .20
1256	— — —	1012	21	13	31	44	14	21	44	.839	— ^m .691	— ^m .626	— ^m .476	.424	.671	.699	— ^m .20
1304	— Dec. 15	1560	71	5	51	8	8	48	38	.972	— ^m .670	— ^m .665	— ^m .417	.302	.710	.737	— ^m .18
1311	— — 19	1570	72	7	56	7	10	56	7	.975	— ^m .675	— ^m .600	— ^m .499	.336	.746	.693	— ^m .17
1321	— — 27	1589	52	2	31	6	4	38	36	.910	— ^m .705	— ^m .689	— ^m .349	.325	.663	.755	— ^m .22
1345	— — 29	1594	74	3	1	31	6	6	31	.903	— ^m .689	— ^m .739	— ^m .311	.322	.707	.707	— ^m .28
1348	1928 Jan. 11	1626	21	4	6	0	4	56	0	.846	— ^m .711	— ^m .683	— ^m .332	.282	.656	.789	— ^m .15
1349	— — —	1626	21	4	58	30	5	48	30	.837	— ^m .729	— ^m .694	— ^m .320	.337	.723	.683	— ^m .20
1350	— — —	1626	11	5	53	30	6	18	30	.949	— ^m .693	— ^m .653	— ^m .418	.344	.769	.652	— ^m .20
1353	— — 13	1631	19	5	15	59	6	3	29	.977	— ^m .704	— ^m .660	— ^m .383	.318	.682	.746	— ^m .29

¹⁾ taken with a grating in front of the objective. ²⁾ —^m.10 at the beginning, gradually changing to —^m.28 at the end.

from the mean magnitude of the comparison stars as zeropoint, were then multiplied by a factor for gradation, different for each plate, in order to reduce them to the correct scale of magnitude. These factors, given in the 7th column of Table 2 are thus to be considered as the reciprocal relative gradation of the plate in question. ³⁾ The resulting differential magnitudes of the comparison stars for each plate are given in the columns 8 to 13 of Table 2. The mean values are for the star *g*: —^m.695, *a*: —^m.643, *e*: —^m.419, *c*: +^m.328, *d*: +^m.692, *f*: +^m.736. There still remained systematic differences between the plates in the maximum brightness of the variable. Accordingly, for each plate a constant was added to the derived magnitudes of the variable, in order to reduce the maximum brightness in every case to zero magnitude. The reduction constants adopted for this purpose are

³⁾ The mean deviation of a plate from the mean gradation is about ± 11 per cent.

given in the last column of Table 2. Their mean value is —^m.205. Accordingly the variable is at maximum brightness found ^m.205 darker than the mean of the six comparison stars.

It should be remembered that the variable is so near to Castor that its surroundings are subject to variable fogging according to the haziness of the atmosphere and that the yellow colour of Castor C is probably considerably different from that of the average comparison star. The greatest hour angle at which an exposure was made that has been used is 6^h51^m51^s past the meridian. The corresponding height of Castor above the horizon at Leiden is 17°·6. Systematic errors of the kind described above are therefore not surprising.

The results thus obtained for each of the 1166 exposures are given in Table 3. The normal exposure time was 140 sec., with 10 sec. between two consecutive exposures. Small deviations, merely of an accidental character, occur now and then from this rule.

TABLE 3.

J. D.	phase	Δm	J. D.	phase	Δm	J. D.	phase	Δm	J. D.	phase	Δm
plate no. 1200			d	P	m	d	P	m	d	P	m
2424791			·6632	·026	+ 45	·6736	·052	+ 24	·5683	·110	+ 03
d	P	m	·6650	·031	+ 43	·6753	·057	+ 25	·5700	·114	0
·5490	·746	+ 05	·6667	·035	+ 43	·6771	·061	+ 25	·5718	·118	+ 8
·5507	·750	— 3	·6684	·039	+ 34	·6788	·065	+ 7	·5735	·123	+ 3
·5524	·754	+ 1	·6702	·043	+ 34	·6823	·074	+ 14	·5752	·127	+ 3
·5541	·758	— 2	·6719	·048	+ 30	·6840	·078	+ 8	·5770	·131	— 2
·5559	·763	— 3	·6736	·052	+ 27	·6857	·082	+ 11	·5787	·135	+ 7
·5576	·767	+ 2	·6753	·056	+ 22	·6874	·086	+ 12	·5804	·140	— 2
·5593	·771	— 4	·6771	·060	+ 21	·6892	·091	+ 8	·5822	·144	— 3
·5611	·775	+ 1	·6788	·065	+ 19	·6909	·095	+ 12	·5839	·148	0
·5628	·780	— 2	·6805	·069	+ 19	·6926	·099	+ 9	·5856	·152	+ 4
·5645	·784	— 6	·6823	·073	+ 22	·6944	·104	+ 7	·5873	·157	+ 4
·5663	·788	— 6	·6840	·077	+ 13				·5891	·161	+ 1
·5680	·792	+ 2	·6857	·082	+ 15	plate no. 1209			·5908	·165	— 3
·5697	·797	— 4				2424875			·5925	·169	— 5
·5715	·801	— 3	plate no. 1202			d	P	m	·5943	·174	— 2
·5732	·805	+ 5	2424848			·4800	·893	+ 03	·5960	·178	— 1
·5749	·809	+ 4	d	P	m	·4817	·897	+ 3	·5977	·182	— 8
·5767	·814	— 4	·5801	·823	— 01	·4835	·902	— 2	·5995	·186	— 2
·5784	·818	— 6	·5818	·827	+ 5	·4852	·906	— 3	·6012	·191	— 3
·5801	·822	+ 0	·5836	·831	+ 7	·4869	·910	+ 7	·6029	·195	— 2
·5819	·827	+ 4	·5853	·836	+ 4	·4887	·914	+ 5	·6047	·199	— 1
·5836	·831	+ 5	·5870	·840	+ 4	·4904	·919	+ 3			
·5853	·835	— 1	·5888	·844	— 3	·4921	·923	+ 4	plate no. 1217		
·5870	·839	+ 1	·5905	·848	— 7	·4939	·927	+ 9	2424914		
·5888	·844	+ 3	·5922	·852	— 4	·4956	·931	+ 9	d	P	m
·5905	·848	+ 2	·5940	·857	— 3	·4973	·935	+ 11	·5467	·847	— 03
·5922	·852	+ 3	·5957	·861	— 3	·4992	·940	+ 8	·5484	·851	— 3
·5940	·856	+ 3	·5974	·865	+ 1	·5008	·944	+ 14	·5501	·855	+ 5
·5957	·860	+ 3	·5991	·869	— 1	·5025	·948	+ 16	·5519	·859	+ 1
·5974	·865	— 3	·6009	·874	— 3	·5042	·952	+ 13	·5536	·864	— 1
·5992	·869	+ 1	·6026	·878	— 1	·5060	·957	+ 18	·5553	·868	+ 2
·6009	·873	+ 4	·6043	·882	+ 3	·5077	·961	+ 16	·5571	·872	— 2
·6026	·877	+ 1	·6061	·887	+ 4	·5094	·965	+ 21	·5588	·876	— 3
·6044	·882	+ 1	·6078	·891	+ 1	·5112	·970	+ 24	·5605	·881	— 6
·6061	·886	— 8	·6095	·895	— 2	·5129	·974	+ 29	·5623	·885	+ 1
·6078	·890	+ 2	·6113	·899	0	·5146	·978	+ 23	·5640	·889	0
·6096	·895	0	·6130	·904	+ 7	·5164	·982	+ 35	·5657	·893	+ 4
·6113	·899	— 1	·6217	·925	+ 13	·5181	·987	+ 44	·5674	·898	+ 2
·6130	·903	— 5	·6234	·929	+ 8	·5198	·991	+ 48	·5692	·902	0
·6147	·907	— 4	·6251	·933	+ 8	·5216	·995	+ 44	·5709	·906	+ 4
·6165	·912	— 6	·6269	·938	+ 16	·5233	·999	+ 51	·5726	·910	+ 10
·6182	·916	+ 6	·6286	·942	+ 15	·5250	·004	+ 54	·5761	·919	+ 11
·6199	·920	+ 10	·6303	·946	+ 21	·5267	·008	+ 52	·5778	·923	+ 11
·6217	·924	+ 4	·6320	·950	+ 22	·5285	·012	+ 52	·5796	·928	+ 12
·6234	·929	+ 11	·6338	·955	+ 27	·5302	·016	+ 49	·5813	·932	+ 25
·6251	·933	+ 12	·6355	·959	+ 28	·5319	·020	+ 44			
·6269	·937	+ 8	·6372	·963	+ 33	·5337	·025	+ 38	plate no. 1221		
·6286	·941	+ 17	·6390	·967	+ 33	·5354	·029	+ 36	2424916		
·6303	·945	+ 14	·6407	·972	+ 31	·5371	·033	+ 31	d	P	m
·6321	·950	+ 15	·6424	·976	+ 43	·5389	·038	+ 33	·5965	·881	— 06
·6338	·954	+ 21	·6442	·980	+ 48	·5406	·042	+ 34	·5983	·886	— 7
·6355	·958	+ 22	·6459	·984	+ 59	·5423	·046	+ 25	·6000	·890	— 1
·6373	·963	+ 39	·6476	·989	+ 52	·5441	·050	+ 25	·6017	·894	— 5
·6390	·967	+ 34	·6494	·993	+ 57	·5458	·055	+ 25	·6035	·899	— 1
·6407	·971	+ 42	·6511	·997	+ 51	·5475	·059	+ 15	·6052	·903	— 1
·6424	·975	+ 23	·6528	·001	+ 55	·5493	·063	+ 23	·6121	·920	— 1
·6442	·980	+ 36	·6546	·006	+ 61	·5510	·067	+ 15	·6138	·924	+ 2
·6459	·984	+ 44	·6563	·010	+ 60	·5527	·072	+ 10	·6156	·928	+ 4
·6476	·988	+ 45	·6597	·018	+ 54	·5545	·076	+ 15	·6173	·932	+ 5
·6494	·992	+ 56	·6615	·023	+ 43	·5562	·080	+ 10	·6190	·937	+ 9
·6511	·997	+ 63	·6632	·027	+ 42	·5579	·084	+ 9	·6208	·941	+ 9
·6563	·009	+ 60	·6649	·031	+ 37	·5596	·088	+ 14	·6225	·945	+ 16
·6580	·013	+ 55	·6667	·035	+ 42	·5614	·093	+ 10	·6242	·949	+ 18
·6598	·018	+ 48	·6684	·040	+ 40	·5631	·097	+ 5	·6260	·954	+ 26
·6615	·022	+ 44	·6701	·044	+ 30	·5648	·101	+ 8	·6277	·958	+ 28
			·6719	·048	+ 30	·5666	·106	— 2			

TABLE 3 (continued).

J. D.	phase	Δm	J. D.	phase	Δm	J. D.	phase	Δm	J. D.	phase	Δm
d	P	m	d	P	m	d	P	m	d	P	m
6294	962	+ 35	4601	915	- 08	3794	173	+ 04	5498	047	+ 19
6312	967	+ 37	4618	919	+ 2	3811	177	- 1	5515	052	+ 21
6329	971	+ 38	4636	923	- 3	3829	181	+ 6	5532	056	+ 17
6346	975	+ 42	4653	928	- 3	3846	185	- 1	5549	060	+ 13
6363	979	+ 47	4670	932	+ 4	3863	190	+ 2	5567	064	+ 14
6381	983	+ 45	4688	936	+ 9	3881	194	+ 8	5584	068	+ 13
6398	988	+ 54	4705	940	+ 9	3898	198	+ 3	5601	073	+ 2
6415	992	+ 56	4722	944	+ 11	3915	202	+ 2	5619	077	+ 2
6433	996	+ 60	4740	949	+ 19	3932	207	- 2	5636	081	+ 10
6450	000	+ 56	4757	953	+ 23	3950	211	- 3	5653	085	+ 3
6467	005	+ 52	4774	957	+ 26	3967	215	- 11	5671	090	- 5
6485	009	+ 52	4791	961	+ 30	3984	219	+ 3	5688	094	+ 1
6502	013	+ 52	4809	966	+ 41	4002	224	- 8	5705	098	- 1
6519	017	+ 43				4019	228	- 2	5723	103	- 3
6537	022	+ 51	plate no. 1224			4036	232	- 10	5740	107	0
6554	026	+ 52				4054	237	+ 2	5757	111	- 3
6571	030	+ 50	2424920			4071	241	- 5	5775	115	- 6
6589	035	+ 46	d	P	m	4088	245	+ 2	5792	120	- 9
6606	039	+ 35	2877	947	+ 12				5809	124	- 1
6623	043	+ 32	2894	952	+ 12	plate no. 1228			5826	128	- 1
6641	047	+ 29	2911	956	+ 13	2424921			5844	132	- 6
6658	052	+ 29	2928	960	+ 18	d	P	m	5861	137	+ 1
6675	056	+ 37	2946	964	+ 23	4684	847	+ 05	5878	141	+ 1
6689	059	+ 19	2963	969	+ 26	4701	852	+ 7	5896	145	+ 4
6710	064	+ 15	2980	973	+ 27	4718	856	+ 5	5913	149	+ 3
6727	068	+ 9	2998	977	+ 36	4736	860	- 2	5930	153	+ 4
6744	073	+ 13	3015	981	+ 40	4753	864	+ 6	5948	158	+ 3
6762	077	+ 13	3032	986	+ 36	4770	869	- 1	5965	162	+ 5
6779	081	+ 10	3049	990	+ 46	4788	873	- 2	5982	166	+ 12
6796	085	+ 12	3067	994	+ 49	4805	877	- 2	6000	171	0
6814	090	+ 14	3084	998	+ 37	4822	881	+ 1	6017	175	- 2
6831	094	+ 10	3101	002	+ 43	4840	886	- 3	6034	179	+ 4
6848	098	+ 5	3119	007	+ 52	4857	890	- 2	6052	183	+ 5
6866	103	+ 3	3136	011	+ 47	4874	894	- 11	6069	188	- 6
6883	107	+ 4	3153	015	+ 43	4892	899	0	6086	192	- 1
6900	111	- 3	3171	020	+ 41	4909	903	0	6103	196	- 4
6918	115	+ 7	3188	024	+ 40	4926	907	- 8	6121	200	- 1
6935	120	+ 9	3205	028	+ 35	4943	911	+ 7	6138	205	+ 1
			3223	032	+ 33	4961	915	+ 1			
plate no. 1223			3240	037	+ 34	4978	920	+ 7	plate no. 1229		
2424919			3257	041	+ 29	4995	924	+ 7	2424922		
d	P	m	3275	045	+ 13	5013	928	+ 6	d	P	m
4151	804	- 05	3292	049	+ 26	5030	932	+ 9	3202	940	+ 01
4168	808	- 1	3309	054	+ 22	5047	937	+ 16	3219	944	+ 5
4185	813	+ 3	3327	058	+ 14	5065	941	+ 17	3236	948	+ 4
4203	817	- 3	3344	062	+ 14	5082	945	+ 16	3254	952	+ 11
4220	821	+ 2	3361	066	+ 6	5117	954	+ 34	3271	957	+ 21
4237	825	+ 2	3378	071	+ 12	5134	958	+ 42	3288	961	+ 19
4255	830	0	3396	075	+ 5	5151	962	+ 49	3306	965	+ 20
4272	834	+ 1	3413	079	+ 9	5169	967	+ 43	3323	969	+ 22
4289	838	+ 2	3430	083	+ 7	5186	971	+ 36	3340	973	+ 28
4307	843	- 1	3448	088	- 2	5203	975	+ 32	3358	978	+ 38
4324	847	- 3	3482	096	- 1	5220	979	+ 36	3392	986	+ 39
4341	851	- 4	3500	100	- 3	5238	984	+ 48	3410	991	+ 47
4359	855	+ 1	3517	105	- 2	5255	988	+ 48	3427	995	+ 41
4376	859	0	3534	109	0	5272	992	+ 55	3444	999	+ 37
4393	864	- 3	3552	113	+ 7	5290	996	+ 62	3461	003	+ 36
4411	868	- 1	3569	117	- 1	5307	000	+ 63	3479	008	+ 41
4428	872	- 3	3586	122	+ 4	5324	005	+ 54	3496	012	+ 39
4445	876	- 4	3603	134	+ 8	5342	009	+ 60	3513	016	+ 24
4462	881	- 3	3620	139	0	5359	013	+ 51	3531	020	+ 22
4480	885	+ 2	3638	143	- 7	5376	017	+ 45	3548	025	+ 25
4497	889	+ 8	3655	147	+ 3	5394	022	+ 53	3565	029	+ 26
4512	893	+ 2	3673	151	+ 3	5411	026	+ 40	3583	033	+ 22
4529	897	+ 2	3690	156	0	5428	030	+ 33	3600	037	+ 14
4546	901	- 3	3707	160	+ 3	5446	035	+ 30	3617	042	+ 24
4563	905	- 14	3725	164	- 3	5463	039	+ 27	3635	046	+ 24
4580	911	- 3	3742	169	+ 5	5480	043	+ 19	3652	050	+ 17
			3759								
			3777								

TABLE 3 (continued).

J. D.	phase	Δm	J. D.	phase	Δm	J. D.	phase	Δm	J. D.	phase	Δm
d	P	m	d	P	m	d	r	m	plate no. 1244	P	m
'3669	'054	+ '11	'3822	'004	+ '35	'5157	'929	+ '05		'987	+ '46
'3687	'059	+ '11	'3839	'008	+ '40	'5174	'933	+ '12	d	'991	+ '53
'3704	'063	+ '11	'3856	'013	+ '25	'5192	'937	+ '12	'3536	'996	+ '53
'3721	'067	+ '11	'3873	'017	+ '33	'5209	'942	+ '10	'3553	'000	+ '51
'3738	'071	+ '9	'3891	'021	+ '46	'5226	'946	+ '14	'3571	'004	+ '53
'3756	'076	+ '2	'3908	'025	+ '39	'5244	'950	+ '11	'3588	'012	+ '53
'3773	'080	+ '8	'3925	'029	+ '24	'5261	'954	+ '24	'3605	'017	+ '48
'3790	'084	- '1	'3943	'034	+ '44	'5278	'959	+ '15	'3640	'021	+ '29
'3808	'088	+ '3	'3960	'038	+ '20	'5296	'963	+ '23	'3657	'025	+ '40
'3825	'093	+ '5	'3977	'042	+ '25	'5313	'967	+ '24	'3675	'029	+ '38
'3842	'097	+ '5	'3995	'047	+ '30				'3692	'034	+ '31
'3860	'101	+ '1	'4012	'051	+ '24	plate no. 1240			'3709		
'3877	'105	+ '1	'4029	'055	+ '20	d	P	m	'3727		
'3894	'110	- '8	'4047	'059	+ '10	'5350	'976	+ '28	plate no. 1245		
'3912	'114	+ '8	'4064	'064	+ '10	'5365	'980	+ '40	d	P	m
'3928	'118	- '12	'4081	'068	+ '17	'5382	'984	+ '41	'3779	'047	+ '27
'3946	'122	- '1	'4099	'072	+ '16	'5399	'988	+ '45	'3790	'051	+ '20
'3964	'127	+ '5	'4116	'076	+ '1	'5417	'993	+ '47	'3813	'055	+ '26
'3981	'131	+ '3	plate no. 1232			'5434	'997	+ '47	'3830	'059	+ '20
'3998	'135	+ '1	d	P	m	'5451	'001	+ '54	'3848	'064	+ '14
'4016	'140	+ '8	'4185	'093	+ '18	'5469	'006	+ '42	'3865	'068	+ '12
'4033	'144	+ '11	'4202	'098	+ '24	'5486	'010	+ '58	'3882	'072	+ '13
'4050	'148	+ '10	'4220	'102	+ '9	'5503	'014	+ '59	'3900	'076	+ '13
'4067	'152	+ '1	'4237	'106	+ '12	'5521	'018	+ '48	'3917	'080	+ '9
'4085	'156	0	'4254	'110	+ '7	plate no. 1241			'3934	'085	+ '4
'4102	'161	- '1	'4272	'115	- '14	d	P	m	'3952	'089	+ '5
'4119	'165	- '13	'4289	'119	+ '3	'5573	'031	+ '63	plate no. 1246		
'4137	'169	- '7	'4306	'123	+ '1	'5590	'035	+ '32	d	P	m
'4154	'173	- '10	'4324	'127	+ '7	'5607	'039	+ '36	'4021	'106	+ '01
'4171	'178	- '4	'4341	'132	+ '8	'5625	'044	+ '17	'4038	'110	- '2
'4189	'182	- '2	'4358	'136	- '6	'5642	'048	+ '25	'4056	'115	+ '1
'4206	'186	- '8	'4376	'140	- '14	'5659	'052	+ '23	'4073	'119	- '3
'4223	'190	- '1	'4393	'144	- '6	'5676	'056	+ '19	'4090	'123	- '1
'4241	'195	+ '3	'4415	'157	- '12	'5694	'061	+ '10	'4108	'127	- '7
'4258	'199	+ '7	'4462	'161	- '11	'5711	'065	+ '17	'4125	'132	+ '2
'4275	'203	+ '3	'4479	'166	+ '5	'5728	'069	- '5	'4142	'136	- '2
plate no. 1230			'4497	'170	- '4	'5746	'074	- '9	'4159	'140	+ '2
2424924			'4514	'174	+ '3	plate no. 1242			'4177	'144	+ '2
d	P	m	'4531	'178	+ '2	2424957			'4194	'149	+ '2
'3354	'889	- '06	'4549	'183	+ '13	d	P	m	'4211	'153	+ '3
'3371	'893	+ '3	'4566	'187	+ '5	'3051	'868	+ '05	'4229	'157	+ '6
'3389	'898	+ '3	plate no. 1234			'3069	'872	- '5	'4246	'161	+ '1
'3406	'902	+ '4	2424943			'3086	'876	0	'4263	'165	+ '1
'3423	'906	+ '16	d	P	m	'3103	'881	+ '2	'4281	'170	+ '1
'3441	'911	+ '19	'4623	'868	- '12	'3121	'885	0	plate no. 1248		
'3458	'915	+ '20	plate no. 1238			'3138	'889	0	2424961		
'3475	'919	+ '11	2424956			'3155	'893	0	d	P	m
'3493	'923	+ '11	d	P	m	'3173	'898	- '3	'3666	'843	- '04
'3510	'928	+ '13	'4915	'863	- '06	'3190	'902	- '1	'3683	'848	- '2
'3527	'932	+ '15	'4932	'874	+ '3	'3207	'906	- '3	'3700	'852	+ '6
'3545	'936	+ '9	'4949	'878	+ '0	'3225	'911	0	'3718	'856	- '1
'3562	'940	+ '12	'4967	'882	- '1	plate no. 1243			'3735	'860	+ '1
'3579	'944	0	'4984	'886	- '1	d	P	m	'3752	'865	- '4
'3596	'949	- '4	'5001	'891	+ '1	'3294	'927	- '02	'3770	'869	- '4
'3614	'953	+ '5	'5019	'895	+ '3	'3311	'932	+ '1	'3787	'873	- '2
'3631	'957	+ '11	'5036	'899	+ '3	'3328	'936	+ '10	'3804	'877	- '4
'3648	'961	+ '8	'5053	'903	+ '1	'3346	'940	+ '11	'3822	'882	- '3
'3666	'966	+ '42	'5070	'908	+ '3	'3363	'944	+ '18	'3839	'886	- '4
'3683	'970	+ '42	'5088	'912	+ '4	'3380	'949	+ '21	'3856	'890	+ '2
'3700	'974	+ '28	plate no. 1239			'3398	'953	+ '21	'3874	'895	- '2
plate no. 1231			d	P	m	'3415	'957	+ '30	'3891	'899	- '3
d	P	m	'5140	'925	+ '06	'3432	'961	+ '37	'3908	'903	- '4
'3770	'991	+ '59				'3450	'966	+ '38	'3925	'907	+ '4
'3787	'996	+ '42				'3467	'970	+ '37	'3943	'911	+ '6
'3804	'000	+ '43									

TABLE 3 (continued).

J. D.	phase	Δm	J. D.	phase	Δm	J. D.	phase	Δm	J. D.	phase	Δm
d	P	m	d	P	m	d	P	m	d	P	m
'3960	'916	+ '03	'3821	'864	+ '07	'5353	'962	+ '20	'5972	'939	+ '19
'3977	'920	+ 6	'3838	'869	0	'5370	'967	+ 27	'5989	'943	+ 16
'3995	'924	+ 8	'3856	'873	+ 2	'5387	'971	+ 40	'6007	'948	+ 18
'4012	'928	+ 10	'3873	'877	- 3	'5405	'975	+ 39	'6024	'952	+ 25
'4029	'933	+ 9	'3890	'881	+ 2	'5422	'979	+ 45	'6041	'956	+ 22
'4047	'937	+ 9	'3907	'886	- 2	'5439	'984	+ 43	'6059	'960	+ 24
'4064	'941	+ 15	'3925	'890	+ 4	'5456	'988	+ 44	'6076	'965	+ 32
'4081	'945	+ 17				'5491	'996	+ 49	'6093	'969	+ 37
'4099	'950	+ 16	plate no. 1255			'5508	'000	+ 54	'6111	'973	+ 42
'4116	'954	+ 19	d	P	m	'5526	'005	+ 48	'6128	'977	+ 41
'4133	'958	+ 18	'3977	'903	+ '11	'5543	'009	+ 46	'6145	'982	+ 45
'4151	'963	+ 32	'3994	'907	+ 8	'5560	'013	+ 38	'6162	'986	+ 43
'4168	'967	+ 41	'4011	'911	+ 9	'5578	'018	+ 46	'6180	'990	+ 47
'4185	'971	+ 39	'4029	'916	+ 7	'5595	'022	+ 48	'6197	'994	+ 51
'4203	'975	+ 42	'4046	'920	+ 10	'5612	'026	+ 38	'6214	'998	+ 57
'4220	'980	+ 34	'4063	'924	+ 11	'5630	'030	+ 42	'6232	'003	+ 50
'4237	'984	+ 41	'4081	'928	+ 18	'5647	'035	+ 36	'6249	'007	+ 47
'4254	'988	+ 50	'4098	'932	+ 18	'5664	'039	+ 33	'6266	'011	+ 44
'4272	'992	+ 48	'4124	'939	+ 17	'5682	'043	+ 27	'6284	'016	+ 50
'4289	'996	+ 54	'4150	'945	+ 22	'5699	'047	+ 22	'6301	'020	+ 45
'4306	'001	+ 57	'4167	'949	+ 26	'5716	'052	+ 17	'6318	'024	+ 43
'4324	'005	+ 55				'5733	'056	+ 18	'6336	'028	+ 39
'4341	'009	+ 44	plate no. 1256			'5751	'060	+ 11	'6353	'033	+ 29
'4358	'013	+ 43	d	P	m	'5768	'064	+ 10	'6370	'037	+ 24
'4376	'018	+ 46	'4271	'975	+ '47	'5785	'069	+ 7	'6388	'041	+ 27
'4393	'022	+ 41	'4288	'979	+ 47	'5803	'073	+ 7	'6405	'045	+ 25
'4410	'026	+ 34	'4306	'984	+ 49	'5820	'077	+ 5	'6422	'050	+ 8
'4428	'031	+ 33	'4323	'988	+ 59	'5837	'081	+ 6	'6439	'054	+ 11
'4445	'035	+ 34	'4340	'992	+ 56	'5855	'086	- 1	'6457	'058	+ 12
'4462	'039	+ 27	'4358	'996	+ 49	'5872	'090	- 1	'6474	'062	+ 13
'4480	'043	+ 20	'4375	'001	+ 59	'5889	'094	- 4	'6491	'067	+ 14
'4497	'048	+ 22	'4392	'005	+ 45	'5907	'098	+ 8	'6509	'071	+ 15
'4514	'052	+ 22	'4410	'009	+ 51	'5924	'103	0	'6526	'075	+ 15
'4531	'056	+ 14	'4427	'013	+ 50	'5941	'107	- 2	'6543	'079	+ 14
'4549	'060	+ 21	'4444	'017	+ 45	'5959	'111	+ 2	'6561	'084	+ 6
'4566	'064	+ 20	'4461	'022	+ 44	'5976	'115	+ 3	'6578	'088	+ 8
'4583	'069	+ 15	'4479	'026	+ 43	'5993	'120	+ 8	'6595	'092	+ 6
'4601	'073	+ 14	'4496	'030	+ 42	'6010	'124	+ 3	'6613	'096	+ 5
'4618	'077	+ 16	'4513	'034	+ 30	'6028	'128	+ 5	'6630	'101	+ 9
'4635	'081	+ 11	'4531	'039	+ 23	'6045	'132	+ 2	'6647	'105	+ 6
'4653	'086	+ 4	'4548	'043	+ 25	'6062	'137	+ 1	'6664	'109	+ 8
'4670	'090	+ 5	'4565	'047	+ 13	'6080	'141	+ 2	'6682	'113	+ 8
'4687	'094	+ 4	'4583	'052	+ 29	'6097	'145	+ 7	'6699	'118	+ 1
'4705	'099	+ 3	'4600	'056	+ 17	'6114	'149	+ 4	'6717	'122	+ 2
'4722	'103	+ 1	'4617	'060	+ 14	'6132	'154	- 5	'6734	'126	+ 3
'4739	'107	+ 10				'6149	'158	- 3	'6751	'130	+ 5
'4757	'111	- 3	plate no. 1304			'6166	'162	- 7	'6768	'135	+ 3
'4774	'116	- 7				'6184	'167	- 1	'6786	'139	0
'4791	'120	+ 1	2425230			'6201	'171	- 5	'6803	'143	+ 1
'4808	'124	+ 3	d	P	m	'6218	'175	- 3	'6820	'147	+ 4
'4826	'128	+ 8	'5041	'886	- '06	'6236	'179	- 1	'6838	'152	- 1
'4843	'133	+ 8	'5058	'890	- 5	'6253	'183	- 1	'6855	'156	- 3
'4860	'137	- 1	'5076	'894	- 5	'6270	'188	+ 11	'6872	'160	- 8
'4878	'141	- 1	'5093	'899	- 2				'6890	'165	- 7
'4895	'145	+ 1	'5110	'903	- 1	plate no. 1311			'6907	'169	- 7
'4912	'149	- 1	'5127	'907	- 3				'6924	'173	- 6
'4930	'154	+ 7	'5145	'911	- 4	2425234			'6942	'177	+ 3
'4947	'158	+ 1	'5162	'916	- 6	d	P	m	'6959	'181	- 1
'4964	'162	0	'5179	'920	- 4	'5799	'897	+ '03	'6976	'186	- 1
			'5197	'924	- 1	'5816	'901	- 4	'6994	'190	- 2
plate no. 1254			'5214	'928	+ 1	'5834	'905	+ 8	'7011	'194	- 7
2425007			'5231	'932	+ 6	'5851	'909	+ 12	'7028	'198	- 3
d	P	m	'5249	'937	+ 5	'5868	'914	+ 13	'7045	'203	- 8
'3752	'848	- '01	'5266	'941	+ 6	'5885	'918	+ 12			
'3769	'852	- 3	'5283	'945	+ 12	'5903	'922	+ 12	plate no. 1321		
'3786	'856	- 6	'5301	'950	+ 14	'5920	'926	+ 12	2425242		
'3804	'860	0	'5318	'954	+ 20	'5937	'930	+ 10	d	P	m
			'5335	'958	+ 26	'5955	'935	+ 11	'3332	'940	+ '03
									'3349	'944	+ 13

TABLE 3 (continued).

J. D.	phase	Δm	J. D.	phase	Δm	J. D.	phase	Δm	J. D.	phase	Δm
d	P	m	d	P	m	d	P	m	d	P	m
'3366	'948	+ '14	'3506	'895	+ '07	'4475	'133	+ '03	'4083	'967	+ '34
'3384	'953	+ '13	'3523	'899	+ '5	'4493	'137	+ '9	'4100	'971	+ '39
'3401	'957	+ '31	'3540	'903	+ '6	'4510	'141	- '5	'4118	'975	+ '39
'3418	'961	+ '31	'3558	'908	- '6	'4527	'146	+ '5	'4135	'979	+ '55
'3436	'965	+ '39	'3575	'912	+ '5	'4545	'150	+ '2	'4152	'984	+ '49
'3453	'970	+ '43	'3592	'916	+ '3	'4562	'154	- '3	'4170	'988	+ '47
'3470	'974	+ '48	'3610	'920	+ '17	'4596	'163	- '2	'4187	'992	+ '49
'3488	'978	+ '37	'3627	'925	+ '24	'4614	'167	- '5	'4204	'996	+ '54
'3505	'982	+ '54	'3644	'929	+ '14	'4631	'171	- '6	'4222	'001	+ '52
'3522	'987	+ '53	'3662	'933	+ '12	'4648	'175	- '8	'4239	'005	+ '52
'3540	'991	+ '54	'3679	'937	+ '19	'4666	'180	+ '5	'4256	'009	+ '50
'3557	'995	+ '55	'3696	'942	+ '20	'4683	'184	+ '8	'4274	'013	+ '42
'3574	'999	+ '64	'3713	'946	+ '23	'4700	'188	- '16	'4291	'018	+ '49
'3592	'004	+ '50	'3731	'950	+ '19	'4718	'193	- '5			
'3609	'008	+ '58	'3748	'954	+ '24	'4735	'197	- '5			
'3626	'012	+ '48	'3765	'958	+ '24	'4752	'201	- '5			
'3643	'016	+ '45	'3783	'963	+ '31	'4770	'205	+ '3			
'3661	'021	+ '40	'3800	'967	+ '30				plate no. 1350		
'3678	'025	+ '42	'3817	'971	+ '33				d	P	m
'3695	'029	+ '39	'3835	'976	+ '31				'4326	'026	+ '45
'3713	'033	+ '26	'3852	'980	+ '27	plate no. 1348			'4346	'030	+ '39
'3730	'038	+ '28	'3869	'984	+ '39				'4360	'035	+ '37
'3747	'042	+ '23	'3887	'988	+ '35	2425257			'4378	'039	+ '38
'3765	'046	+ '26	'3904	'993	+ '50	d	P	m	'4395	'043	+ '33
'3782	'050	+ '20	'3921	'997	+ '46	'3581	'843	- '01	'4412	'047	+ '28
'3799	'055	+ '12	'3941	'002	+ '49	'3598	'847	- '1	'4429	'052	+ '31
'3817	'059	+ '8	'3956	'005	+ '33	'3616	'852	- '5	'4447	'056	+ '18
'3834	'063	+ '11	'3973	'010	+ '29	'3633	'856	- '6	'4464	'060	+ '15
'3851	'067	+ '7	'3990	'014	+ '51	'3650	'860	- '1	'4481	'064	+ '14
'3869	'072	+ '6	'4008	'018	+ '42	'3668	'865	- '1	'4499	'069	+ '14
'3886	'076	+ '5	'4025	'022	+ '33	'3685	'869	0			
'3903	'080	+ '5	'4042	'027	+ '34	'3702	'873	+ '4			
'3920	'084	+ '6	'4060	'031	+ '32	'3720	'877	0			
'3938	'089	+ '5	'4077	'035	+ '35	'3737	'882	+ '3	plate no. 1353		
'3955	'093	- '3	'4094	'039	+ '28	'3754	'886	+ '8			
'3972	'097	0	'4112	'044	+ '31	'3772	'890	+ '5	2425259		
'3990	'101	- '6	'4129	'048	+ '14	'3789	'894	- '4			
'4007	'106	+ '1	'4146	'052	+ '16	'3806	'899	0	d	P	m
'4024	'110	- '1	'4164	'056	+ '10	'3824	'903	+ '4	'4011	'861	- '07
'4042	'114	0	'4181	'061	+ '17	'3841	'907	+ '3	'4028	'865	+ '4
'4059	'118	- '6	'4198	'065	+ '8	'3858	'911	- '1	'4046	'870	- '5
'4076	'123	+ '2	'4216	'069	+ '14	'3875	'915	+ '5	'4063	'874	+ '6
'4094	'127	+ '2	'4233	'073	+ '10	'3893	'920	+ '8	'4080	'878	+ '2
'4111	'131	- '4	'4250	'078	+ '8	'3910	'924	+ '5	'4098	'883	+ '0
'4128	'135	- '6	'4267	'082	+ '8	'3927	'928	+ '1	'4115	'887	+ '5
'4146	'140	+ '10	'4285	'086	+ '11				'4132	'891	+ '1
'4163	'144	+ '2	'4302	'091	- '5	plate no. 1349			'4150	'895	- '3
'4180	'148	+ '9	'4319	'095	- '3	d	P	m	'4167	'899	+ '6
'4197	'152	- '3	'4337	'099	+ '5	'3945	'933	+ '08	'4184	'904	+ '8
'4215	'157	+ '3	'4354	'103	+ '13	'3962	'937	+ '12	'4201	'908	- '8
			'4371	'107	+ '10	'3979	'941	+ '20	'4236	'916	- '14
plate no. 1345			'4389	'112	- '5	'3997	'945	+ '19	'4253	'921	- '8
2425244	P	m	'4406	'116	- '2	'4014	'950	+ '22	'4271	'925	- '9
d	'890	+ '06	'4423	'120	- '10	'4031	'954	+ '27	'4288	'929	- '4
'3488			'4441	'125	- '3	'4049	'958	+ '33	'4305	'933	- '2
			'4458	'129	- '1	'4066	'962	+ '36	'4323	'938	- '1
									'4340	'942	+ '3

The mean error for a single exposure during minimum is found to be ± 0.068 from the differences between two observations following each other in phase.

The observations were now arranged according to phase and divided into groups as indicated in Table 4. Of the 23 larger groups of 50 observations each, 21 are shown graphically in Figure 2. By the aid of a

curve drawn through the points of Figure 2 the phase of minimum was, in the way described in *B. A. N.* 147, p. 179, found to be $P.0024$, while the mean of the phases of the 11 minima between J. D. 2424791 and 5242 of Table 1 is $P.0023$. The mean epoch of the observations of the present paper is:

$$J. D. \text{ hel. M. astr. T. Grw. } 2424989^d \cdot 1169 \pm 0.0004 \text{ (m.e.)},$$

TABLE 4.

number of exposures	phase Δm		number of exposures	phase Δm		number of exposures	phase Δm		number of exposures	phase Δm		number of exposures	phase Δm	
	P	m		P	m		P	m		P	m		P	m
6	.7563	.000	10	.9545	.233	10	.0568	.197	10	.0568	.197	10	.0568	.197
10	.7897	.022	10	.9574	.229	10	.0595	.137	10	.0595	.137	10	.0595	.137
10	.8170	.004	10	.9595	.247	10	.0620	.155	10	.0620	.155	10	.0620	.155
10	.8328	.028	10	.9620	.313	10	.0644	.138	10	.0644	.138	10	.0647	.132
10	.8445	.004	10	.9648	.321	10	.0675	.118	10	.0675	.118	10	.0675	.118
10	.8502	.024	10	.9672	.325	10	.0702	.112	10	.0702	.112	10	.0702	.112
10	.8551	.011	10	.9702	.365	10	.0730	.092	10	.0730	.092	10	.0730	.092
10	.8604	.011	10	.9726	.344	10	.0761	.076	10	.0761	.076	10	.0761	.076
10	.8653	.010	10	.9753	.366	10	.0788	.100	10	.0788	.100	10	.0791	.085
10	.8689	.025	10	.9783	.405	10	.0821	.083	10	.0821	.083	10	.0821	.083
10	.8729	.004	10	.9810	.404	10	.0855	.074	10	.0855	.074	10	.0855	.074
10	.8765	.010	10	.9842	.456	10	.0893	.040	10	.0893	.040	10	.0893	.040
10	.8806	.008	10	.9873	.448	10	.0931	.042	10	.0931	.042	10	.0931	.042
10	.8842	.001	10	.9894	.503	10	.0967	.050	10	.0967	.050	10	.0966	.043
10	.8871	.015	10	.9920	.524	10	.1001	.043	10	.1001	.043	10	.1001	.043
10	.8900	.012	10	.9950	.507	10	.1040	.038	10	.1040	.038	10	.1040	.038
10	.8930	.013	10	.9968	.507	10	.1072	.029	10	.1072	.029	10	.1072	.029
10	.8960	.009	10	.9999	.525	10	.1109	.013	10	.1109	.013	10	.1109	.013
10	.8988	.008	10	.0025	.487	10	.1146	.005	10	.1146	.005	10	.1146	.003
10	.9015	.003	10	.0051	.456	10	.1183	.025	10	.1183	.025	10	.1183	.025
10	.9034	.018	10	.0082	.481	10	.1218	.017	10	.1218	.017	10	.1218	.017
10	.9065	.003	10	.0103	.501	10	.1258	.015	10	.1258	.015	10	.1258	.015
10	.9093	.033	10	.0128	.457	10	.1300	.009	10	.1300	.009	10	.1300	.009
10	.9119	.042	10	.0158	.447	10	.1340	.032	10	.1340	.032	10	.1340	.012
10	.9150	.017	10	.0180	.443	10	.1382	.014	10	.1382	.014	10	.1382	.014
10	.9194	.065	10	.0211	.407	10	.1418	.011	10	.1418	.011	10	.1418	.011
10	.9219	.061	10	.0237	.420	10	.1455	.026	10	.1455	.026	10	.1455	.026
10	.9244	.063	10	.0261	.415	10	.1497	.033	10	.1497	.033	10	.1497	.033
10	.9276	.050	10	.0291	.351	10	.1540	.003	10	.1540	.003	10	.1540	.006
10	.9294	.088	10	.0313	.388	10	.1583	.004	10	.1583	.004	10	.1583	.004
10	.9323	.111	10	.0343	.344	10	.1626	.028	10	.1626	.028	10	.1626	.028
10	.9347	.085	10	.0365	.302	10	.1672	.015	10	.1672	.015	10	.1672	.015
10	.9374	.114	10	.0391	.321	10	.1720	.025	10	.1720	.025	10	.1720	.025
10	.9402	.104	10	.0422	.288	10	.1771	.011	10	.1771	.011	10	.1773	.009
10	.9422	.125	10	.0443	.230	10	.1824	.024	10	.1824	.024	10	.1824	.024
10	.9446	.142	10	.0471	.237	10	.1879	.018	10	.1879	.018	10	.1879	.018
10	.9471	.157	10	.0495	.217	10	.1945	.019	10	.1945	.019	10	.1945	.019
10	.9496	.167	10	.0520	.239	10	.2015	.004	10	.2015	.004	10	.2040	.016
10	.9524	.161	10	.0550	.173	10	.2259	.034	10	.2259	.034	10	.2259	.034

with the epoch 967 in the counting of Table 1.

The 117 smaller groups of Table 4 were then arranged anew according to the phase counted from minimum. Mean results thus obtained are given for 24 groups of about 50 observations each in Table 5. The results for 21 of these groups nearest to minimum are shown graphically in Figure 3.

FIGURE 2.

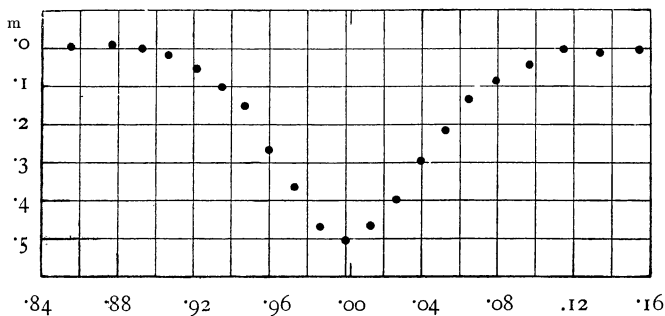
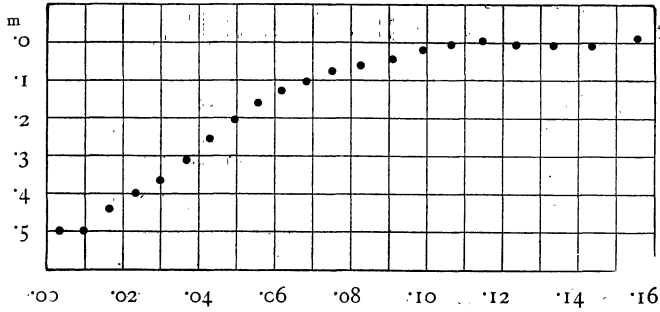


TABLE 5.

number of exposures	phase counted from minimum	mean Δm	number of exposures	phase counted from minimum	mean Δm
50	± .0033	.499	50	± .0826	.060
50	± .0098	.498	50	± .0911	.041
50	± .0162	.440	50	± .0990	.019
50	± .0234	.399	50	± .1065	.004
50	± .0300	.361	50	± .1148	.005
50	± .0367	.311	50	± .1236	.005
50	± .0430	.251	50	± .1335	.005
50	± .0494	.205	50	± .1438	.010
50	± .0555	.160	50	± .1556	.011
50	± .0618	.127	50	± .1717	.000
50	± .0683	.104	50	± .1950	.012
50	± .0752	.075	16	± .2320	.021

FIGURE 3.



2. A new computation of the geometrical elements of the system was now made. No sensible difference in the depth of even and odd minima was noted. The system is assumed to consist of two identical spherical components of uniform surface brightness, revolving in a circular orbit. The unknown quantities

which can now be found from the lightcurve are the inclination of the orbit i , and the ratio r/a between the semidiameters of each component and of the orbit. The relation between the two unknowns is:

$$\left(\frac{\delta}{r}\right)^2 \cdot \left(\frac{r}{a}\right)^2 = 1 - \sin^2 i \cos^2 \zeta \quad (1)$$

in which δ denotes the projected distance of the centres, and ζ the phase angle, counted from the middle of the eclipse as zero point. If we take $(r/a)^2$ and $\sin^2 i$ as the unknowns, this relation is linear in both, and a least square solution to determine $(r/a)^2$ and $\sin^2 i$ was now made. For this purpose the first 16 data from Table 5 (representing 16×50 observations) were collected in the first two columns of Table 6. The third column contains $\sin^2 \zeta = \sin^2(\pi \times \text{phase})$. The fourth column contains the quantity $\alpha =$ the fraction of one disc obscured by the other one, computed from the second

TABLE 6.

1		2		3		4		5		6		7		8		9		10		11		12		13		14	
P		m		$\sin^2 \pi P$		α		$\left(\frac{\delta}{r}\right)^2$		α		$\left(\frac{\delta}{r}\right)^2$		α		$\left(\frac{\delta}{r}\right)^2$		$(7)-(9)$		$\frac{4}{(10)^2}$		$\left(\frac{\delta}{r}\right)^2$		α		O-C	
.0033	.499	.0001075	.7370	.1731	.7252	.1893	.7486	.1581	.0312	4100	.1672	.7415		-	.004												
.0098	.498	.000947	.7358	.1748	.7240	.1911	.7474	.1596	.0315	4030	.1999	.7178		+	15												
.0162	.440	.002588	.6664	.2812	.6540	.3031	.6786	.2606	.0425	2220	.2637	.6767		-	8												
.0234	.399	.005395	.6150	.3777	.6022	.4041	.6278	.3522	.0519	1490	.3728	.6174		-	2												
.0300	.361	.008857	.5658	.4850	.5524	.5168	.5788	.4551	.0617	1050	.5074	.5503		+	7												
.0367	.311	.013234	.4982	.6577	.4842	.6974	.4842	.6974	.0774	667	.6775	.4912		+	5												
.0430	.251	.018139	.4128	.9229	.3982	.9742	.4274	.8737	.1005	395	.8682	.4290		-	11												
.0494	.205	.023830	.3440	1.1805	.3288	1.2437	.3592	1.1200	.1237	261	1.0894	.3671		-	15												
.0555	.160	.030095	.2740	1.4916	.2580	1.5705	.2898	1.4163	.1542	168	1.3330	.3082		-	22												
.0618	.127	.037222	.2208	1.7681	.2044	1.8621	.2370	1.6799	.1822	120	1.6100	.2503		-	18												
.0683	.104	.045339	.1826	1.9943	.1658	2.1025	.1994	1.8917	.2108	90	1.9256	.1938		-	7												
.0752	.075	.054779	.1334	2.3293	.1162	2.4614	.1506	2.2055	.2559	61	2.2925	.1384		-	3												
.0826	.060	.065844	.1076	2.5313	.0900	2.6821	.1248	2.3944	.2877	48	2.7226	.0856		+	12												
.0911	.041	.079699	.0742	2.8305	.0564	3.0147	.0918	2.6660	.3487	33	3.2612	.0359		+	21												
.0990	.019	.093654	.0348	3.2721	.0164	3.5581	.0528	3.0548	.5033	16	3.8037	.0047		+	16												
.1065	.004		.0074	3.7311			.0256	3.4066						+	4												

column; and the fifth column contains the corresponding projected distance of the centres δ/r , in terms of the radius of each component. In the equation (1) the coefficient $\cos^2 \zeta$ is exact, and the uncertainty is wholly in the coefficient $(\delta/r)^2$. Now for each of the points of the lightcurve it was computed how big the change in δ/r was, corresponding to a change of $m \cdot 01$ in Δm , in both directions. Columns 6, 7, 8 and 9 give the results of these computations. Accordingly, weights were given to the equations in the least square solution. These weights are given in column 11. The result of the least square solution for the equation (1) was:

$$.025617 \left(\frac{\delta}{r}\right)^2 = 1 - .995823 \cos^2 \zeta,$$

from which follows: $\frac{r}{a} = .160053$ (157)

and: $i = 86^\circ.3$ (86°·2)

Between brackets have been added the values found for these quantities in B. A. N. 97. It is remarkable how well they agree with the values derived in this paper, although they were derived from observations during one minimum only.

The columns 12 and 13 were now computed with the new values for r/a and i , and the corresponding difference between observed and computed lightcurve in column 14. The mean error of the O-C's is ± 0.014 .

3. The absolute dimensions may again be computed with the aid of the spectrographic data given by JOY and SANFORD in *Ap. J.* 64, p. 250. Taking the maximum separation of the spectral lines of the two components as 240.7 km/sec, the following quantities result:

radius of each component:	$r = 432000$ km
radius of orbit :	$a = 2701000$ km
mass of each component: $\frac{1}{2}(M_1 + M_2) =$	$0.593 \odot$
density :	$\rho = 2.468 \rho_{\odot}$

The absolute visual magnitude of each component is $9^m.15$ (parallax = ".1) (*B. A. N.* 97). Computing the mass from EDDINGTON's mass-luminosity relation

(EDDINGTON, *The internal constitution of the stars*, p. 137), the value $0.593 \odot$ is found, exactly the mass as derived directly from the observations.

4. Comparing the absolute visual magnitude of each component of Castor C with the sun's absolute visual magnitude + $4^m.67$ (parallax = ".1), and taking into account the difference in size, it is found that the surface brightness of Castor C is $3^m.45$ darker than that of the sun. Adopting for the sun an effective temperature of 5741° , and using the table on p. 139 of EDDINGTON, *The intern. const. of the stars* (HERTZSPRUNG's formula), this gives an effective temperature of Castor C of 3400° , in good agreement with its spectrum M. According to the effective wavelengths given by FRANK S. HOGG in *H. B.* 848 the colour index of Castor C in the mean system of DOORN (*B. A. N.* 140) is + $1^m.52$.