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## Photographic measures of six southern variable stars

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## COMMUNICATIONS FROM THE OBSERVATORY AT LEIDEN

### Photographic measures of six southern variable stars, by *C. J. Kooreman*.

The six variable stars AY Pup;  $7^{\text{h}}35^{\text{m}}45^{\text{s}}$ ,  $-25^{\circ}21'9$  (1875); WX Pup;  $7^{\text{h}}46^{\text{m}}44^{\text{s}}$ ,  $-20^{\circ}59'1$  (1875); WW Pup and C.P.D. —  $25^{\circ}2896$  have been measured with the Schilt microphotometer by the writer on plates taken at Johannesburg with the Franklin-Adams camera mainly by Dr. H. VAN GENT. For all variables and their comparison stars the galvanometer readings were converted into provisional magnitudes with the aid of the table of *B.A.N.* No. 318.

The measures of the first four stars have been discussed by Prof. E. HERTZSPRUNG in *B.A.N.* No. 340. The variability of C.P.D. —  $25^{\circ}2896$  was discovered by Dr. H. VAN GENT, while A. BLAAUW will give a discussion of these and other observations in a subsequent number of these publications.

The observations of WW Pup will be discussed by Prof. E. HERTZSPRUNG in a later issue of the *B.A.N.*

The reduced measures are given in the table.

J.D.— 2420000	AY Pup	$7^{\text{h}}35^{\text{m}}45^{\text{s}}$ — $25^{\circ}21'9$	WX Pup	$7^{\text{h}}46^{\text{m}}44^{\text{s}}$ — $20^{\circ}59'1$	WW Pup	C.P.D. — $25^{\circ}2896$
55076121	.46	.39	.31	.26	.40	.67
245716	.08	.38	.31	—	.21	.06
5945	.09	.38	.30	—	.28	.10
314879	.60	.24	.11	.20	.33	.01
5108	.58	.03	.05	.10	.24	.04
325884	.20	.49	.07	.35	.63	.03
615086	.55	.42	.48	.23	.15	.26
5307	.50	.46	.51	.29	.24	.13
625056	.17	.28	.75	.12	.50	.48
5257	.05	.45	.89	.20	.66	.28
645044	.19	.41	1'23	.37	.29	.13
5262	.37	.40	1'30	.38	.25	.05
684948	.23	.32	.28	.14	.39	.14
5170	.34	.28	.19	.16	.19	.13
704507	.40	.02	.46	.22	.40	.41
4736	.19	.12	.45	.21	.46	.58
56133667	.28	.27	.33	.22	.03	.59
3896	.13	.40	.33	.11	.14	.36
145067	.68	.42	.32	.28	.32	.64
5289	.40	.26	.31	.27	.42	.40
153544	.06	.33	.58	.36	.52	.10
3761	.10	.33	.52	.26	.59	.10
162686	.00	.61	.52	.31	.65	.19
414403	.41	.05	.13	.23	.23	.07
4624	.64	.11	.04	—	—	.01
434687	.04	.24	.96	.21	.62	.13
4909	.01	.24	.86	.27	.63	.11
442769	.67	.52	1'22	.29	.33	.13
2991	.52	.58	1'19	.34	.36	.02
3213	.29	.46	1'29	.25	.36	.08
4071	.00	.53	1'28	.25	.52	.10
4290	.08	.45	1'32	.22	.57	.13
4975	.47	.44	1'11	.11	.63	.08
452583	.38	.43	1'23	—	.46	.06
2801	.15	.39	1'15	.26	.52	.12
56462639	.01	.47	.99	—	—	.21
2857	.04	.56	.96	.02	—	.05
3871	.60	.59	1'10	.34	—	.00
4089	.56	.54	1'22	.00	—	.07
4848	.11	.52	.94	.22	.10	.58
5069	.14	.45	.94	.30	.12	.75
5824	.24	.45	.62	.12	.02	.09
492601	.23	.51	.20	.12	.56	.01
2826	.16	.48	.32	.11	.40	.02
3046	.06	.44	.31	.21	.36	.16
3249	.02	.45	.28	.28	.46	.33
3453	.04	.33	.39	.29	.42	.56
3671	.11	.22	.40	.26	.38	.52
503228	.19	.54	.27	.32	.87	.07
3450	.41	.50	.29	.26	.88	.08
4139	—	.58	.32	.20	.82	.05
4357	.17	.50	.32	.23	.80	.07
5036	.01	.50	.29	.02	.80	.61
5254	.03	.46	.19	.17	.69	.41
512578	.18	.41	.61	.19	.36	.10
2796	.28	.45	.69	—	.26	.08
4295	.00	.02	.76	.16	.27	—
4517	.10	.03	.75	.08	.17	.07
522626	.70	.36	.91	.20	.13	.23
2843	.41	.35	.94	.18	.12	.07
3059	.19	.41	—	.06	.14	.05
3276	.08	.48	1'03	.04	.03	.05
3492	.03	.50	.91	.18	.17	.09
3709	.02	.48	.94	.17	.13	.14
3925	.04	—	.95	—	.14	.07
4147	.08	.48	1'00	.22	.16	.23
4366	.14	.43	1'02	.20	.32	.13
4583	.40	.47	.96	.20	.09	.19
4801	.58	.50	.99	.28	.21	.06
5017	.61	.47	.92	.25	.15	.06

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J.D.— 2420000	AY Pup	7h 35m 45s —25° 21' 9"	WX Pup	7h 46m 44s —20° 59' 1"	WW Pup	C.P.D. —25° 28' 96"	J.D.— 2420000	AY Pup	7h 35m 45s —25° 21' 9"	WX Pup	7h 46m 44s —20° 59' 1"	WW Pup	C.P.D. —25° 28' 96"	
5652	42	47	99	30	19	13	5854	51	58	26	19	81	22	
5234	20	48	08	21	43	15	87	09	44	90	09	79	09	
53	10	43	12	21	51	01	93	27	47	79	10	61	00	
2781	08	39	16	22	49	14	5296	50	44	84	13	57	07	
2997	07	27	22	25	43	37	5915	08	35	29	02	51	12	
3214	03	32	22	30	50	59	4838	04	39	30	02	66	11	
3430	13	33	32	24	46	70	22	01	60	1	06	04	07	
3647	29	19	30	32	47	51	4968	06	46	1	23	04	04	
3863	54	09	21	26	48	22	23	07	24	84	25	23	14	
4086	68	03	28	32	45	10	4604	02	22	85	28	26	14	
4303	60	10	19	17	48	07	43	33	09	06	22	45	15	
4512	28	25	06	21	59	10	4439	50	02	03	24	54	15	
4729	15	00	93	—	43	04	4660	01	54	83	23	02	11	
4945	13	45	25	26	76	14	50	02	64	85	12	06	08	
54	10	30	34	20	58	10	4138	02	16	79	19	36	38	
2990	51	32	30	22	59	17	68	58	34	84	21	40	18	
3205	28	43	19	16	77	03	3535	47	43	07	20	33	04	
3422	15	53	31	18	67	10	69	05	43	07	21	21	09	
4106	10	—	87	—	07	11	3778	03	49	04	18	32	01	
55	55	37	00	15	17	07	71	01	55	30	18	—	—	
2510	08	26	78	20	34	15	3911	56	50	35	34	26	13	
3292	03	03	76	30	58	13	4129	37	46	38	38	49	10	
3749	16	05	88	26	54	06	4805	04	46	37	22	34	10	
4556	35	05	79	32	55	06	72	56	05	27	15	06	56	
4774	51	05	74	26	62	02	3392	49	29	32	24	11	28	
4991	09	44	85	30	28	03	4064	07	45	24	12	09	06	
5207	20	42	79	22	29	11	4201	08	29	21	01	04	36	
73	40	05	73	24	56	16	73	20	45	81	24	27	64	
2725	64	07	66	25	57	10	4623	35	47	84	22	32	50	
2943	09	49	11	15	84	04	5724	04	07	84	26	44	05	
78	02	45	02	18	70	07	74	11	20	96	20	58	11	
2565	00	04	00	09	38	60	3702	22	32	1	13	57	05	
2787	00	09	00	01	33	36	4370	67	38	1	00	54	12	
83	60	38	28	30	13	30	4592	44	43	1	02	62	15	
2669	46	45	40	24	12	56	96	24	40	—	09	65	56	
2887	04	52	74	20	69	08	3051	14	33	—	03	59	77	
84	08	51	75	19	58	16	4201	61	50	21	23	48	37	
2384	65	19	35	20	58	03	97	05	53	05	33	34	08	
2603	59	01	39	30	56	01	2937	05	53	05	33	34	08	
85	29	52	75	23	89	06	4021	61	50	21	23	48	37	
3260	10	58	72	23	93	20	4239	60	52	10	22	48	62	
57	06	30	91	16	43	08	98	51	07	28	25	68	06	
3028	07	24	91	26	42	15	3911	27	01	28	02	59	08	
3253	03	10	97	18	38	10	6000	04	06	78	24	14	00	
2824	02	50	1	22	25	00	4036	08	00	86	31	19	04	
3042	08	53	1	15	30	01	02	07	18	—	20	26	02	
3260	65	46	74	09	71	01	05	37	56	06	12	07	06	
05	53	—	37	—	19	—	07	26	59	36	25	49	07	
2935	33	42	32	24	23	06	2910	32	51	34	23	50	07	
3153	12	46	68	24	43	08	09	46	09	58	81	24	58	44
06	09	56	65	25	46	07	4892	02	60	88	24	61	35	
2837	33	47	77	21	66	06	10	08	19	1	15	22	07	
3059	12	46	68	24	43	08	4726	19	12	1	15	20	03	
3277	09	56	65	25	46	07	12	41	8	1	18	30	09	
3277	03	10	97	18	38	10	4366	41	03	1	10	24	09	
07	08	53	1	15	30	01	13	57	54	—	23	38	08	
3003	65	46	74	09	71	01	3788	44	51	61	34	41	14	
09	30	49	68	06	63	05	5132	01	56	49	24	44	18	
2324	53	—	37	—	19	—	14	26	46	—	14	—	06	
2781	33	42	32	24	23	06	2864	65	55	—	14	20	07	
13	12	46	68	24	43	08	3605	03	47	—	11	25	15	
2589	09	56	65	25	46	07	3823	02	35	—	11	25	15	
14	33	47	77	21	66	06	4041	01	41	—	09	1	02	
2121	12	46	68	24	43	08	4266	01	24	—	13	26	07	
2340	09	56	65	25	46	07	4485	05	06	—	07	23	04	
15	33	47	77	21	66	06	4703	08	06	—	08	29	10	
2990	26	42	1	20	22	—	4921	27	01	—	17	23	03	
17	13	36	1	26	29	04	5143	51	13	—	11	27	03	
2529	19	35	—	22	39	04	5304	47	20	—	18	16	03	
2747	23	40	—	10	41	04	15	38	51	—	31	—	14	
19	23	40	—	10	41	04	—	—	—	—	—	—	—	
2482	24	45	1	26	13	16	—	—	—	—	—	—	—	
2701	50	38	1	21	13	04	—	—	—	—	—	—	—	
34	60	12	1	13	28	44	—	—	—	—	—	—	—	
2780	48	—	1	13	—	44	—	—	—	—	—	—	—	
2998	04	03	59	06	34	11	—	—	—	—	—	—	—	
39	02	27	65	13	25	01	—	—	—	—	—	—	—	
2529	21	43	36	26	60	09	—	—	—	—	—	—	—	
2747	43	43	50	29	44	11	—	—	—	—	—	—	—	
41	08	—	—	—	—	—	—	—	—	—	—	—	—	
2327	40	44	16	09	89	50	—	—	—	—	—	—	—	
2546	—	—	—	—	—	—	—	—	—	—	—	—	—	
58	—	—	—	—	—	—	—	—	—	—	—	—	—	
1859	—	—	—	—	—	—	—	—	—	—	—	—	—	
2077	—	—	—	—	—	—	—	—	—	—	—	—	—	
61	—	—	—	—	—	—	—	—	—	—	—	—	—	
2156	—	—	—	—	—	—	—	—	—	—	—	—	—	
5854	40	44	16	09	89	50	15	38	51	28	31	34	14	

J.D.— 2420000	AY Pup	$\gamma_{h,35m}^{4s}$ —25°21'9	WX Pup	$\gamma_{h,46m}^{4s}$ —20°59'1	WW Pup	C.P.D. —25°28'6	J.D.— 2420000	AY Pup	$\gamma_{h,35m}^{4s}$ —25°21'9	WX Pup	$\gamma_{h,46m}^{4s}$ —20°59'1	WW Pup	C.P.D. —25°28'6
6015'4582	m .40	m .60	m .22	m .29	m .38	m .12	6269'4862	m .05	m .41	m .93	m .17	m .07	m .50
28'3092	.16	.58	1'13	.22	.22	.69	5532	.01	.28	1'03	.23	.18	.31
3310	.35	.48	1'06	.34	.34	.52	5751	.09	.14	1'07	.34	.08	.10
29'3881	.06	.42	1'33	.00	.43	.11	70'5130	.02	.38	1'15	.26	.22	.03
4491	.02	.53	1'36	.10	.49	.71	5348	.19	.37	1'26	.13	.25	.03
30'3005	.09	.45	1'21	.12	.12	.17	73'5217	.03	.39	.10	.23	.90	.74
3223	.10	.54	1'23	.15	.19	.14	5435	.00	.34	.13	.26	.86	.38
36'2545	.07	.58	.87	.22	.83	.16	76'4583	.67	.23	.31	.24	.33	.06
2761	.16	.58	.86	.14	.90	.43	4805	.29	.30	.41	.30	.29	.01
38'3965	.18	.49	1'35	.21	.02	.17	77'4858	.06	.40	.74	.21	.56	.47
4183	.34	.47	1'39	.12	.12	.11	5074	.07	.29	.89	.18	.66	.71
39'2915	.01	.01	1'23	.19	.18	.09	94'4139	.01	.13	.13	.09	.78	.02
3133	.08	.20	1'13	.16	.22	.10	99'4145	.58	.46	.46	.34	.49	.01
40'4505	.04	.50	.38	.32	.54	.11	4363	.52	.46	.50	.27	.67	.01
4723	.07	.41	.43	.37	.63	.20	6303'4118	.52	.46	.39	.15	.20	.08
42'3860	.14	.45	.19	.15	.78	.13	4357	.21	.59	.45	.20	.01	.14
4079	.36	.48	.21	.03	.67	.07	5479	.03	.53	.56	.10	.04	.17
63'2829	.50	.33	.94	.41	.07	.09	5697	.05	.54	.50	.33	.04	.04
3047	.50	.17	.89	.37	.14	.01	05'5204	.61	.52	1'06	.30	.73	.61
64'3514	.04	.62	1'24	.26	.75	.36	5419	.35	.46	1'03	.22	.67	.46
3732	.02	.49	1'20	.20	.74	.15	06'3799	.08	.48	1'07	.23	.36	.02
65'3175	.04	.21	1'31	.17	.36	.07	4710	.51	.09	1'29	.28	.65	.05
67'3205	.31	.25	.35	.10	.48	.10	4945	.25	.01	1'25	.08	.71	.06
83'2432	.59	.51	1'37	.23	.19	.12	09'5083	.54	.53	.06	.14	.27	.69
84'2259	.05	.40	1'05	.17	.43	.01	5302	.34	.63	.10	.18	.20	.65
85'2141	.01	.49	.30	.27	.29	.08	10'3471	.10	.38	.03	.22	.69	.08
2359	.00	.61	.35	.26	.21	.08	4582	.51	.22	.22	.20	.56	.15
86'2133	.04	.20	.09	.24	.82	.07	4799	.23	.15	.25	.18	.62	.03
2355	.26	.34	.02	.34	.84	.04	23'3615	.44	.31	1'01	.11	.64	.03
87'2268	.46	.49	.36	.05	.39	.25	4973	.07	.53	1'05	.19	.64	.09
2486	.22	.47	.33	.05	.30	.06	5189	.01	.43	1'23	.32	.68	.19
89'2665	.14	.48	.67	.24	.39	.09	24'4548	.15	.49	1'19	.35	.18	.04
2887	.20	.55	.23	.23	.34	.03	4766	.23	.33	1'27	.09	.24	.03
91'2561	.12	.56	1'22	.26	.53	.05	25'4289	.47	.42	1'16	.11	.19	.04
2779	.09	.42	1'23	.30	.69	.06	4507	.48	.39	1'07	.03	.19	.14
92'2561	.01	.31	1'36	.22	.57	.11	33'3049	.06	.11	1'18	.26	.54	.07
2779	.07	.40	1'39	.23	.62	.25	5570	.06	.06	.06	.06	.06	.06
93'2609	.13	.52	1'04	.04	.00	.13	37'2858	.03	.10	.04	.27	.67	.23
2827	.32	.59	.92	.12	.10	.15	3997	.60	.22	.16	.27	.41	.03
94'2494	.50	.20	.31	.30	.23	.09	4216	.53	.45	.36	.31	.47	.00
2712	.46	.22	.28	.25	.27	.11	38'5041	.13	.41	.27	.24	.66	.05
97'2504	.17	.53	.27	.31	.89	.05	5230	.10	.46	.23	.25	.77	.03
2722	.37	.49	.20	.22	.82	.05	62'4149	.03	.53	.22	.28	.60	.04
99'2593	.03	.90	.22	.08	.06	.06	4377	.04	.47	.13	.30	.43	.01
6101'2786	.52	.44	1'26	.16	.66	.06	63'3976	.23	.15	.02	.03	.03	.04
02'2436	.44	.02	.91	.20	.32	.23	4198	.53	.14	.13	.09	.13	.01
2774	.21	.14	.79	.20	.57	.32	6476'2394	.48	.48	1'23	.29	.59	.01
15'1944	.02	.49	.20	.20	.05	.60	2610	.23	.53	1'30	.21	.81	.09
2162	.00	.54	.23	.25	.01	.42	7365'4834	.08	.05	.35	.09	.21	.03
17'1937	.26	.47	.28	.28	.57	.10	5053	.05	.20	.29	.20	.26	.09
2165	.49	.42	.92	.18	.42	.07	7717'5038	.12	.34	.73	.76	.76	.13
6241'5823	.07	.04	.73	.22	.29	.04	5252	.30	.55	.84	.12	.67	.04
6045	.01	.25	.77	.26	.33	.04	48'4740	.35	.24	.12	.18	.05	.07
48'5467	.47	.51	.28	.24	.26	.09	4955	.54	.34	.13	.26	.06	.05
5692	.35	.40	.39	.21	.13	.01	7802'4384	.63	.46	.07	.26	.74	.63
49'5461	.06	.04	.34	.06	.47	.33	4596	.50	.51	.03	.24	.68	.69
5679	.07	.32	.13	.58	.15	.15	03'3512	.43	.48	.30	.17	.15	.09
64'4881	.60	.41	.11	.15	.00	.02	3727	.61	.34	.37	.13	.16	.08
5099	.34	.44	.05	.27	.13	.07	07'3183	.23	.49	1'15	.06	1'00	.08
65'5277	.04	.39	.05	.15	.21	.42	3397	.44	.49	1'24	.06	.85	.09
5495	.02	.27	.11	.21	.43	.27	8219'3083	.33	.37	1'35	.20	.48	.10
66'5295	.09	.38	.32	.30	.54	.15	3298	.52	.32	1'30	.19	.56	.13
5514	.22	.45	.34	.41	.58	.11	8656'2190	.27	.20	1'13	.21	.06	.05
68'4629	.63	.43	.62	.08	.62	.09	2577	.03	.39	1'13	.25	.03	.04
4847	.55	.39	.73	.27	.69	.07	8660'2244	.12	.12	.12	.12	.12	.12
5543	.05	.42	.74	.14	.61	.11	8965'2903	.09	.36	.27	.27	.10	.06
5763	.02	.55	.78	.21	.58	.08	3124	.10	.44	.27	.12	.30	.06
69'4644	.13	.48	.87	.19	.33	.33	3574	.05	.40	.29	.26	.21	.16

J.D.— 2420000	AY Pup	$7^h35^m45^s$ — $25^{\circ}21'9$	WX Pup	$7^h46^m44^s$ — $20^{\circ}59'1$	WW Pup	C.P.D. — $25^{\circ}28'6$
8965'4236	<sup>m</sup> .31	<sup>m</sup> .42	<sup>m</sup> .31	<sup>m</sup> .09	<sup>m</sup> .34	<sup>m</sup> .00
85'2571	— .01	—	—	— .22	— .45	—
2785	— .02	—	—	— .15	— .44	—
3478	.20	—	—	.23	.58	—
3947	.47	—	—	.16	.63	—
9380'2091	.24	— .04	.88	—	.36	— .06
2271	.36	—	.92	— .16	.37	— .01
94'2557	.05	— .01	.02	.27	.67	.61
99'2040	.21	— .52	1'17	.23	.56	— .05
2282	.48	— .51	1'24	— .22	.59	— .11

## AY Pup.

Three comparison stars have been used, which are the same as used by HERTZSPRUNG in *B.A.N.* No. 340. The average magnitude differences between the comparison stars in provisional magnitudes from 362 plates were found to be:  $m'_b - m'_a = .91$  and  $m'_c - m'_a = .75$ .

The provisional magnitudes of the variable were reduced for each plate according to the formula  $m = .84 (m'_v - m'_a) / [\frac{1}{2}(m'_b + m'_c) - m'_a]$ , all plates thus being reduced to an "average" gradation.

 $7^h35^m45^s$ , —  $25^{\circ}21'9$ .

This variable is star *b* in *B.A.N.* No. 340. Only one comparison star was used, viz. the same as used by HERTZSPRUNG. In Table I the difference  $m'_v - m'_a$  is given for each plate,  $m'_v$  and  $m'_a$  being the provisional magnitudes of the variable and the comparison star respectively.

## WX Pup.

The images of this variable and the comparison stars are strongly overexposed on most of the plates. They had to be measured with a greater diaphragm than is customary in the old Schilt photometer. The same comparison stars have been used as in *B.A.N.* No. 340.

The average provisional magnitudes for the comparison stars from 349 plates, with *a* as zeropoint, are:  $m'_b = .37$  and  $m'_c = 1.27$ . From two plates taken with a grating in front of the objective the difference  $m_c - \frac{1}{2}(m_a + m_b)$  was found to be  $1^m.4$ .

The  $m_{pr}$  of the variable have been reduced for each plate according to the formula

$$m_v = 1.4 (2 m'_v - m'_a - m'_b) / (2 m'_c - m'_a - m'_b)$$

 $7^h46^m44^s$ , —  $20^{\circ}59'1$ .

This is variable *g* in *B.A.N.* No. 340. Four com-

J.D.— 2420000	AY Pup	$7^h35^m45^s$ — $25^{\circ}21'9$	WX Pup	$7^h46^m44^s$ — $20^{\circ}59'1$	WW Pup	C.P.D. — $25^{\circ}28'6$
9399'2483	<sup>m</sup> .57	<sup>m</sup> .53	<sup>m</sup> 1'07	<sup>m</sup> .12	<sup>m</sup> .58	<sup>m</sup> .03
2642	.51	— .44	1'00	— .26	.57	.01
9400'1981	.54	—	1'00	— .30	.62	.01
2198	.29	— .08	.97	— .26	.65	.14
02'2077	— .05	— .15	— .14	— .02	— .48	.13
2302	.09	— .12	— .23	— .17	— .53	.37
2531	.31	— .01	— .25	— .22	— .39	.49
07'2034	.55	— .46	1'02	— .24	— .69	.02
2228	.64	— .35	1'02	— .23	— .62	.02
2422	.43	— .39	1'05	— .26	— .77	.01

parison stars have been used, the coordinates of which relative to the variable are: *a* +  $16^s.7$ , —  $0'.5$ ; *b* —  $3^s.3$ , +  $3'.8$ ; *c* —  $7^s.6$ , +  $3'.3$  while *d* is the same as used by HERTZSPRUNG. The average  $m_{pr}$  of the comparison stars from 342 plates was found to be, with *a* as zeropoint,  $m'_b = .38$ ,  $m'_c = .63$  and  $m'_d = .45$ . The difference between the  $m_{pr}$  of the variable and the mean of the  $m_{pr}$  of the four comparison stars was formed without regard to the differences in gradation between the different plates.

## WW Pup.

Three comparison stars have been used, viz. *a* = C.P.D. —  $20^{\circ}28'33$ , *b* = C.P.D. —  $20^{\circ}28'26$  and *c* at  $7^h36^m15^s$ , —  $20^{\circ}47'6$  (1875).

The average  $m_{pr}$  of the comparison stars from 357 plates was, with *a* as zeropoint,  $m'_b = 1.11$ ,  $m'_c = 1.92$ .

From two plates taken with a grating in front of the objective the difference in magnitude between the comparison stars *a* and *c* was found to be  $2^m.37$ . The  $m_{pr}$  of the variable were reduced for each plate according to the formula

$$m_v = 2.37 (m'_v - m'_b) / (m'_c - m'_a)$$

C.P.D. —  $25^{\circ}28'6$ .

Three comparison stars have been used, viz. *a* = C.P.D. —  $25^{\circ}28'68$ , *b* = C.P.D. —  $25^{\circ}28'73$  and *c* at  $7^h43^m4^s$ , —  $25^{\circ}47'5$  (1875).

The average  $m_{pr}$  of the comparison stars from 351 plates was, with *a* as zeropoint,  $m'_b = .42$ ,  $m'_c = 1.28$ .

From one plate taken with a grating in front of the objective the differences between the comparison stars were found to be  $m_b - m_a = 1^m.40$  and  $m_c - m_a = 1^m.73$ .

The  $m_{pr}$  of the variable have been reduced according to the formula

$$m_v = 1.3 [m'_v - \frac{1}{2}(m'_a + m'_b)] / [m'_c - \frac{1}{2}(m'_a + m'_b)]$$