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COMMUNICATIONS FROM THE OBSERVATORY AT LEIDEN

Photographic observations of RS Bootis, an RR Lyrae-type variable with long secondary period, by *P. Th. Oosterhoff*¹⁾.

During the years 1938–1944 2418 photographic observations have been obtained with the 33 cm Leiden refractor. The plates were measured in a Schilt microphotometer. The internal mean error of a magnitude determination is ± 0.036 , but there is a strong indication of the existence of systematic plate errors with a mean dispersion of at least ± 0.032 . The individual magnitudes are given in Table 9. Epochs, 33 in number, have been derived by least squares for a point on the rising branch of brightness $\Delta m = 0.00$. They clearly show that RS Bootis has a secondary period during which the form of the light-curve changes considerably. The most probable elements for these epochs are:

$$\text{Epoch} = 2428972^{\text{d}}.6633 \pm 7 \pm 18 + \frac{\text{d}.37733657}{18} t - \frac{\text{d}.0038}{4} \sin 2\pi\psi + \frac{\text{d}.0086}{4} \cos 2\pi\psi \quad \text{m.e.}$$

where ψ is the phase of the secondary period. This period is very long, namely (1424 ± 10) P or 537 days. For five other stars of similar character the secondary period varies between 64 P and 160 P.

Mean light-curves for different values of the phase ψ are shown in the Figures 4a and 4b. When the rising branch begins early, its slope is small and the range of the light-variation is a minimum. After half the secondary period the rising branch is steep, but comes 27 minutes later and the range is a maximum. The extreme values of minimum and maximum brightness are about $11^{\text{m}}.02 - 11^{\text{m}}.22$ and $9^{\text{m}}.86 - 9^{\text{m}}.71$ respectively. Figure 5 represents the variation in brightness for a point of given phase during a secondary period. Sufficient material is only available for the part of the light-curve from minimum to maximum. The older observations are too few in number to permit the determination of improved periods from the combined material, but they indicate that the ordinary period increases in a secular or long period manner.

This variable was put on the program of the 33 cm Leiden refractor for the following reasons. According to *Geschichte und Literatur des Lichtwechsels der Veränderlichen Sterne* by R. PRAGER the light-curve of this star is subject to considerable variations, especially near maximum brightness, which may be an indication that its light-variation is of a complicated character similar to that of RR Lyrae. It seems probable that accurate observations will reveal this two-period-type of light-variation for many more cluster type variables and a detailed study of this phenomenon is much to be desired. An important step in this direction has already been made by JULIA BALÁZS and L. DETRE, who have published extensive series of observations for RW Draconis²⁾, AR Herculis³⁾ and RR Lyrae⁴⁾. As the position and brightness of RS Bootis are quite favourable for the photographic refractor of the Leiden Observatory observations have been started in 1938.

The plates used are mainly Eastman 40, although in 1939 a number of observations were made on plates of the brand Guilleminot La Superguil. The exposure time, which usually was 90 seconds, varies from thirty seconds to two and a half minutes. As a rule about 44 exposures were made on a single plate. They

were taken one millimetre inside the best focus. The total number of plates and exposures is 75 and 2418 respectively.

Some data about the comparison stars have been collected in Table 1. The last three stars play only a secondary role in the reduction. It is seen from the fourth and fifth column that the position of the com-

TABLE 1

star	B.D.	m_{pg}	$\Delta\alpha \cos \delta$	$\Delta\delta$	r
var.	+ 32° 2489	—	0'0	0'0	15'9
1	+ 32 2485	9'76 ^m	— 15'3	— 7'2	1'8
2	—	10'60	— 15'6	— 7'3	2'0
3	+ 32 2487	11'10	— 13'9	— 1'8	3'7
4	+ 31 2627	9'79	— 22'6	— 26'5	22'4
5	+ 32 2481	10'15	— 53'0	+ 7'7	40'3
6	+ 32 2484	11'08	— 23'4	— 15'9	13'4

parison stars relative to the variable is not very satisfactory, as they are all situated on its preceding side. Their distance in minutes of arc from the mean position of the first three comparison stars is given in the last column. These figures will be used later. The photographic magnitudes in the third column have

¹⁾ Received in July 1944.

²⁾ *Mitteilungen der Sternwarte Budapest-Svábhegy*, Nr 5, 1938.

³⁾ *Mitteilungen der Sternwarte Budapest-Svábhegy*, Nr 8, 1939.

⁴⁾ *Mitteilungen der Sternwarte Budapest-Svábhegy*, Nr 17, 1943.

TABLE 2

plate	n	relative grada- tion	star 1	star 2	star 3	star 4	star 5	star 6	plate	n	relative grada- tion	star 1	star 2	star 3	star 4	star 5	star 6
4348	10	1'11	m 9'76	m 10'59	m 11'10	m 9'77	m 10'00	m 11'08	5669	47	1'33	m 9'77	m 10'58	m 11'11	m 9'76	m 9'98	m 11'09
4349	10	1'13	'76	'59	'10	'71	9'91	'01	5677	45	1'31	'76	'59	'10	'84	10'24	'08
4350	10	1'24	'76	'59	'10	'87	10'07	'08	5714	11	1'00	'76	'59	'11	'73	'11	'07
4362	17	1'18	'76	'59	'11	'80	'24	'05	5726	34	1'22	'76	'59	'10	'80	'09	'07
4363	17	1'16	'77	'59	'11	'78	'16	'08	5945	44	1'05	'77	'59	'11	'74	'20	'05
4364	17	1'21	'76	'59	'10	'89	'26	'11	5946	25	1'11	'77	'58	'11	'76	'19	'06
4764	32	1'06	'76	'60	'10	'84	'11	'05	5947	42	1'15	'77	'59	'11	'70	'20	'04
4765	32	1'07	'76	'60	'10	'83	'08	'06	5948	44	1'17	'76	'60	'10	'79	'13	'07
4766	11	1'26	'76	'59	'11	'85	'09	'01	5949	44	1'16	'76	'59	'10	'86	'20	'08
4825	32	1'26	'75	'62	'09	'83	'11	'10	5980	44	1'20	'76	'59	'10	'75	'23	'08
4826	31	1'34	'76	'60	'10	'74	'06	'07	5981	43	1'29	'77	'59	'11	'78	'16	'09
4827	30	1'27	'75	'62	'09	'72	'12	'09	5982	44	1'32	'76	'59	'11	'77	'19	'07
4837	3	1'35	'77	'56	'12	'77	'16	'07	5983	44	1'28	'77	'59	'11	'80	'19	'07
4838	32	1'28	'77	'58	'11	'80	'18	'03	5984	18	1'22	'76	'59	'11	'78	'16	'10
4839	20	1'29	'76	'59	'10	'87	'11	'10	5988	44	1'15	'77	'58	'11	'85	'16	'09
5297	44	1'21	'77	'58	'11	'74	'13	'09	5989	22	1'17	'76	'59	'10	'79	'19	'09
5320	18	1'26	'77	'58	'11	'81	'29	'08	6006	44	1'30	'77	'58	'11	'80	'22	'08
5330	50	1'27	'76	'59	'11	'78	'22	'10	6015	42	1'20	'76	'59	'11	'81	'21	'08
5331	44	1'13	'76	'60	'10	'73	'14	'06	6045	36	1'40	'76	'59	'11	'79	'14	'07
5349	48	1'25	'77	'58	'11	'83	'21	'11	6047	43	1'26	'77	'58	'11	'74	'21	'07
5354	32	1'23	'76	'59	'11	'81	'03	'10	6067	39	1'31	'76	'60	'10	'81	'33	'05
5359	44	1'20	'76	'59	'11	'82	'10	'09	6097	44	1'29	'76	'59	'11	'83	'15	'08
5360	45	1'33	'77	'58	'11	'81	'14	'11	6121	22	1'20	'76	'59	'11	'80	'24	'08
5361	45	1'37	'77	'58	'11	'82	'10	'09	6294	39	1'24	'76	'60	'10	'76	'10	'12
5362	34	1'25	'76	'58	'11	'76	'07	'07	6296	13	1'36	'76	'59	'11	'81	'08	'09
5363	19	1'36	'76	'59	'11	'81	'08	'10	6297	44	1'34	'77	'58	'11	'82	'07	'12
5553	11	1'15	'77	'58	'11	'80	'21	'08	6304	44	1'23	'77	'59	'11	'81	'12	'11
5554	11	1'14	'76	'59	'11	'75	'22	'01	6305	44	1'20	'77	'58	'11	'79	'22	'08
5555	11	1'15	'77	'59	'11	'83	'15	'12	6319	7	1'22	'77	'59	'11	'84	'32	'11
5556	11	1'09	'76	'60	'10	'83	'09	'08	6354	44	1'25	'76	'59	'10	'85	'22	'08
5580	45	1'27	'76	'59	'11	'77	'17	'10	6393	43	1'26	'77	'59	'11	'73	'22	'05
5581	45	1'22	'76	'61	'10	'77	'13	'09	6394	41	1'31	'76	'60	'10	'89	'16	'13
5582	45	1'22	'76	'60	'10	'82	'17	'11	6562	44	1'16	'77	'58	'11	'75	'15	'03
5583	27	1'17	'76	'60	'10	'77	'10	'06	6565	43	1'11	'76	'59	'10	'75	'14	'11
5590	45	1'24	'76	'59	'11	'75	'19	'09	6583	44	1'08	'76	'59	'11	'78	'24	'07
5620	11	1'21	'77	'59	'11	'76	'24	'06	6587	35	1'02	'76	'59	'11	'69	9'99	'02
5621	34	1'19	'77	'58	'11	'71	'14	'05	6593	22	1'17	'76	'59	'11	'80	10'22	'05
5622	23	1'20	'76	'59	'11	'77	'17	'09									

been taken from SEARES and SHAPLEY¹⁾ for the first three stars. Their colour-index is according to the same authors $+^m.5$, which value does not differ much from that of the variable, which according to SEARES and SHAPLEY varies between $-^m.1$ and $+^m.5$. The remaining magnitudes of Table 1 are derived below. In order to test the scale of these magnitudes a plate has been taken with three exposures with a coarse grating in front of the objective. The resulting magnitudes differ by 2.5 per cent from the scale of SEARES and SHAPLEY in such a manner that the range of the variable would be increased if these magnitudes were adopted. This difference of a few per cent is however too small to be considered as ascertained and the magnitudes of the table have been used.

The plates have been measured in the Schilt micro-photometer partly by Mr C. J. KOOREMAN but mainly by the writer. As some of the stars are several centimetres apart on the plates, much care has been taken to perform the measurement of the different stars on the same plate at the same focus of the photometer.

¹⁾ *Ap. J.* 48, 229, Table VII, 1918; *Mt Wilson Contr.* No. 159.

This is important as a slight change in this focus may cause a considerable difference in the resulting measure. It forms the main reason why the photometric results obtained with such a photometer usually decrease in accuracy with increasing distance between the stars. The galvanometer readings have been reduced to magnitudes by means of the following reduction method. The readings were first turned into provisional magnitudes by means of WESSELINK's table¹⁾. Then for each exposure differences were computed from the mean provisional magnitude of the six comparison stars and the mean values of these differences for all exposures of each plate were formed. These mean differences were finally reduced with least squares to the scale and zeropoint of SEARES and SHAPLEY by means of the first three comparison stars. The resulting mean magnitudes are given for each plate in Table 2. In the third column the mean relative gradations are given. These are the figures by which the mean provisional magnitudes must be divided in order to reduce them to the correct photo-

¹⁾ *B.A.N.* No. 318, 333, 1939.

metric scale. The mean magnitudes of the first three comparison stars necessarily agree closely with the values from Table 1. The magnitudes of the remaining stars have been derived from Table 2. The mean magnitude and its dispersion for each comparison star as derived from Table 2 is found to be:

star	mean magnitude	mean dispersion	r
1	9.763	$\pm .0053$	1.8
2	10.590	$\pm .0089$	2.0
3	11.106	$\pm .0056$	3.7
4	9.790	$\pm .044$	22.4
5	10.154	$\pm .076$	40.3
6	11.078	$\pm .026$	13.4

In this computation equal weight has been given to all plates. From these figures it is clear that systematic plate errors occur. They are probably caused by systematic variations in the thickness of the photographic emulsion over the plate, whereas the above mentioned effect of changes in the photometer focus may also be partly responsible. It is interesting to notice that the dispersions are practically proportional to the distance r of the stars from the mean position of the first three comparison stars, the magnitudes of which were adjusted by means of least squares. As for RS Bootis this distance is 15''.9 one should expect a mean systematic plate error for the variable of $\pm .032$. Later we shall compare this value with another derived from the light-curve.

For some plates the gradation is evidently not the same for all exposures, which fact probably is due to variations in the seeing conditions and to guiding errors. I therefore decided that the relative gradation of each individual exposure should be taken into account in the determination of the magnitude of the variable. The gradation has been determined by means of the six comparison stars and for each plate the magnitudes which are given in Table 2 have been used. In this manner the systematic plate errors do not enter the determination of the gradation. The gradation-factor having been applied, which reduces the photometric scale to that of SEARES and SHAPLEY, the zeropoint was chosen in such a way that for each exposure it is given by the mean magnitude of the first three comparison stars.

The reduction which has just been described can be summarized as follows. For each exposure the magnitude of RS Bootis has been derived with the aid of the first three comparison stars. The photometric scale is that of SEARES and SHAPLEY; the zeropoint coincides with the mean magnitude of these three comparison stars. The remaining comparison stars have only been used in order to obtain a more accurate determination of the relative gradation for each exposure.

The magnitudes Δm have been listed in Table 9 at the end of this article. They are transformed into apparent magnitudes by addition of 10.49. In the first column of this table the heliocentric Julian Day is given. The reduction to the sun has been made by the formula:

$$\text{Reduction} = + .00387 X + .00167 Y$$

where X and Y are rectangular equatorial coordinates of the sun. The last column of Table 9 will be explained below.

From a preliminary discussion of the present observations it became soon clear that the variable shows the characteristic features of the complicated light-variation of the type of RR Lyrae itself. Therefore two periods must be determined, namely in the first place the ordinary period P of about $d.37$ and in addition the secondary period P' . The best method to determine these periods seems to be with the aid of epochs for points on the steep ascending branch, which can be derived with a greater accuracy than for any other point of the light-curve. This method has however a drawback, namely the fact that in this case a certain amount of interlocking exists between the two periods. On the other hand one could derive a value for the secondary period quite independent from the ordinary period by using for example the steepness of the rising branches, but this would mean a considerable loss in accuracy. A third possibility is offered by the existence of several old series of observations, which in combination with the present material would probably yield a value of the ordinary period, which on account of the long time interval covered by them would be accurate enough for the short series presented here. But in this case a secular or long period change of the period, as has been found to exist in the case of RR Lyrae, RW Draconis and AR Herculis, would make the result too uncertain. In the following discussion we shall therefore make use of our own observations only, which form a homogeneous material and which cover a sufficiently long time interval for a satisfactory determination of both periods. The first method of epochs for a point on the steep rising branch will be applied.

The epoch for a point on the ascending branch of brightness $\Delta m = .00$ has been derived with the assumption that for a small part of this branch near the point in question the magnitude is a linear function of the time and accordingly an equation of the type: $\Delta m = a + b t$ has been solved by least squares for all observed rising branches. The correct way to do this would be to include only those observations which fall within a certain interval of phase. In the present case this cannot be done as the two periods and consequently also the phase have not yet been determin-

ed. Therefore those observations have been used which fall within an interval of ± 0.140 around a provisional epoch, which had been derived when only a preliminary reduction of the observations had been carried out. For the derivation of this first epoch the observations were selected between certain limits of brightness.

The relations computed by least squares have been tabulated in Table 3. The unit of t is $d.0001$ and its zeropoint is given by the Julian Day in the first column. The mean error of one observation as derived from the residuals of these formulae is given in the

third column, whereas the computed time at which Δm equals zero is tabulated in the last. The observations which were used in the computation and their residuals ($O-C$) have been listed in Table 4.

The two periods P and P' have then been derived in the following manner. I have assumed that the epochs for a point on the rising branch can be represented by the equation:

$$\text{Epoch} = A + Bt + C \sin 2\pi\psi + D \cos 2\pi\psi.$$

Here B is identical with the period P , t is the number of periods elapsed and it has therefore a meaning

TABLE 3

J. D.	relation between Δm and t	m.e. of one observation	t_0	J. D.	relation between Δm and t	m.e. of one observation	t_0
2428972.6600	$\Delta m = +.562 - .00461 t$ $\pm .30$	$\pm .027$	122	2430462.3800	$\Delta m = +.684 - .00500 t$ $\pm .16$	$\pm .020$	137
2428977.5700	$\Delta m = +.336 - .00373 t$ $\pm .16$	$\pm .028$	90	2430465.4000	$\Delta m = +.652 - .00558 t$ $\pm .23$	$\pm .029$	117
2429326.5900	$\Delta m = +.581 - .00450 t$ $\pm .33$	$\pm .057$	129	2430466.5300	$\Delta m = +.625 - .00470 t$ $\pm .29$	$\pm .036$	133
2429373.3900	$\Delta m = +.280 - .00441 t$ $\pm .17$	$\pm .033$	63	2430486.5300	$\Delta m = +.625 - .00499 t$ $\pm .35$	$\pm .039$	125
2429694.4900	$\Delta m = +.331 - .00333 t$ $\pm .22$	$\pm .028$	99	2430488.4200	$\Delta m = +.554 - .00461 t$ $\pm .17$	$\pm .019$	120
2429726.5600	$\Delta m = +.423 - .00319 t$ $\pm .29$	$\pm .037$	133	2430514.4600	$\Delta m = +.426 - .00511 t$ $\pm .20$	$\pm .027$	83
2429730.3400	$\Delta m = +.178 - .00309 t$ $\pm .27$	$\pm .034$	58	2430517.4800	$\Delta m = +.333 - .00498 t$ $\pm .18$	$\pm .020$	67
2429751.4700	$\Delta m = +.353 - .00358 t$ $\pm .35$	$\pm .044$	99	2430531.4400	$\Delta m = +.622 - .00524 t$ $\pm .21$	$\pm .024$	119
2429752.6000	$\Delta m = +.281 - .00347 t$ $\pm .50$	$\pm .054$	81	2430790.6500	$\Delta m = +.248 - .00337 t$ $\pm .51$	$\pm .064$	74
2430066.5600	$\Delta m = +.482 - .00515 t$ $\pm .34$	$\pm .045$	94	2430812.5400	$\Delta m = +.344 - .00369 t$ $\pm .28$	$\pm .031$	93
2430071.4600	$\Delta m = +.805 - .00525 t$ $\pm .19$	$\pm .028$	153	2430849.5200	$\Delta m = +.213 - .00347 t$ $\pm .20$	$\pm .022$	61
2430092.5900	$\Delta m = +.464 - .00367 t$ $\pm .22$	$\pm .028$	126	2431144.6100	$\Delta m = +.428 - .00399 t$ $\pm .34$	$\pm .043$	107
2430114.4800	$\Delta m = +.271 - .00530 t$ $\pm .21$	$\pm .027$	51	2431172.5300	$\Delta m = +.517 - .00487 t$ $\pm .20$	$\pm .024$	106
2430117.5000	$\Delta m = +.239 - .00431 t$ $\pm .24$	$\pm .030$	55	2431200.4500	$\Delta m = +.425 - .00381 t$ $\pm .35$	$\pm .039$	112
2430162.4000	$\Delta m = +.158 - .00411 t$ $\pm .63$	$\pm .055$	38	2431223.4700	$\Delta m = +.246 - .00373 t$ $\pm .25$	$\pm .028$	66
2430168.4300	$\Delta m = +.309 - .00328 t$ $\pm .29$	$\pm .033$	94	2431240.4500	$\Delta m = +.180 - .00337 t$ $\pm .40$	$\pm .044$	53
2430443.5200	$\Delta m = +.255 - .00400 t$ $\pm .21$	$\pm .027$	64				

TABLE 4

[illegible]

different from the discussion given above, and ψ is the phase computed with the secondary period P' . A preliminary investigation had already proved that the secondary period is very long, namely about 1400 times the ordinary period. The four constants of the

equation have therefore been determined by the method of least squares for three different sets of ψ , which correspond with values of the secondary period of 1390, 1430 and 1470 P. The results obtained are:

$$\begin{aligned}
 P' = 1390 \text{ P: Epoch} &= 2428972^{\text{d}}.6626 + .37733683 t - .0001 \sin 2\pi\psi_1 + .0091 \cos 2\pi\psi_1 \\
 &\quad \pm 8 \pm .21 \pm 5 \pm 5 \text{ m.e.} \\
 P' = 1430 \text{ P: Epoch} &= 2428972^{\text{d}}.6634 + .37733652 t - .0043 \sin 2\pi\psi_2 + .0084 \cos 2\pi\psi_2 \\
 &\quad \pm 7 \pm .18 \pm 4 \pm 4 \text{ m.e.} \\
 P' = 1470 \text{ P: Epoch} &= 2428972^{\text{d}}.6646 + .37733613 t - .0073 \sin 2\pi\psi_3 + .0061 \cos 2\pi\psi_3 \\
 &\quad \pm 9 \pm .24 \pm 5 \pm 6 \text{ m.e.}
 \end{aligned}$$

TABLE 5

Epoch on rising branch $\Delta m = .00$	t	ψ_1	$O-C_1$	Epoch - ($A_1 + B_1 t$)	ψ_2	$O-C_2$	Epoch - ($A_2 + B_2 t$)	ψ_3	$O-C_3$	Epoch - ($A_3 + B_3 t$)
$2428972^{\text{d}}.6722$	0	.000	+ .0005	+ .0096	.000	+ .0004	+ .0088	.000	+ .0015	+ .0076
77'5790	13	.009	+ 19	+ 110	.009	+ 20	+ 102	.009	+ 34	+ 90
9326'6029	938	.675	+ 23	- 16	.656	- 10	- 22	.638	- 46	- 30
73'3963	1062	.764	+ 10	- 20	.743	- 24	+ 15	.722	- 53	+ 7
9694'4999	1913	1'376	- 15	- 81	1'338	- 3	- 83	1'301	+ 2	- 87
9726'5733	1998	1'437	+ 2	- 83	1'397	+ 8	- 85	1'359	+ 5	- 89
30'3458	2008	1'445	- 5	- 92	1'404	- 2	- 94	1'366	- 2	- 98
51'4799	2064	1'485	+ 32	- 59	1'443	+ 33	- 61	1'404	+ 27	- 65
52'6081	2067	1'487	- 6	- 97	1'445	- 5	- 99	1'406	- 12	- 103
2430066'5694	2899	2'086	- 5	+ 73	2'027	- 2	+ 74	1'972	+ 1	+ 73
71'4753	2912	2'095	+ 3	+ 79	2'036	+ 7	+ 79	1'981	+ 10	+ 79
92'6026	2968	2'135	- 16	+ 43	2'076	- 12	+ 44	2'019	- 8	+ 44
0114'4851	3026	2'177	- 26	+ 13	2'116	- 21	+ 14	2'059	- 16	+ 14
17'5055	3034	2'183	- 7	+ 29	2'122	- 1	+ 31	2'064	+ 3	+ 31
0162'4038	3153	2'268	- 7	- 18	2'205	+ 1	- 17	2'145	+ 5	- 16
68'4394	3169	2'280	- 17	- 36	2'216	- 11	- 35	2'156	- 7	- 34
0443'5264	3898	2'804	+ 17	+ 48	2'726	+ 23	+ 52	2'652	+ 31	+ 56
62'3937	3948	2'840	+ 2	+ 53	2'761	+ 9	+ 57	2'686	+ 17	+ 61
65'4117	3956	2'846	- 7	+ 46	2'766	- 1	+ 50	2'691	+ 7	+ 54
66'5433	3959	2'848	- 12	+ 42	2'769	- 6	+ 46	2'693	+ 2	+ 50
86'5425	4012	2'886	- 24	+ 45	2'806	- 19	+ 50	2'729	- 11	+ 53
88'4320	4017	2'890	+ 2	+ 73	2'809	+ 8	+ 78	2'733	+ 16	+ 82
0514'4683	4086	2'940	- 11	+ 74	2'857	- 7	+ 79	2'780	- 0	+ 83
17'4867	4094	2'945	- 15	+ 71	2'863	- 11	+ 76	2'785	- 5	+ 80
31'4519	4131	2'972	+ 19	+ 108	2'889	+ 21	+ 113	2'810	+ 27	+ 117
0790'6574	4818	3'466	- 51	- 141	3'369	- 45	- 134	3'278	- 44	- 127
0812'5493	4876	3'508	+ 14	- 77	3'410	+ 24	- 70	3'317	+ 29	- 63
49'5261	4974	3'578	- 19	- 99	3'478	- 2	- 92	3'384	+ 10	- 84
1144'6207	5756	4'141	+ 17	+ 73	4'025	+ 6	+ 83	3'916	+ 5	+ 93
72'5406	5830	4'194	+ 13	+ 43	4'077	- 3	+ 53	3'966	- 11	+ 64
1200'4612	5904	4'247	+ 19	+ 19	4'129	+ 2	+ 30	4'016	- 12	+ 41
23'4766	5965	4'291	+ 23	- 2	4'171	+ 5	+ 9	4'058	- 10	+ 20
40'4553	6010	4'324	+ 26	- 17	4'203	+ 11	- 6	4'088	- 8	+ 5

The epochs and their residuals from these three solutions are given in Table 5. They are graphically shown in Figure 1.

The figure clearly shows that the assumption of a sine-curve is fully justified. The second solution seems to give the best representation of the observations. The sum of the squares of the residuals for the three solutions is:

$$\begin{aligned}
 &\Sigma (O-C)^2 \\
 P' = 1390 \text{ P} &\quad 00010637 \\
 P' = 1430 \text{ P} &\quad 00007527 \\
 P' = 1470 \text{ P} &\quad 00013481
 \end{aligned}$$

These three values can be represented by a parabola and the most probable value of P' must cor-

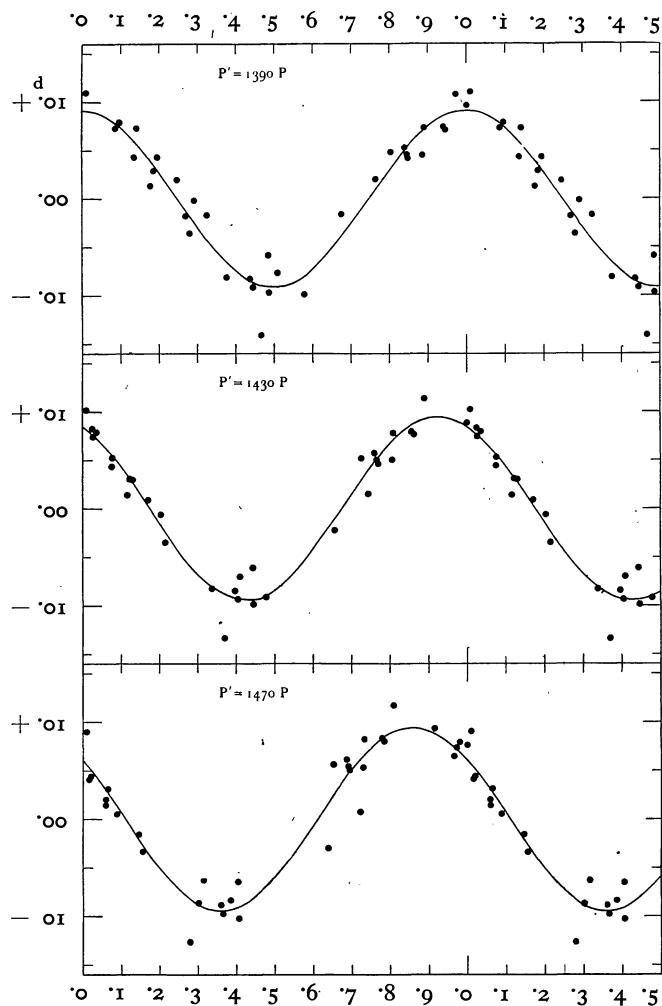
respond with its top. In this way we find the following value with its mean error computed according to the formula derived by PANNEKOEK and ELSA VAN DIEN¹⁾:

$$\begin{aligned}
 P' &= 1424 \text{ P} \\
 &\pm 10 \text{ m.e.}
 \end{aligned}$$

I am convinced that a much shorter period is out of the question. This is well illustrated by Figure 2, where the residuals computed from the first two terms of the second solution have been plotted not against ψ_2 as in Figure 1, but against the number of periods elapsed since the first epoch. During the third,

¹⁾ B.A.N. No. 297, 142, 1937.

FIGURE 1



fourth, fifth and last opposition in which the variable has been observed too many observations have been obtained at intervals varying from a few days to some months to leave a short period undetected.

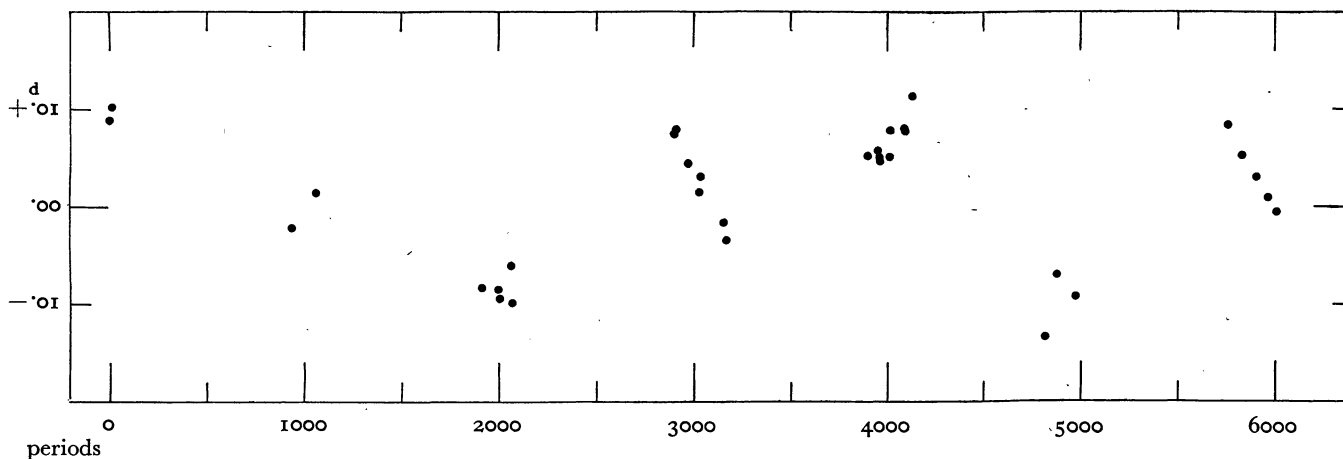
It may be interesting to compare the ratio between secondary and ordinary period as found here for RS Bootis with the same ratio for other variables of the RR Lyrae type. As far as I know the following data have been published:

variable	P	P'	P'/P
	^d	^d	
RS Bootis	377	537	1424
RW Draconis	443	41.6	94
AR Herculis	470	31.5	67
XZ Draconis	476	76	160 ¹⁾
Y Leonis Minoris	522	33.4	64 ²⁾
RR Lyrae	567	41.0	72

For RR Lyrae the figures given by BALÁZS and DETRE have been quoted here, although A. DE SITTER derived a somewhat different value for the secondary period³⁾. The value of P'/P for RS Bootis is very different from that of the other four variables, but as we will see below the characteristic features of the secondary light-variation are of exactly the same type. From the point of view of the observer this large value is rather unpleasant, as it will take many years to collect observations which cover more or less all values of the phase ψ of the secondary period.

The most probable value of the ordinary period P, which corresponds with $P' = 1424 P$, is: $d.37733657 \pm d.00000018$ m.e. for the mean epoch J.D. 2430168.4405. The phases in the third column

FIGURE 2



of Table 9 have therefore been computed by means of the formula:

$$\text{Phase} = 2^{d-1} \cdot 650154 \text{ (J.D. - 2400000)}$$

The phase ψ of the secondary period, which has been given in italics for each plate in Table 9 on the

same line as the plate number, was computed by the formula:

$$\psi = d^{-1} \cdot 001861 \text{ (J.D. - 2400000)}$$

¹⁾ A.N., 271, 231, 1940.

²⁾ Harvard Reprint No. 231, 32, 1941.

³⁾ B.A.N. No. 234, 1932.

TABLE 6

inclination ris. br.	<i>t</i>	phase ψ	<i>O</i> - <i>C</i>	inclination ris. br.	<i>t</i>	phase ψ	<i>O</i> - <i>C</i>	inclination ris. br.	<i>t</i>	phase ψ	<i>O</i> - <i>C</i>
460	0	·000	- 16	367	2968	·084	- 73	511	4086	·869	+ 14
373	13	·009	- 100	530	3026	·125	+ 111	498	4094	·875	0
450	938	·659	+ 20	431	3034	·131	+ 15	524	4131	·901	+ 27
441	1062	·746	- 29	411	3153	·214	+ 36	337	4818	·383	+ 3
333	1913	·343	- 3	328	3169	·225	- 43	369	4876	·424	+ 33
319	1998	·403	- 15	400	3898	·737	- 66	347	4974	·493	- 6
309	2008	·410	- 26	500	3948	·772	+ 21	399	5756	·042	- 61
358	2064	·449	+ 18	558	3956	·778	+ 77	487	5830	·094	+ 52
347	2067	·452	+ 5	470	3959	·780	- 12	381	5904	·146	- 28
515	2899	·036	+ 53	499	4012	·817	+ 8	373	5965	·189	- 14
525	2912	·045	+ 67	461	4017	·821	- 31	337	6010	·221	- 35

where $(d^{-1} \cdot 001861)^{-1} = 1424 \times d \cdot 37733657 = 537^d \cdot 3$.

Some remarks should still be made regarding the second solution of Table 5. This solution, which was carried out with the adopted value $P' = 1430$ P, is practically identical with the best possible solution with $P' = 1424$ P, as we are near the top of the parabola. The mean error for a single epoch is found to be $\pm d \cdot 0016$. On the ascending branch an increase of $d \cdot 0001$ in time corresponds on the average with an increase of $m \cdot 0042$ in brightness, as is seen from Table 3. The uncertainty of an epoch therefore corresponds with a mean error of $\pm m \cdot 067$, which is considerably larger than should be expected, as about 10 observations were used on each rising branch¹⁾. In order to see how this discrepancy can be explained it is necessary to form an idea about the accuracy of the observations.

The accidental errors are easily determined. With the aid of the figures in the third column of Table 3 the mean accidental error is found to be $\pm m \cdot 036$, a value which has been derived from the residuals of the least squares solutions of the observations on the steep rising branch. This value has been confirmed in the following manner from a much larger material. The differences in magnitude were formed between consecutive observations for each plate and the mean accidental error has then been derived from the relation: $(m.e.)^2 = \frac{\Sigma \Delta^2}{2n}$. This has been carried out separately for the observations between the phases ·10 and ·95 and for the remaining observations, with the following result:

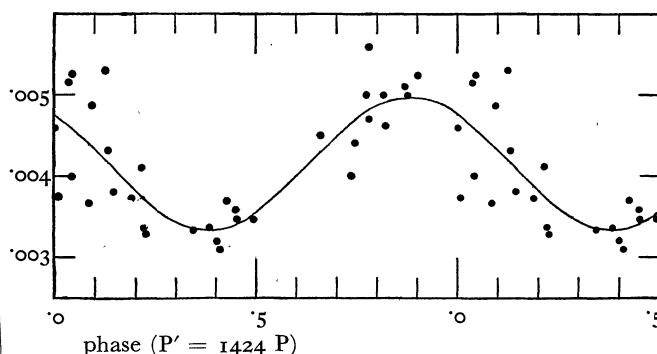
phase	<i>n</i>	m.e.
·10 - ·95	1144	$\pm \cdot 036$
·95 - ·10	1215	$\pm \cdot 047$

The last figure must be too large, because the ob-

servations cover the steep rising branch and consequently a correction should be applied for the genuine change in brightness. The interval between two consecutive observations is on the average about $d \cdot 0016$, which corresponds with a change in brightness of $m \cdot 068$ on the steepest part of the light-curve. As the observations cover also a part of the minimum and maximum the correction has been computed on the rather arbitrary assumption that one third of the observations must be corrected for the full amount, whereas the remaining two thirds do not need a correction. The mean error which results in this way is $\pm m \cdot 038$. Taking all evidence together we conclude that the mean accidental error is $\pm m \cdot 036$. This value, combined with a probable mean systematic plate error of $\pm m \cdot 032$, is too small to explain the mean error of a single epoch, as derived from the least squares solution. Therefore the systematic plate errors must be larger than has been anticipated or there must exist real fluctuations in the light-variation of the variable which have not been taken into account. It may be that the secondary light-variation has a more complicated character than the assumed sine-curve, that a secular or long period change of the period still makes itself felt in the six years of observation or that other minor variations of unknown type have remained undiscovered.

The existence of real variations in the light-curve,

FIGURE 3



¹⁾ The corresponding figures derived from the observations by the writer for RR Leonis are: $\pm d \cdot 0009$ and $\pm m \cdot 046$. (See B.A.N. No. 293, 124, 1937.)

apart from those which are due to the secondary period of 537 days, can be tested by means of the inclination or slope of the rising branch. It is seen that the coefficient of t in the second column of Table 3 is closely correlated with the phase ψ of the secondary

period. A least squares solution yields the following relation:

$$\text{inclination} = +416 - 55 \sin 2\pi\psi + 61 \cos 2\pi\psi \\ + 8 + 11 \quad + 12 \quad \text{m.e.}$$

TABLE 7

<i>n</i>	mean phase	mean bright- ness	<i>n</i>	mean phase	mean bright- ness	<i>n</i>	mean phase	mean bright- ness	<i>n</i>	mean phase	mean bright- ness	<i>n</i>	mean phase	mean bright- ness
P' = '006 <i>n</i> = 111			P <i>n</i> = 44			P <i>n</i> = 44			P <i>n</i> = 44			P' = '796 <i>n</i> = 105		
	P	m	5	'0910	- '764	10	'7057	+ '548	20	'9818	+ '544		P	m
10	'9249	+ '688	5	'1038	- '764	10	'7277	+ '553	10	'9893	+ '506	10	'9634	+ '694
10	'9565	+ '639	6	'1197	- '710	10	'7498	+ '538	10	'9953	+ '472	10	'9881	+ '625
10	'9786	+ '527	P' = '261 <i>n</i> = 44			10	'7718	+ '560	10	'0001	+ '385	10	'0057	+ '552
10	'9970	+ '416				10	'7939	+ '562	10	'0056	+ '343	5	'0170	+ '448
5	'0106	+ '280	5	'9544	+ '506	10	'8184	+ '600	10	'0105	+ '287	5	'0250	+ '306
5	'0200	+ '180	5	'9726	+ '306	11	'8455	+ '643	10	'0155	+ '251	5	'0324	+ '176
5	'0302	+ '046	5	'9910	+ '098	10	'8686	+ '636	10	'0213	+ '138	5	'0400	+ '078
5	'0400	- '112	5	'0094	- '160	10	'8948	+ '610	10	'0276	+ '047	5	'0478	- '074
5	'0494	- '284	5	'0276	- '322	10	'9140	+ '617	10	'0335	- '050	5	'0554	- '258
5	'0584	- '412	5	'0460	- '510	10	'9279	+ '564	10	'0398	- '170	5	'0628	- '376
5	'0678	- '542	5	'0644	- '608	10	'9411	+ '558	10	'0457	- '283	5	'0710	- '522
5	'0766	- '630	4	'0808	- '678	10	'9515	+ '524	10	'0522	- '373	5	'0782	- '588
5	'0864	- '684	5	'0976	- '658	10	'9647	+ '387	10	'0599	- '475	5	'0858	- '650
6	'1043	- '740	P' = '314 <i>n</i> = 347			10	'9786	+ '221	10	'0676	- '576	5	'0938	- '740
5	'1250	- '730				10	'9921	+ '084	10	'0742	- '662	5	'1046	- '766
5	'1434	- '654	10	'5297	+ '447	10	'0062	- '101	10	'0797	- '704	5	'1160	- '790
5	'1616	- '554	10	'5663	+ '432	10	'0230	- '329	10	'0855	- '724	5	'1276	- '758
5	'1802	- '488	10	'6271	+ '508	10	'0451	- '548	10	'0903	- '757	5	'1416	- '726
P' = '052 <i>n</i> = 136			10	'6664	+ '512	10	'0669	- '704	10	'0963	- '766	P' = '953 <i>n</i> = 376		
			10	'7032	+ '484	10	'0835	- '721	10	'1022	- '773			
10	'9349	+ '690	10	'7398	+ '492	10	'0972	- '693	10	'1101	- '802	10	'5201	+ '381
10	'9525	+ '669	10	'8669	+ '602	10	'1109	- '688	10	'1188	- '763	10	'5623	+ '451
10	'9655	+ '614	10	'8877	+ '629	10	'1299	- '648	10	'1300	- '691	10	'5990	+ '467
10	'9787	+ '548	10	'9077	+ '683	10	'3172	+ '003	10	'1422	- '648	10	'8088	+ '577
10	'9918	+ '425	10	'9312	+ '612	10	'3538	+ '111	10	'1553	- '610	10	'8455	+ '651
10	'0050	+ '288	10	'9451	+ '529	10	'3924	+ '212	10	'1680	- '557	10	'8822	+ '724
5	'0148	+ '184	10	'9531	+ '466	10	'4309	+ '277	10	'1804	- '502	10	'9146	+ '725
5	'0212	+ '060	10	'9608	+ '396	10	'4743	+ '354	10	'1924	- '466	10	'9337	+ '707
5	'0280	- '036	10	'9690	+ '347	P' = '577 <i>n</i> = 75			10	'2046	- '434	10	'9472	+ '742
5	'0342	- '112	10	'9766	+ '240	6	'9548	+ '553	10	'2169	- '369	10	'9598	+ '734
5	'0410	- '270	10	'9850	+ '091	6	'9657	+ '463	10	'2290	- '318	10	'9694	+ '713
5	'0476	- '388	10	'9949	- '003	5	'9760	+ '442	10	'2424	- '285	10	'9779	+ '650
5	'0540	- '454	10	'0049	- '140	5	'9850	+ '416	10	'2589	- '225	10	'9849	+ '632
5	'0606	- '572	10	'0148	- '260	5	'9940	+ '300	10	'2724	- '180	10	'9914	+ '603
5	'0670	- '604	10	'0245	- '351	5	'0034	+ '174	10	'2977	- '082	10	'9980	+ '522
5	'0740	- '696	10	'0321	- '424	5	'0236	- '142	10	'3178	- '047	10	'0066	+ '470
5	'0802	- '730	10	'0403	- '490	5	'0330	- '344	10	'3178	- '047	10	'0145	+ '403
5	'0868	- '812	10	'0500	- '550	5	'0420	- '420	10	'3362	+ '003	10	'0221	+ '324
5	'0948	- '772	10	'0598	- '585	5	'0510	- '550	10	'3610	+ '086	10	'0286	+ '218
5	'1068	- '712	10	'0700	- '631	5	'0604	- '636	11	'3995	+ '191	10	'0352	+ '134
6	'1312	- '615	10	'0805	- '595	6	'0703	- '737	11	'4398	+ '227	10	'0419	+ '018
P' = '128 <i>n</i> = 102			10	'0940	- '606	6	'0905	- '728	10	'4967	+ '346	10	'0486	- '101
			10	'1107	- '537	6	'1033	- '752	P' = '737 <i>n</i> = 79			10	'0582	- '288
10	'9596	+ '584	9	'2580	- '107	P' = '677 <i>n</i> = 692			5	'9658	+ '674	10	'0660	- '406
10	'9788	+ '384	9	'2911	- '038				5	'9790	+ '650	10	'0741	- '545
5	'9908	+ '272	9	'3241	+ '050	20	'5518	+ '444	5	'9906	+ '574	10	'0820	- '653
5	'9972	+ '186	10	'3590	+ '163	20	'6302	+ '480	5	'0018	+ '464	10	'0900	- '760
5	'0036	+ '168	10	'4028	+ '233	20	'7066	+ '534	5	'0134	+ '346	10	'1013	- '797
5	'0102	+ '074	10	'4562	+ '321	20	'7616	+ '602	5	'0248	+ '192	10	'1285	- '739
5	'0168	- '010	10	'4928	+ '388	20	'8020	+ '630	5	'0366	- '010	10	'1768	- '566
5	'0234	- '078	P' = '382 <i>n</i> = 351			20	'8388	+ '705	5	'0478	- '200	6	'2062	- '442
5	'0298	- '208				20	'8766	+ '713	5	'0592	- '420	10	'2355	- '332
5	'0366	- '280	10	'5154	+ '425	20	'9082	+ '728	5	'0708	- '536	10	'2722	- '205
5	'0426	- '372	10	'5522	+ '427	20	'9288	+ '698	5	'0824	- '690	10	'3119	- '071
5	'0502	- '456	10	'5888	+ '439	20	'9419	+ '680	5	'0936	- '762	10	'3603	+ '073
5	'0588	- '504	10	'6260	+ '462	20	'9522	+ '660	5	'1052	- '822	10	'3971	+ '190
5	'0674	- '656	10	'6616	+ '498	20	'9612	+ '651	5	'1166	- '834	10	'4338	+ '253
6	'0778	- '693	10	'6837	+ '499	20	'9718	+ '614	5	'1314	- '784	10	'4705	+ '338
									4	'1510	- '710			

FIGURE 4a

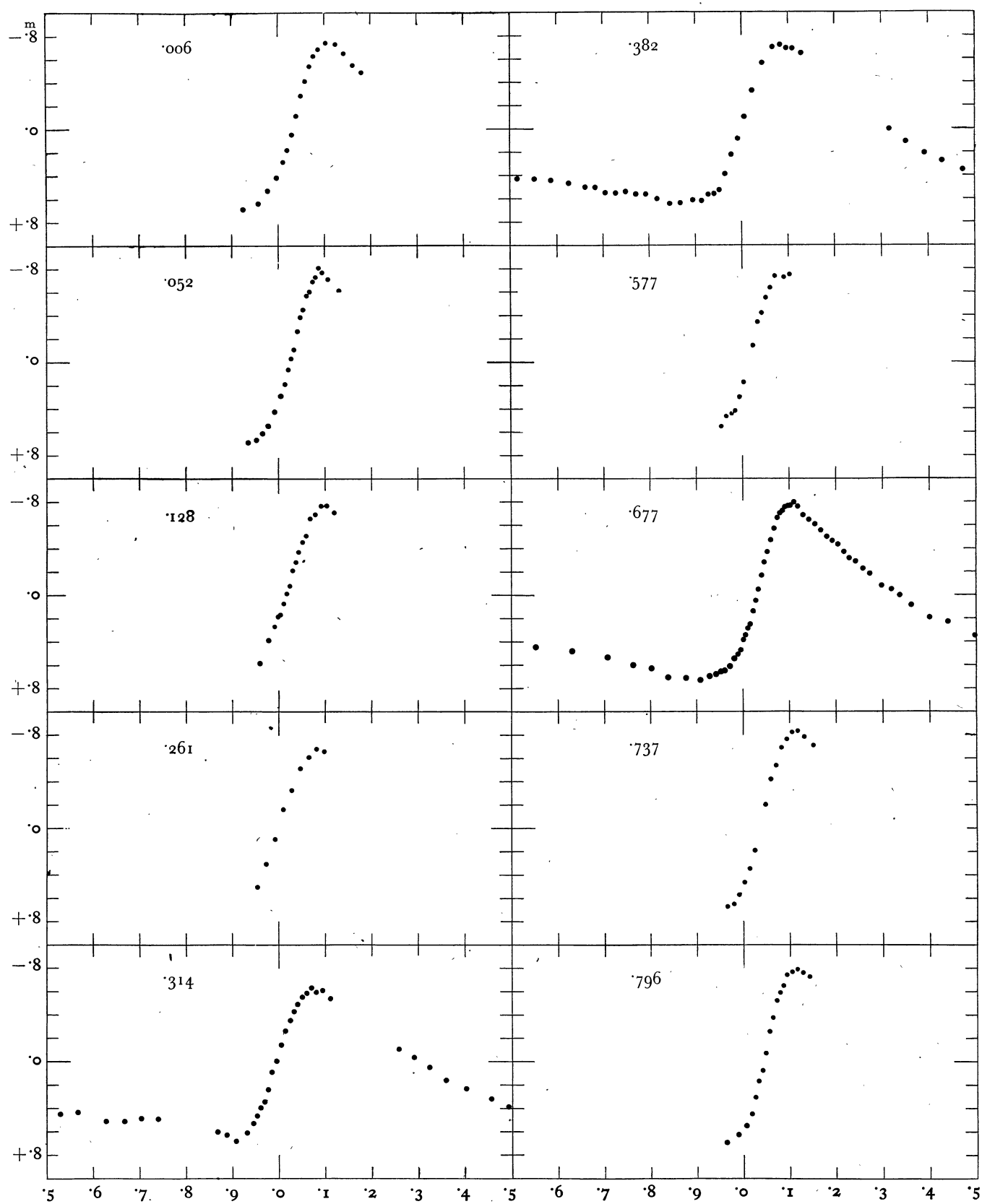
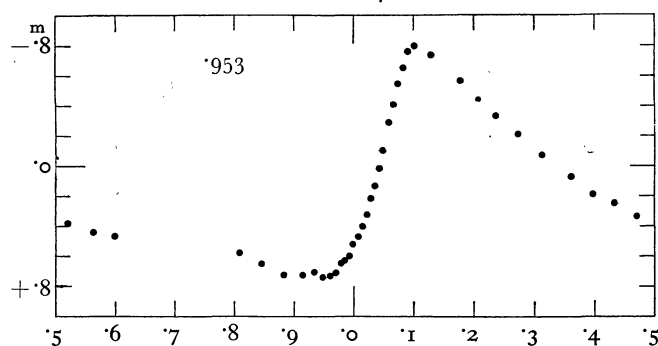


FIGURE 4b



The details are given in Table 6 and the relation is shown in Figure 3. The figures in the first column have been taken from Table 3 after multiplication with the factor 10^5 . The phase ψ is the product of t and $(1424)^{-1}$. In order to compare this phase with that of Table 9, which has been used further below, $\cdot 918$ should be added. The deviations of the individual points from the sine-curve are considerable as compared with the amplitude of 41 . The mean error is found to be ± 46 . When the second Fourier terms are included in the solution, their coefficients appear to be much smaller than their mean error, which indicates that the sine-curve is a sufficient approximation. It is noteworthy that the mean error of the inclinations, as computed from the individual observations, is considerably smaller than the figure derived here from the deviations of the sine-curve. In the second column of Table 3 the mean error has been given for the inclination of every rising branch. The mean error derived from the figures in this table is ± 30 . As the inclinations have been computed with one or two exceptions only from observations taken on the same plate, it seems unlikely that systematic plate errors should have any influence on this result. Still this indication that the variable should show variations in the light-curve, which are not accounted for by the secondary period of 537 days, is in itself quite weak and needs further confirmation.

Next mean light-curves have been formed for different values of the phase ψ of the secondary period. The observations have been divided into eleven groups, the phase limits of which are:

group	n	phase	group	n	phase
1	111	$\cdot 002 - \cdot 012$	7	75	$\cdot 577$
2	136	$\cdot 043 - \cdot 064$	8	692	$\cdot 653 - \cdot 698$
3	102	$\cdot 107 - \cdot 143$	9	79	$\cdot 735 - \cdot 739$
4	44	$\cdot 261$	10	105	$\cdot 787 - \cdot 819$
5	347	$\cdot 301 - \cdot 342$	11	376	$\cdot 918 - \cdot 965$
6	351	$\cdot 367 - \cdot 411$			

For each group a mean light-curve has been computed. The number of observations, the mean phase and

the mean magnitude of each normal point have been listed in Table 7. The mean light-curves are shown in the Figures 4a and 4b. The dots are of different size corresponding with 5, 10 and 20 observations respectively. All normal points are independent of each other and are direct mean values of observed quantities. The writer has preferred this form of representation over the method chosen by BALÁZS and DETRE¹⁾ for AR Herculis, in which a considerable amount of smoothing has been done. Between the phases $\cdot 95$ and $\cdot 10$ of the ordinary period the observations cover the phase of the secondary period more or less uniformly. For the remaining part of the light-curve the observations are far less complete and the whole light-curve has practically been obtained for the four following values of ψ only, $\cdot 314$, $\cdot 382$, $\cdot 677$ and $\cdot 953$. Accidentally more than a quarter of all observations falls within an interval of $\cdot 045$ of the phase ψ around $\cdot 677$. It is a happy circumstance that two of these light-curves nearly represent the extreme forms which are reached during the course of a secondary period. The figures show clearly that the variations in the shape of the light-curve are of the usual type. When the rising branch begins early its slope is small and the range of the light-variation is a minimum. This is caused as well by a high minimum brightness as by a low maximum. When on the other hand the rising branch comes late, it is steep and the light-range is largest. The light-curve has a rather smooth appearance and the sudden dip just in front of the rising branch in the light-curve for $\psi = \cdot 314$ is certainly not real, but it is caused by the systematic deviation of the observations of plate 6354, which starts at phase $\cdot 874$. When the individual observations of these mean light-curves are plotted, it is evident that there exist systematic differences between several plates. They can hardly be interpreted as differences in the phase ψ , the effect of which usually should be very small.

The mean dispersion of these systematic differences has been determined in the following manner. For each of the mean light-curves those parts have been selected, which are covered by the observations of three or more plates. Then the sum of the squares has been formed of the differences in magnitude between successive observations. After a correction for accidental errors had been applied, the mean dispersion of the systematic plate errors was found to be $\pm m \cdot 067$. This figure is twice as large as that derived from the comparison stars, but in the latter case the assumption that the dispersion increases proportionally with the distance from the mean position of the three main comparison stars may not be fulfilled. On the other

¹⁾ L.c. Figure 6.

hand part of the dispersion found here must be due to differences in the phase ψ , although this effect should be small and is difficult to estimate, whereas also the possibility exists that the light-curve is subject to variations of a still unknown character. The present material is however not sufficient to allow a final decision with regard to this question.

On page 106 we have found that a point on the ascending branch of brightness $\Delta m = .00$ oscillates with a period of 537 days and with an amplitude of $(.0043^2 + .0084^2)^{1/2} = .0094$, or about 13.5 minutes. We shall now investigate in which manner the magnitude varies for a point of given phase. Due to the distribution of the observations over the phase ψ this can only be done for that part of the light-curve which is comprised between the phases .95 and .10. Practically this covers the minimum, the rising branch and the maximum. The magnitude at certain equidistant phases has been read from the mean light-curves. The results are given in Table 8. A better picture of these variations can be obtained from Figure 5. Starting at the top of the figure, which means near the minimum of the light-curve, the range is about two tenths of a magnitude, the maximum being near phase .35, the minimum near .85. Progressing towards larger phase values we find an increasing range, which reaches a maximum in the neighbourhood of phase .025, when it amounts to nearly three quarters of a magnitude. Thereafter it rapidly decreases, while the form of the curve begins to deviate from a simple sine-curve, the minimum being clearly sharper than the maximum. The phases of minimum and maximum however remain unchanged. This is no longer the case in the last two diagrams of Figure 5. In the first of these the minimum near phase .85 is still present, but instead of the maximum near phase .35 there is now an indication of a second minimum. In the last diagram, which practically represents the maximum of the light-curve, this second minimum has become a minimum in the absolute sense, whereas that near .85 has disappeared altogether. Thus the smallest brightness of the variable near minimum occurs at the same phase ψ as the largest value near maximum. The range of maximum brightness has not been determined very well, but it seems to be about $m.15$. This means that the range of the light-curve varies to an amount of about one third of a magnitude, its extreme values being $m.50$ and $m.20$.

These are the main features, which can be derived from the present material. Before some remarks will be made about the older observations, it should be emphasized that RS Bootis is an interesting variable, not only on account of its secondary period and the phenomena related therewith, but also because of the fact that its light-curve should be classified as type *a* or

FIGURE 5

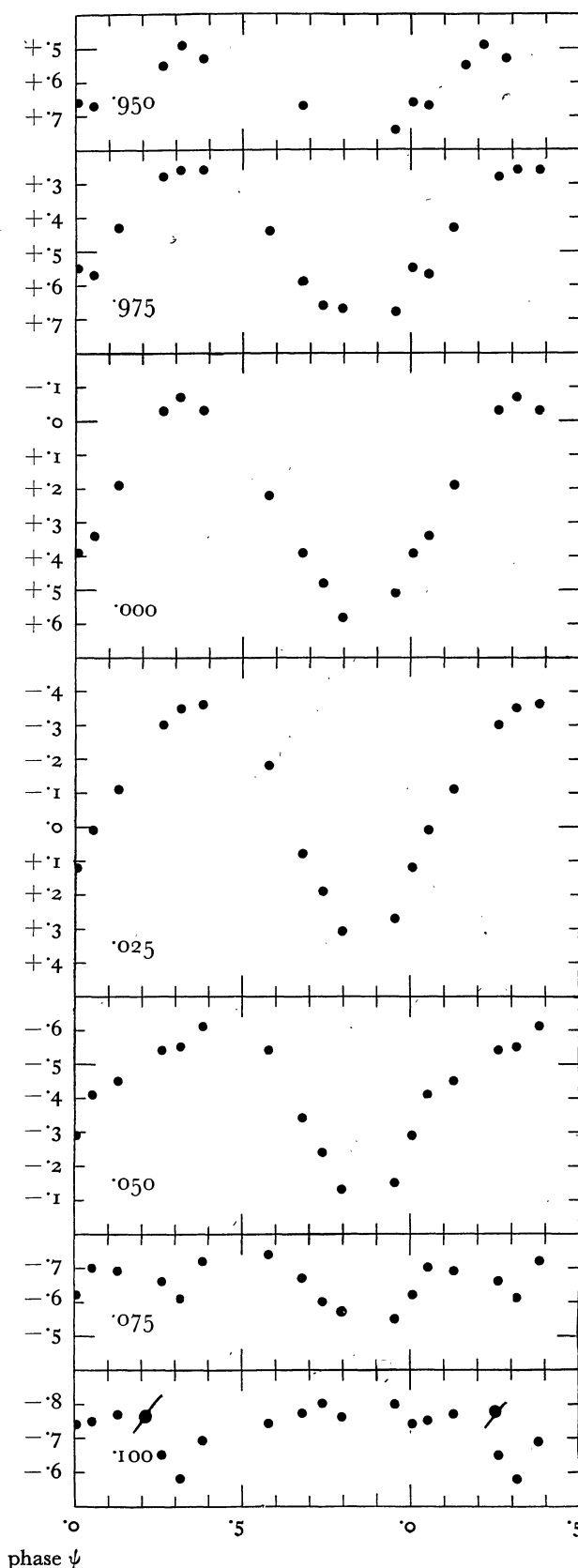


TABLE 8

$\begin{matrix} P' \\ P \end{matrix}$	.006	.052	.128	.261	.314	.382	.577	.677	.737	.796	.953
.950	^m + .66	^m + .67	^m —	^m + .55	^m + .49	^m + .53	^m —	^m + .67	^m —	^m —	^m + .74
.975	+ .55	+ .57	+ .43	+ .28	+ .26	+ .26	+ .44	+ .59	+ .66	+ .67	+ .68
.000	+ .39	+ .34	+ .19	— .03	— .07	— .03	+ .22	+ .39	+ .48	+ .58	+ .51
.025	+ .12	+ .01	— .11	— .30	— .35	— .36	— .18	+ .08	+ .19	+ .31	+ .27
.050	— .29	— .41	— .45	— .54	— .55	— .61	— .54	— .34	— .24	— .13	— .15
.075	— .62	— .70	— .69	— .66	— .61	— .72	— .74	— .67	— .60	— .57	— .55
.100	— .74	— .75	— .77	— .65	— .58	— .69	— .74	— .77	— .80	— .76	— .80

b in BAILEY's scheme notwithstanding the short period of .38 days. No such star is known in any of the globular clusters and although RS Bootis does not stand alone in this respect among the RR Lyrae-type variables, which are scattered among the stars of our galaxy, this combination of period and type seems to be very rare.

The older observations consist of different series, obtained visually or photographically, which are all rather limited in number as well as in the time interval covered by them. Consequently they are of little help in the derivation of a more accurate value for the two periods in question. The oldest and most extensive series of observations, which covers somewhat over three years, consists of visual measures by SEARES, HAYNES and SHAPLEY ¹⁾. When mean light-curves are computed for different phases of the secondary period, some characteristic differences are evident, especially with regard to the phase of the rising branch, but the material seems insufficient to improve the secondary period by the combination of these old observations with the present data. Of the intermediate observations some are of considerable accuracy, such as the photographic and photovisual series by SEARES and SHAPLEY ²⁾ and the photographic observations of JORDAN ³⁾. It must therefore

be regretted that these observations cover a very short time interval and consequently they provide information about the light-curve for a single value of the phase ψ of the secondary period only. The observations clearly indicate that this phase ψ has a different value for both series of observations.

While the existing material would be hardly sufficient for the determination of improved values of both periods, if the assumption of their constancy proved to be correct, the situation is still complicated by a possible secular or long period variation of the ordinary period. Amongst others the following values have been derived:

SEARES and SHAPLEY	^d 37733506 ± 52 m.e.	1907—1914
DOMBROWSKI ¹⁾	37733530 ± 11	1907—1932
OOSTERHOFF	37733657 ± 18	1938—1944

In the determination of the first two figures and of their mean errors the secondary period has not been taken into account, but the difference between the old and new values of the period seems to be too large to be explained by the omission of the influence of the secondary period. A secular or long period change in period is therefore rather probable. Additional observations will be necessary to determine this secular increase of the period with some accuracy.

¹⁾ *Ap. J.* **48**, 215, 1918; *Mt Wilson Contr.* No. 159.

²⁾ L.C.

³⁾ *Allegheny Publ.* **7**, 25, 1929.

¹⁾ NISHNI-NOVGOROD, *Veränderliche Sterne*, **4**, No. 4, 1933.

TABLE 9

J. D. Hel. — 2400000	Δm	phase	J. D. Hel. — 2400000	Δm	phase	J. D. Hel. — 2400000	Δm	phase	J. D. Hel. — 2400000	Δm	phase
plate 4348		·918	d 28977·5744	m + ·20	P ·035	d 29326·6093	m — ·31	P ·031	d 29373·3798	m + ·52	P ·980
d 28972·6330	m + ·72	P ·939	·5752	+ ·16	·037	·6100	— ·37	·033	·3805	+ ·52	·982
·6344	+ ·79	·943	·5761	+ ·15	·039	·6107	— ·34	·035	·3812	+ ·63	·984
·6358	+ ·77	·947	·5770	+ ·08	·042	·6114	— ·44	·037	·3819	+ ·42	·986
·6371	+ ·72	·950	·5778	+ ·01	·044	·6120	— ·36	·038			
·6385	+ ·73	·954	·5787	— ·04	·046	·6127	— ·44	·040	plate 4826		·664
·6399	+ ·65	·958	·5796	— ·03	·048	·6134	— ·42	·042			
·6413	+ ·69	·961	plate 4364		·927	·6141	— ·44	·044	29373·3860	+ ·39	·996
·6427	+ ·66	·965				·6148	— ·44	·046	·3867	+ ·40	·998
·6441	+ ·71	·969	28977·5830	— ·15	·057	·6155	— ·56	·047	·3874	+ ·43	·000
·6455	+ ·66	·972	·5839	— ·15	·060	·6162	— ·52	·049	·3888	+ ·34	·004
plate 4349		·918	·5848	— ·21	·062	·6169	— ·56	·051	·3895	+ ·26	·006
28972·6489	+ ·64	·981	·5856	— ·24	·064	·6176	— ·55	·053	·3902	+ ·30	·008
·6503	+ ·66	·985	·5865	— ·27	·067	·6183	— ·56	·055	·3909	+ ·21	·009
·6517	+ ·70	·989	·5873	— ·33	·069	·6190	— ·59	·057	·3916	+ ·13	·011
·6531	+ ·66	·993	·5882	— ·36	·071	·6197	— ·70	·059	·3923	+ ·21	·013
·6545	+ ·55	·996	·5891	— ·39	·074	·6204	— ·63	·060	·3929	+ ·15	·015
·6558	+ ·61	·000	·5899	— ·40	·076	·6210	— ·65	·062	·3936	+ ·13	·017
·6572	+ ·57	·003	·5908	— ·50	·078	·6217	— ·61	·064	·3943	+ ·14	·018
·6586	+ ·46	·007	·5917	— ·49	·081	·6224	— ·69	·066	·3950	+ ·05	·020
·6600	+ ·45	·011	·5925	— ·59	·083	·6231	— ·74	·068	·3957	+ ·03	·022
·6614	+ ·38	·014	·5934	— ·61	·085	·6238	— ·66	·069	·3964	— ·02	·024
plate 4350		·918	·5943	— ·65	·087	·6245	— ·76	·071	·3971	— ·03	·026
28972·6648	+ ·32	·024	·5951	— ·67	·090	·6252	— ·80	·073	·3978	— ·04	·028
·6662	+ ·25	·027	·5960	— ·79	·092	·6259	— ·77	·075	·3985	— ·13	·030
·6676	+ ·21	·031	·5969	— ·82	·094	·6266	— ·66	·077	·3992	— ·08	·031
·6690	+ ·12	·035	plate 4764		·577	plate 4766		·577	·3999	— ·15	·033
·6704	+ ·07	·038	29326·5788	+ ·60	·950	29326·6314	— ·72	·090	·4006	— ·18	·035
·6718	+ ·05	·042	·5795	+ ·53	·952	·6321	— ·75	·091	·4013	— ·21	·037
·6732	— ·02	·046	·5802	+ ·62	·954	·6328	— ·79	·093	·4020	— ·24	·039
·6745	— ·08	·049	·5809	+ ·54	·956	·6335	— ·74	·095	·4026	— ·30	·040
·6759	— ·19	·053	·5816	+ ·56	·958	·6342	— ·71	·097	·4033	— ·26	·042
·6773	— ·26	·057	·5823	+ ·47	·959	·6349	— ·74	·099	·4040	— ·34	·044
plate 4362		·927	·5830	+ ·54	·961	·6356	— ·77	·101	·4047	— ·42	·046
28977·5480	+ ·76	·965	·5836	+ ·43	·963	·6363	— ·75	·102	·4054	— ·41	·048
·5489	+ ·73	·967	·5843	+ ·44	·965	·6370	— ·74	·104	·4061	— ·42	·050
·5498	+ ·74	·970	·5850	+ ·49	·967	·6377	— ·82	·106	·4068	— ·44	·052
·5506	+ ·77	·972	·5857	+ ·47	·968	·6384	— ·69	·108	·4075	— ·43	·053
·5515	+ ·70	·974	·5864	+ ·41	·970	plate 4825		·664	plate 4827		·664
·5524	+ ·62	·976	·5871	+ ·57	·972	29373·3604	+ ·75	·929	29373·4116	— ·58	·064
·5532	+ ·65	·979	·5878	+ ·46	·974	·3611	+ ·73	·930	·4123	— ·56	·066
·5541	+ ·66	·981	·5885	+ ·44	·976	·3618	+ ·80	·932	·4137	— ·65	·070
·5550	+ ·65	·983	·5892	+ ·40	·978	·3625	+ ·80	·934	·4144	— ·78	·072
·5558	+ ·70	·985	·5899	+ ·34	·980	·3632	+ ·79	·936	·4151	— ·72	·074
·5567	+ ·64	·988	·5906	+ ·41	·981	·3639	+ ·72	·938	·4158	— ·71	·075
·5576	+ ·58	·990	·5913	+ ·34	·983	·3646	+ ·76	·940	·4165	— ·78	·077
·5584	+ ·61	·992	·5920	+ ·47	·985	·3652	+ ·75	·941	·4172	— ·71	·079
·5593	+ ·56	·995	·5927	+ ·48	·987	·3659	+ ·67	·943	·4179	— ·79	·081
·5602	+ ·51	·997	·5933	+ ·38	·989	·3666	+ ·70	·945	·4186	— ·75	·083
·5610	+ ·54	·999	·5940	+ ·29	·990	·3673	+ ·68	·947	·4193	— ·74	·085
·5619	+ ·48	·002	·5947	+ ·38	·992	·3680	+ ·68	·949	·4200	— ·76	·087
plate 4363		·927	·5954	+ ·30	·994	·3687	+ ·66	·951	·4207	— ·83	·088
28977·5657	+ ·46	·012	·5961	+ ·30	·996	·3694	+ ·78	·952	·4213	— ·80	·090
·5666	+ ·40	·014	·5968	+ ·23	·998	·3701	+ ·69	·954	·4220	— ·79	·092
·5674	+ ·39	·016	·5975	+ ·25	·000	·3708	+ ·56	·956	·4227	— ·71	·094
·5683	+ ·37	·019	·5982	+ ·29	·002	·3715	+ ·60	·958	·4234	— ·81	·096
·5692	+ ·35	·021	·5989	+ ·11	·003	·3722	+ ·63	·960	·4241	— ·83	·097
·5700	+ ·33	·023	·5996	+ ·03	·005	·3729	+ ·71	·962	·4248	— ·76	·099
·5709	+ ·28	·025	·6003	+ ·19	·007	·3736	+ ·76	·964	·4255	— ·79	·101
·5718	+ ·27	·028	plate 4765		·577	·3743	+ ·64	·965	·4262	— ·83	·103
·5726	+ ·31	·030	29326·6051	— ·09	·020	·3749	+ ·59	·967	·4269	— ·86	·105
·5735	+ ·18	·032	·6058	— ·11	·022	·3756	+ ·70	·969	·4276	— ·87	·107
			·6065	— ·10	·024	·3763	+ ·55	·971	·4283	— ·83	·109
			·6072	— ·21	·025	·3770	+ ·60	·973	·4290	— ·82	·110
			·6079	— ·20	·027	·3777	+ ·67	·974	·4297	— ·76	·112
			·6086	— ·26	·092	·3784	+ ·55	·976	·4303	— ·76	·114
						·3791	+ ·53	·978	·4310	— ·86	·116
									·4317	— ·79	·118
									·4324	— ·80	·119

TABLE 9 (continued)

J. D. Hel. — 2400000	Δm	phase	J. D. Hel. — 2400000	Δm	phase	J. D. Hel. — 2400000	Δm	phase	J. D. Hel. — 2400000	Δm	phase
plate 4837		·677	^d 29694 ^d 4877	^m + ·38	^P ·965	^d 29726 ^d 5643	^m + ·31	^P ·973	^d 29730 ^d 3629	^m — ·47	^P ·040
^d 29380 ^d 5082	^m + ·72	^P ·871	4891	+ ·33	·969	5657	+ ·24	·977	3643	— ·56	·044
5096	+ ·74	·875	4905	+ ·29	·973	5670	+ ·25	·980	3657	— ·57	·048
5121	+ ·79	·882	4919	+ ·29	·976	5684	+ ·19	·984	3671	— ·57	·051
			4932	+ ·24	·980	5698	+ ·10	·988	3684	— ·62	·055
plate 4838		·677	4946	+ ·19	·984	5712	+ ·13	·992	3698	— ·62	·058
			4960	+ ·13	·987	5726	+ ·02	·995	3712	— ·58	·062
^d 29380 ^d 5219	^m + ·77	^P ·908	4974	+ ·10	·991	5740	+ ·03	·999	3726	— ·60	·066
5226	+ ·71	·909	4988	+ ·04	·995	5754	— ·13	·003	3740	— ·60	·070
5233	+ ·65	·911	5002	+ ·03	·998	5767	— ·12	·006	3754	— ·66	·073
5240	+ ·76	·913	5015	— ·11	·002	5781	— ·15	·010	3768	— ·60	·077
5247	+ ·79	·915	5029	— ·11	·006	5795	— ·24	·014	3781	— ·58	·080
5254	+ ·81	·917	5043	— ·16	·009	5809	— ·20	·017	3795	— ·63	·084
5261	+ ·65	·919	5057	— ·19	·013	5823	— ·27	·021	3809	— ·61	·088
5268	+ ·70	·921	5071	— ·23	·017	5837	— ·31	·025	3823	— ·62	·092
5275	+ ·57	·922	5085	— ·27	·020	5851	— ·29	·028	3837	— ·62	·095
5282	+ ·64	·924	5099	— ·27	·024	5864	— ·35	·032	3851	— ·63	·099
5288	+ ·67	·926	5112	— ·33	·028	5878	— ·36	·036	3864	— ·57	·102
5295	+ ·64	·928	5126	— ·37	·031	5892	— ·37	·039			
5302	+ ·67	·930	5140	— ·37	·035	5906	— ·39	·043	plate 5349		·367
5309	+ ·67	·931	5154	— ·44	·039	5920	— ·43	·047			
5316	+ ·61	·933	5168	— ·46	·042	5934	— ·40	·050	^d 29751 ^d 4567	^m + ·71	^P ·942
5323	+ ·66	·935	5182	— ·50	·046	5947	— ·44	·054	4581	+ ·70	·946
5330	+ ·60	·937	5196	— ·58	·050	5961	— ·46	·058	4595	+ ·69	·949
5337	+ ·67	·939	5209	— ·57	·053	5975	— ·41	·061	4609	+ ·60	·953
5344	+ ·58	·941	5223	— ·56	·057	5989	— ·47	·065	4623	+ ·56	·957
5351	+ ·59	·943	5237	— ·60	·061	6003	— ·47	·069	4637	+ ·46	·961
5358	+ ·64	·944	5251	— ·60	·064	6017	— ·49	·072	4651	+ ·44	·964
5365	+ ·64	·946	5265	— ·62	·068	6031	— ·48	·076	4664	+ ·36	·968
5372	+ ·72	·948	5279	— ·66	·072	6044	— ·54	·080	4678	+ ·34	·971
5378	+ ·58	·950	5292	— ·61	·075	6058	— ·53	·083	4692	+ ·26	·975
5385	+ ·70	·952	5306	— ·70	·079	6072	— ·50	·087	4706	+ ·29	·979
5392	+ ·55	·953	5320	— ·70	·083	6086	— ·54	·091	4720	+ ·28	·983
5399	+ ·68	·955	5334	— ·70	·086	6100	— ·58	·094	4734	+ ·27	·986
5406	+ ·68	·957	5348	— ·70	·090	6114	— ·61	·098	4747	+ ·16	·990
5413	+ ·61	·959	5362	— ·60	·094	6128	— ·54	·102	4761	+ ·14	·993
5420	+ ·57	·961	5376	— ·64	·098	6141	— ·55	·105	4775	+ ·09	·997
5427	+ ·58	·963	5389	— ·69	·101	6155	— ·58	·109	4789	+ ·02	·001
5434	+ ·63	·965	5403	— ·66	·105	6169	— ·57	·113	4803	— ·02	·005
			plate 5320		·310	6183	— ·49	·116	4817	— ·00	·008
plate 4839		·677	^d 29720 ^d 5121	^m + ·66	^P ·934	6197	— ·43	·120	4831	— ·08	·012
			5135	+ ·63	·938	6211	— ·43	·124	4844	— ·19	·015
^d 29380 ^d 5475	^m + ·66	^P ·975	5162	+ ·57	·945	plate 5331		·328	4858	— ·29	·019
5482	+ ·63	·977	5176	+ ·58	·949				4872	— ·23	·023
5489	+ ·54	·979	5190	+ ·48	·952	^d 29730 ^d 3269	^m + ·45	^P ·945	4886	— ·34	·027
5496	+ ·61	·981	5204	+ ·43	·956	3283	+ ·50	·948	4900	— ·31	·030
5503	+ ·48	·983	5218	+ ·32	·960	3297	+ ·41	·952	4914	— ·40	·034
5510	+ ·50	·985	5232	+ ·44	·963	3310	+ ·48	·956	4928	— ·48	·038
5517	+ ·42	·987	5246	+ ·37	·967	3324	+ ·39	·959	4941	— ·49	·041
5524	+ ·50	·988	5259	+ ·35	·971	3338	+ ·37	·963	4955	— ·56	·045
5531	+ ·48	·990	5273	+ ·31	·974	3352	+ ·38	·967	4969	— ·58	·049
5538	+ ·49	·992	5287	+ ·30	·978	3366	+ ·33	·970	4983	— ·64	·052
5545	+ ·48	·994	5301	+ ·23	·982	3380	+ ·20	·974	4997	— ·64	·056
5552	+ ·39	·996	5400	+ ·33	·024	3394	+ ·19	·978	5011	— ·69	·060
5559	+ ·42	·998	5474	— ·34	·028	3407	+ ·13	·981	5024	— ·63	·063
5565	+ ·33	·999	5488	— ·36	·031	3421	+ ·15	·985	5038	— ·65	·067
5572	+ ·30	·001	5502	— ·45	·035	3435	+ ·05	·989	5052	— ·64	·071
5579	+ ·31	·003	5516	— ·45	·039	3449	+ ·04	·992	5066	— ·61	·074
5600	+ ·27	·009				3463	— ·01	·996	5080	— ·64	·078
5607	+ ·24	·010	plate 5330		·321	3477	— ·06	·000	5094	— ·68	·082
5614	+ ·22	·012	^d 29726 ^d 5532	^m + ·61	^P ·944	3491	— ·13	·004	5108	— ·65	·085
5621	+ ·19	·014	5546	+ ·56	·948	3504	— ·20	·007	5121	— ·66	·089
plate 5297		·261	5560	+ ·48	·951	3518	— ·20	·011	5135	— ·67	·093
			5574	+ ·51	·955	3532	— ·22	·014	5149	— ·68	·096
^d 29694 ^d 4808	^m + ·59	^P ·947	5587	+ ·39	·958	3546	— ·22	·018	5163	— ·65	·100
4822	+ ·55	·951	5601	+ ·42	·962	3560	— ·28	·022	5177	— ·65	·104
4835	+ ·54	·954	5615	+ ·39	·966	3574	— ·37	·026	5191	— ·63	·107
4849	+ ·53	·958	5629	+ ·38	·970	3587	— ·41	·029	5204	— ·69	·111
4863	+ ·32	·962				3601	— ·40	·033	5218	— ·68	·115
						3615	— ·42	·036			

TABLE 9 (continued)

J. D. Hel. - 2400000	Δm	phase	J. D. Hel. - 2400000	Δm	phase	J. D. Hel. - 2400000	Δm	phase	J. D. Hel. - 2400000	Δm	phase
plate 5354		370	d 29755 4139	m + 27	P 429	d 29755 5122	m + 48	P 690	d 6106	m + 41	P 950
d 29752 5724	m + 60	P 899	4153	+ 29	433	5136	+ 51	693	plate 5363		382
5738	+ 59	902	4167	+ 31	437	5150	+ 54	697	29759 4313	- 77	076
5752	+ 65	906	4180	+ 34	440	5164	+ 55	701	4327	- 78	080
5766	+ 66	910	4194	+ 33	444	5178	+ 52	705	4340	- 79	083
5779	+ 65	913	4208	+ 26	447	5191	+ 57	708	4354	- 73	087
5793	+ 61	917	4222	+ 32	451	5205	+ 56	712	4368	- 72	090
5807	+ 56	921	4236	+ 30	455	5219	+ 56	715	4382	- 68	094
5821	+ 52	924	4250	+ 31	459	5233	+ 54	719	4396	- 72	098
5835	+ 53	928	4263	+ 34	462	5247	+ 53	723	4410	- 69	102
5849	+ 53	932	plate 5360		375	5261	+ 57	727	4424	- 72	105
5863	+ 60	936	29755 4319	+ 37	477	5275	+ 61	730	4437	- 68	109
5876	+ 51	939	4333	+ 35	481	5288	+ 52	734	4451	- 68	112
5890	+ 50	943	4347	+ 43	484	5302	+ 50	737	4465	- 68	116
5904	+ 57	946	4360	+ 41	488	5316	+ 57	741	4479	- 68	120
5918	+ 50	950	4374	+ 36	491	5330	+ 52	745	4493	- 61	124
5932	+ 45	954	4388	+ 35	495	5344	+ 55	749	4507	- 60	127
5946	+ 42	958	4402	+ 36	499	5358	+ 53	752	4521	- 65	131
5959	+ 40	961	4416	+ 40	503	5372	+ 48	756	4534	- 66	134
5973	+ 31	965	4430	+ 41	506	5385	+ 50	759	4548	- 65	138
5987	+ 34	968	4444	+ 43	510	5399	+ 55	763	4562	- 59	142
6001	+ 21	972	4457	+ 41	513	5413	+ 53	767	plate 5553		954
6015	+ 19	976	4471	+ 45	517	5427	+ 51	771	30066 5222	+ 77	914
6029	+ 21	980	4485	+ 44	521	5441	+ 56	774	5236	+ 71	918
6043	+ 04	983	4499	+ 48	525	5455	+ 55	778	5250	+ 81	921
6056	+ 14	987	4513	+ 42	528	5468	+ 51	781	5264	+ 67	925
6070	+ 09	990	4527	+ 45	532	5482	+ 50	785	5278	+ 70	929
6084	- 01	994	4541	+ 41	536	5496	+ 56	789	5292	+ 67	933
6098	- 06	998	4554	+ 45	539	5510	+ 51	793	5306	+ 66	936
6112	- 05	002	4568	+ 45	543	5524	+ 55	796	5319	+ 64	940
6126	- 22	005	4582	+ 38	547	5538	+ 57	800	5333	+ 70	943
6140	- 20	009	4596	+ 43	550	5552	+ 59	804	5347	+ 74	947
6153	- 26	012	4610	+ 39	554	5565	+ 54	807	5361	+ 68	951
plate 5359		375	4624	+ 44	558	5579	+ 58	811	plate 5554		954
29755 3654	- 05	301	4637	+ 47	561	5593		815	30066 5403	+ 78	962
3668	- 01	304	4651	+ 42	565	plate 5362		375	5416	+ 69	965
3682	+ 01	308	4665	+ 43	569	29755 5649	+ 60	829	5430	+ 66	969
3696	+ 03	312	4679	+ 45	572	5662	+ 64	833	5444	+ 73	973
3709	+ 03	315	4693	+ 47	576	5676	+ 53	836	5458	+ 62	977
3723	- 02	319	4707	+ 39	580	5690	+ 57	840	5472	+ 59	980
3737	+ 01	323	4721	+ 44	583	5704	+ 71	844	5486	+ 63	984
3751	+ 01	326	4734	+ 44	587	5718	+ 64	848	5499	+ 54	987
3765	+ 03	330	4748	+ 40	591	5732	+ 62	851	5513	+ 47	991
3779	- 01	334	4762	+ 44	594	5746	+ 64	855	5527	+ 55	995
3793	+ 06	337	4776	+ 37	598	5759	+ 63	858	5541	+ 46	999
3806	+ 09	341	4790	+ 46	602	5773	+ 58	862	plate 5555		954
3820	+ 06	345	4804	+ 53	605	5787	+ 55	866	30066 5583	+ 43	010
3834	+ 14	348	4818	+ 45	609	5801	+ 63	870	5596	+ 44	013
3848	+ 13	352	4831	+ 45	613	5815	+ 62	873	5610	+ 38	017
3862	+ 07	356	4845	+ 44	616	5829	+ 57	877	5624	+ 36	021
3876	+ 09	359	4859	+ 45	620	5842	+ 61	880	5638	+ 26	024
3890	+ 12	363	4873	+ 46	624	5856	+ 58	884	5652	+ 16	028
3903	+ 17	367	4887	+ 44	627	5870	+ 66	888	5666	+ 14	032
3917	+ 18	370	4901	+ 48	631	5884	+ 65	892	5680	+ 10	035
3931	+ 23	374	4914	+ 44	635	5898	+ 62	895	5693	+ 06	039
3945	+ 20	378	4928	+ 48	638	5912	+ 60	899	5707	- 06	043
3959	+ 14	381	plate 5361		375	5926	+ 54	903	5721	- 09	046
3973	+ 17	385	29755 4984	+ 52	653	5939	+ 54	906	plate 5556		954
3986	+ 27	389	4998	+ 43	657	5953	+ 62	910	30066 5763	- 42	057
4014	+ 20	396	5011	+ 51	660	5967	+ 62	914	5776	- 43	061
4028	+ 20	400	5025	+ 48	664	5981	+ 58	917	5790	- 56	065
4042	+ 21	403	5039	+ 44	668	5995	+ 53	921			
4056	+ 26	407	5053	+ 50	671	6009	+ 54	925			
4070	+ 24	411	5067	+ 43	675	6023	+ 51	928			
4083	+ 21	414	5081	+ 48	679	6036	+ 56	932			
4097	+ 25	418	5095	+ 51	683	6050	+ 48	936			
4111	+ 27	422	5108	+ 54	686	6064	+ 45	939			
4125	+ 24	425				6078	+ 45	943			
						6092	+ 42	947			

TABLE 9 (continued)

J. D. Hel. - 2400000	Δm	phase	J. D. Hel. - 2400000	Δm	phase	J. D. Hel. - 2400000	Δm	phase	J. D. Hel. - 2400000	Δm	phase
d 30066 ^d 5804	m - '58	P '068	d 30071 ^d 5357	m - '49	P '201	d 30071 ^d 6354	m + '34	P '465	d 30072 ^d 5524	m + '79	P '895
5818	- '63	'072	5371	- '46	'204	6368	+ '34	'469	5538	+ '80	'899
5832	- '73	'076	5385	- '41	'208	6382	+ '38	'472	5552	+ '76	'902
5846	- '72	'079	5399	- '44	'212	6396	+ '31	'476	5566	+ '70	'906
5860	- '72	'083	5413	- '44	'215	6410	+ '38	'480	5580	+ '75	'910
5873	- '81	'087	5426	- '37	'219	6424	+ '36	'483	5593	+ '67	'913
5887	- '83	'090	5440	- '35	'223	6438	+ '30	'487	5607	+ '69	'917
5901	- '82	'094	5454	- '35	'226	6451	+ '35	'491	5621	+ '75	'921
plate 5580		'963	5468	- '38	'230	6465	+ '40	'494	5635	+ '64	'924
30071 ^d 4519	+ '65	'979	5482	- '36	'234	6479	+ '42	'498	5649	+ '73	'928
4533	+ '63	'982	5496	- '32	'237	plate 5583		'963	5663	+ '76	'932
4547	+ '58	'986	5510	- '31	'241	30071 ^d 6562	+ '35	'520	5677	+ '77	'936
4561	+ '60	'990	5523	- '32	'245	6576	+ '35	'524	5690	+ '75	'939
4575	+ '60	'993	5537	- '27	'248	6590	+ '37	'527	5704	+ '77	'943
4588	+ '49	'997	5551	- '29	'252	6604	+ '41	'531	5718	+ '73	'946
4602	+ '51	'001	5565	- '26	'256	6618	+ '40	'535	5732	+ '73	'950
4616	+ '48	'004	5579	- '26	'259	6632	+ '36	'539	5746	+ '79	'954
4630	+ '43	'008	5593	- '23	'263	6645	+ '40	'542	plate 5620		'002
4644	+ '40	'012	5607	- '24	'267	6659	+ '40	'546	30092 ^d 5563	+ '67	'908
4658	+ '44	'015	5620	- '17	'270	6673	+ '44	'549	5577	+ '73	'912
4672	+ '37	'019	5634	- '20	'274	6687	+ '44	'553	5591	+ '68	'916
4685	+ '30	'023	5648	- '20	'278	6701	+ '43	'557	5604	+ '67	'919
4699	+ '26	'026	5662	- '16	'281	6715	+ '41	'561	5618	+ '70	'923
4713	+ '19	'030	5676	- '19	'285	6728	+ '47	'564	5632	+ '69	'927
4727	+ '15	'034	5690	- '14	'289	6742	+ '42	'568	5646	+ '64	'930
4741	+ '09	'037	5703	- '08	'292	6756	+ '45	'571	5660	+ '68	'934
4755	+ '02	'041	5717	- '11	'296	6770	+ '49	'575	5674	+ '72	'938
4768	- '10	'045	5731	- '13	'300	6784	+ '46	'579	5688	+ '70	'942
4782	- '12	'048	5745	- '11	'303	6798	+ '46	'583	5701	+ '63	'945
4796	- '23	'052	5759	- '10	'307	6812	+ '52	'586	plate 5621		'002
4810	- '27	'056	5773	- '09	'311	6825	+ '44	'590	30092 ^d 5778	+ '57	'965
4824	- '39	'059	5787	- '09	'315	6839	+ '48	'593	5791	+ '55	'969
4838	- '47	'063	5800	- '07	'318	6853	+ '47	'597	5805	+ '55	'973
4852	- '57	'067	plate 5582		'963	6867	+ '47	'601	5819	+ '57	'976
4865	- '58	'070	30071 ^d 5870	'00	'337	6881	+ '47	'605	5833	+ '50	'980
4879	- '64	'074	5884	+ '07	'340	6895	+ '48	'608	5847	+ '46	'984
4893	- '62	'078	5897	+ '01	'344	6909	+ '45	'612	5861	+ '46	'987
4907	- '74	'081	5911	+ '02	'347	6922	+ '43	'615	5875	+ '42	'991
4921	- '78	'085	5925	+ '04	'351	plate 5590		'965	5888	+ '40	'995
4935	- '75	'089	5939	+ '07	'355	30072 ^d 5136	+ '57	'792	5902	+ '39	'998
4949	- '77	'092	5953	+ '05	'359	5150	+ '59	'796	5916	+ '37	'002
4962	- '79	'096	5967	+ '10	'362	5164	+ '53	'800	5930	+ '36	'006
4976	- '75	'100	5980	+ '13	'366	5178	+ '56	'803	5944	+ '31	'009
4990	- '72	'103	5994	+ '10	'369	5192	+ '53	'807	5958	+ '22	'013
5004	- '72	'107	6008	+ '10	'373	5206	+ '65	'811	5971	+ '23	'017
5018	- '77	'111	6022	+ '11	'377	5219	+ '57	'814	5985	+ '16	'020
5032	- '79	'114	6036	+ '16	'381	5233	+ '57	'818	5999	+ '06	'024
5046	- '79	'118	6050	+ '18	'384	5247	+ '61	'822	6013	+ '06	'028
5059	- '76	'122	6064	+ '18	'388	5261	+ '59	'825	6027	+ '01	'031
5073	- '76	'125	6077	+ '15	'391	5275	+ '61	'829	6041	- '02	'035
5087	- '74	'129	6091	+ '16	'395	5289	+ '61	'833	6055	- '13	'039
5101	- '74	'133	6105	+ '20	'399	5303	+ '63	'836	6068	- '12	'042
5115	- '71	'136	6119	+ '17	'403	5316	+ '63	'840	6082	- '22	'046
5129	- '67	'140	6133	+ '25	'406	5330	+ '61	'844	6096	- '29	'050
plate 5581		'963	6147	+ '21	'410	5344	+ '67	'847	6110	- '29	'053
30071 ^d 5191	- '66	'157	6161	+ '24	'414	5358	+ '67	'851	6124	- '36	'057
5205	- '68	'160	6174	+ '24	'417	5372	+ '70	'855	6138	- '44	'061
5219	- '65	'164	6188	+ '19	'421	5386	+ '69	'858	6152	- '47	'065
5233	- '66	'168	6202	+ '21	'425	5399	+ '69	'862	6165	- '53	'068
5246	- '59	'171	6216	+ '25	'428	5413	+ '67	'866	6179	- '56	'072
5260	- '51	'175	6230	+ '32	'432	5427	+ '71	'869	6193	- '56	'075
5274	- '52	'179	6244	+ '30	'436	5441	+ '79	'873	6207	- '63	'079
5288	- '54	'182	6258	+ '28	'439	5455	+ '72	'877	6221	- '61	'083
5302	- '52	'186	6271	+ '27	'443	5469	+ '69	'880	6235	- '68	'087
5316	- '47	'190	6285	+ '20	'447	5483	+ '71	'884			
5329	- '52	'193	6299	+ '27	'450	5496	+ '69	'888			
5343	- '41	'197	6313	+ '29	'454	5510	+ '67	'891			
			6327	+ '32	'458						
			6341	+ '36	'461						

TABLE 9 (continued)

J. D. Hel. — 2400000	Δm	phase	J. D. Hel. — 2400000	Δm	phase	J. D. Hel. — 2400000	Δm	phase	J. D. Hel. — 2400000	Δm	phase
plate 5622		002	d	m	P	d	m	P	d	m	P
30092			5059	— 83	078	30168	+ 36	973	30442	— 35	212
6311	— 78	P	5073	— 84	082	4252	+ 38	977	4620	— 38	216
6325	— 78	107	5087	— 90	086	4269	+ 32	982	4634	— 39	220
6339	— 74	110	5100	— 90	089	4286	+ 35	986	4647	— 36	223
6352	— 74	114				4304	+ 17	991	4661	— 32	227
6366	— 72	118	plate 5677		049	4321	+ 17	996	4675	— 28	231
6380	— 73	121				4338	+ 12	000	4689	— 29	234
6394	— 71	125	30117	+ 69	941	4356	+ 02	005	4703	— 31	238
6408	— 75	129	4741	+ 76	944	4373	+ 05	009	4717		
6422	— 67	132	4755	+ 75	948	4390	— 01	014	plate 5946		653
6435	— 66	136	4769	+ 74	952	4408	— 10	019			
6449	— 66	140	4783	+ 73	956	4425	— 15	023	30442	— 23	258
6463	— 64	143	4796	+ 73	959	4442	— 22	028	4807	— 21	262
6477	— 64	147	4810	+ 74	963	4459	— 29	032	4821	— 19	266
6491	— 58	151	4824	+ 67	966	4477	— 30	037	4834	— 19	269
6505	— 57	154	4838	+ 65	970	4494	— 44	041	4848	— 17	273
6519	— 56	158	4852	+ 62	974	4511	— 45	046	4862	— 16	277
6532	— 58	162	4866	+ 55	978	4529	— 50	051	4876	— 12	280
6546	— 48	165	4880	+ 61	981	4546	— 43	055	4890	— 10	284
6560	— 53	169	4893	+ 48	985	4563	— 54	060	4904	— 12	288
6574	— 49	173	4907	+ 50	988	4581	— 68	064	4917	— 11	291
6588	— 48	176	4921	+ 46	992	4598	— 78	069	4931	— 08	295
6602	— 47	180	4935	+ 44	996	4615	— 74	074	4945	— 02	299
6616	— 47	184	4949	+ 36	000	4633	— 72	078	4959	— 03	302
		188	4963	+ 36	003	4650	— 78	083	4973	— 01	306
plate 5669		043	4976	+ 34	007	4667	— 75	087	4987	— 06	310
30114	+ 64	920	4990	+ 26	010	4685	— 80	092	5001	— 01	313
4463	+ 81	924	5004	+ 23	014	4702	— 81	096	5014	— 03	317
4477	+ 68	928	5018	+ 10	018	4719	— 73	101	5028	— 07	321
4491	+ 59	931	5032	+ 14	022	4736	— 87	106	5042	— 04	324
4505	+ 77	935	5046	+ 05	025	4754	— 87	110	5056	— 05	328
4519	+ 64	939	5060	— 01	029	4771	— 82	115	5070	— 01	332
4533	+ 68	942	5073	— 09	032	4788			5084	+ 04	335
4546	+ 61	946	5087	— 11	036	plate 5945		653	5098	— 02	339
4560	+ 69	950	5101	— 19	040	30442	— 66	080	5111	+ 04	343
4574	+ 59	953	5115	— 26	044	4121	— 66	084	5125	— 02	346
4588	+ 54	957	5129	— 34	047	4135	— 67	088	plate 5947		655
4602	+ 62	961	5143	— 41	051	4149	— 71	091	30443	+ 63	765
4616	+ 60	965	5157	— 45	055	4163	— 70	095	4253	+ 66	769
4630	+ 72	968	5170	— 51	058	4176	— 72	098	4267	+ 63	773
4643	+ 49	972	5184	— 57	062	4190	— 72	102	4281	+ 60	776
4657	+ 60	975	5198	— 63	066	4204	— 76	106	4295	+ 63	780
4671	+ 57	979	5212	— 65	073	4218	— 76	110	4309	+ 64	784
4685	+ 61	983	5226	— 73	080	4232	— 73	117	4322	+ 59	787
4699	+ 51	987	5240	— 76	084	4246	— 72	120	4336	+ 65	791
4713	+ 43	990	5254	— 82	088	4260	— 72	124	4350	+ 67	795
4726	+ 40	994	5267	— 84	091	4273	— 68	128	4364	+ 70	798
4740	+ 33	997	5281	— 80	095	4287	— 70	132	4378	+ 66	802
4754	+ 30	001	5295	— 82	099	4301	— 70	135	4392	+ 68	806
4768	+ 28	005	5309	— 83	102	4315	— 65	143	4406	+ 65	809
4782	+ 24	009	5323			4329	— 64	146	4419	+ 67	813
4796	+ 27	012	5337			4343	— 64	150	4433	+ 73	817
4810	+ 12	016	plate 5714		132	4357	— 68	154	4447	+ 67	820
4823	+ 04	019	30162	+ 28	990	4370	— 62	157	4461	+ 72	824
4837	— 01	023	3962	+ 21	995	4384	— 58	161	4475	+ 73	828
4851	— 06	027	3983	+ 20	006	4398	— 60	165	4489	+ 74	832
4865	— 16	031	4004	+ 03	012	4412	— 56	168	4503	+ 79	835
4879	— 21	034	4025	— 05	017	4426	— 49	172	4516	+ 73	839
4893	— 30	038	4045	— 17	023	4440	— 52	176	4530	+ 70	842
4907	— 46	041	4066	— 21	028	4453	— 51	179	4544	+ 72	846
4920	— 46	045	4087	— 23	034	4467	— 47	183	4558	+ 69	850
4934	— 52	053	4108	— 37	039	4481	— 47	190	4572	+ 72	854
4948	— 62	056	4129	— 43	044	4495	— 43	194	4586	+ 73	857
4962	— 66	060	4149			4509	— 41	198	4599	+ 72	861
4976	— 73	063	plate 5726		143	4523	— 44	201	4613	+ 73	864
4990	— 75	067	30168	+ 48	963	4537	— 42	205	4627	+ 74	868
5003	— 78	071	4217	+ 47	968	4550	— 45	209	4641	+ 72	872
5017	— 86	075	4234			4564			4655	+ 73	876
5031						4578			4669	+ 79	879
5045						4592			4683		

TABLE 9 (continued)

J. D. Hel. - 2400000	Δm	phase	J. D. Hel. - 2400000	Δm	phase	J. D. Hel. - 2400000	Δm	phase	J. D. Hel. - 2400000	Δm	phase
d 30443'4696	+ '71	P '883	d 30443'5708	- '64	P '151	d 30462'4081	- '62	P '073	d 30462'5120	+ '04	P '348
'4710	+ '74	'886	'5721	- '62	'154	'4095	- '67	'076	'5134	+ '02	'352
'4724	+ '81	'890	'5735	- '62	'158	'4109	- '67	'080	'5148	+ '05	'355
'4738	+ '77	'894	'5749	- '63	'162	'4122	- '75	'084	'5162	+ '11	'359
'4752	+ '76	'898	'5763	- '61	'166	'4137	- '75	'088	'5176	+ '09	'363
'4766	+ '69	'901	'5777	- '56	'169	'4151	- '71	'091	'5189	+ '10	'366
'4780	+ '78	'905	'5791	- '56	'173	'4164	- '77	'095	'5203	+ '15	'370
'4793	+ '81	'908	'5805	- '51	'177	'4178	- '75	'098	'5217	+ '18	'374
'4807	+ '76	'912	'5818	- '49	'180	'4192	- '74	'102	'5231	+ '14	'377
'4821	+ '73	'916	'5832	- '57	'184				'5245	+ '14	'381
plate 5948		'655	'5846	- '50	'188	plate 5981		'691	'5259	+ '12	'385
			'5860	- '52	'191				'5272	+ '13	'388
			'5874	- '50	'195	30462'4261	- '68	'120	'5286	+ '15	'392
30443'4883	+ '76	'932	'5888	- '46	'199	'4275	- '72	'124	'5300	+ '16	'396
'4897	+ '68	'936	'5901	- '49	'202	'4289	- '69	'128	'5314	+ '17	'399
'4911	+ '75	'940	'5915	- '42	'206	'4303	- '63	'132	'5328	+ '25	'403
'4925	+ '71	'943	'5929	- '42	'209	'4317	- '64	'135	'5342	+ '25	'407
'4939	+ '76	'947	'5943	- '39	'213	'4331	- '63	'139	'5356	+ '21	'411
'4953	+ '72	'951	'5957	- '37	'217	'4344	- '62	'142	'5369	+ '23	'414
'4967	+ '68	'955	'5971	- '35	'221	'4358	- '60	'146	'5383	+ '29	'418
'4980	+ '72	'958	'5985	- '34	'224	'4372	- '55	'150	'5397	+ '22	'421
'4994	+ '67	'962	'5998	- '30	'228	'4400	- '57	'157	'5411	+ '19	'425
'5008	+ '71	'965	'6012	- '34	'231	'4414	- '58	'161	'5425	+ '25	'429
'5022	+ '64	'969	'6026	- '30	'235	'4428	- '53	'165	'5439	+ '27	'433
'5036	+ '61	'973	'6040	- '24	'239	'4441	- '53	'168	'5453	+ '20	'436
'5050	+ '55	'977	'6054	- '30	'243	'4455	- '50	'172	'5466	+ '18	'440
'5063	+ '58	'980	'6068	- '30	'246	'4469	- '54	'176	'5480	+ '21	'443
'5077	+ '60	'984	'6082	- '23	'250	'4483	- '53	'179	'5494	+ '20	'447
'5091	+ '58	'987	'6095	- '20	'253	'4497	- '47	'183	'5508	+ '24	'451
'5105	+ '50	'991	'6109	- '25	'257	'4511	- '44	'187	'5522	+ '24	'455
'5119	+ '50	'995	'6123	- '17	'261	'4525	- '45	'190	'5536	+ '30	'458
'5133	+ '38	'999	'6137	- '22	'265	'4538	- '47	'194			
'5147	+ '38	'002	'6151	- '22	'268	'4552	- '47	'197	plate 5983		'691
'5160	+ '29	'006				'4566	- '39	'201			
'5174	+ '35	'009	plate 5980		'690	'4580	- '41	'205	30462'5619	+ '35	'480
'5188	+ '33	'013				'4594	- '44	'209	'5633	+ '32	'484
'5202	+ '26	'017	30462'3597	+ '72	'944	'4608	- '36	'212	'5646	+ '32	'487
'5216	+ '19	'021	'3610	+ '71	'948	'4621	- '40	'216	'5660	+ '36	'491
'5230	+ '12	'024	'3624	+ '73	'952	'4635	- '35	'219	'5674	+ '38	'495
'5244	+ '09	'028	'3638	+ '61	'955	'4649	- '35	'223	'5688	+ '33	'499
'5257	+ '02	'031	'3652	+ '62	'959	'4663	- '34	'227	'5702	+ '36	'502
'5271	+ '01	'035	'3666	+ '67	'963	'4677	- '31	'231	'5716	+ '36	'506
'5285	- '08	'039	'3680	+ '53	'966	'4691	- '30	'234	'5730	+ '37	'510
'5299	- '14	'043	'3693	+ '62	'970	'4705	- '34	'238	'5743	+ '31	'513
'5313	- '25	'046	'3707	+ '59	'974	'4718	- '27	'241	'5757	+ '35	'517
'5327	- '26	'050	'3721	+ '56	'977	'4732	- '30	'245	'5771	+ '34	'521
'5341	- '28	'054	'3735	+ '66	'981	'4746	- '26	'249	'5785	+ '43	'524
'5354	- '38	'057	'3749	+ '53	'985	'4760	- '26	'253	'5799	+ '40	'528
'5368	- '42	'061	'3763	+ '59	'988	'4774	- '26	'256	'5813	+ '37	'532
'5382	- '48	'065	'3777	+ '51	'992	'4788	- '24	'260	'5827	+ '46	'535
'5396	- '54	'068	'3790	+ '45	'996	'4802	- '21	'264	'5840	+ '47	'539
'5410	- '55	'072	'3804	+ '41	'999	'4815	- '15	'267	'5854	+ '50	'543
'5424	- '61	'076	'3818	+ '44	'003	'4829	- '20	'271	'5868	+ '43	'546
'5437	- '63	'079	'3832	+ '36	'007	'4843	- '23	'275	'5882	+ '46	'550
'5451	- '73	'083	'3846	+ '40	'010	'4857	- '17	'278	'5896	+ '46	'554
'5465	- '68	'087	'3860	+ '35	'014				'5910	+ '51	'557
'5479	- '75	'090	'3874	+ '27	'018	plate 5982		'691	'5923	+ '46	'561
plate 5949		'655	'3887	+ '25	'021				'5937	+ '45	'565
			'3901	+ '19	'025	30462'4940	- '11	'300	'5951	+ '45	'568
			'3915	+ '12	'029	'4954	- '11	'304	'5965	+ '45	'572
30443'5555	- '79	'110	'3929	- '01	'032	'4968	- '13	'308	'5979	+ '46	'576
'5569	- '81	'114	'3943	- '02	'036	'4982	- '08	'311	'5992	+ '44	'579
'5583	- '79	'118	'3957	- '08	'040	'4995	- '07	'315	'6007	+ '48	'583
'5597	- '78	'122	'3970	- '17	'043	'5009	- '04	'319	'6020	+ '51	'587
'5611	- '72	'125	'3984	- '24	'047	'5023	- '03	'322	'6034	+ '43	'590
'5624	- '71	'129	'3998	- '30	'051	'5037	- '04	'326	'6048	+ '47	'594
'5638	- '75	'132	'4012	- '38	'054	'5051	- '00	'330	'6062	+ '47	'598
'5652	- '72	'136	'4026	- '46	'058	'5065	- '03	'333	'6076	+ '47	'601
'5666	- '70	'140	'4040	- '53	'062	'5079	- '00	'337	'6090	+ '51	'605
'5680	- '65	'144	'4054	- '53	'066	'5092	+ '01	'341	'6104	+ '39	'609
'5694	- '57	'147	'4067	- '59	'069	'5106	+ '05	'344	'6117	+ '44	'612

TABLE 9 (continued)

J. D. Hel. - 2400000	Δm	phase	J. D. Hel. - 2400000	Δm	phase	J. D. Hel. - 2400000	Δm	phase	J. D. Hel. - 2400000	Δm	phase
d 30462 ⁶ 131	+ '45	P ⁶ 16	d 30463 ⁴ 559	+ '72	P ⁸ 50	d 30465 ⁴ 352	- '80	P ⁹ 95	d 30486 ⁵ 474	- '29	P ⁰ 46
'6145	+ '50	'620	'4573	+ '68	'853	'4366	- '82	'099	'5492	- '32	'050
'6159	+ '51	'623	'4587	+ '76	'857	'4380	- '79	'102	'5509	- '41	'055
'6173	+ '52	'627	'4601	+ '65	'861	'4394	- '81	'106	'5526	- '48	'059
'6187	+ '51	'631				'4408	- '81	'110	'5544	- '55	'064
'6200	+ '51	'634	plate 5989		'693				'5561	- '63	'069
'6214	+ '48	'638				plate 6015		'698	'5578	- '68	'073
plate 5984		'691	30463 ⁴ 656	+ '62	'875				'5596	- '70	'078
			'4670	+ '64	'879	30466 ⁵ 135	+ '59	'953	'5613	- '77	'082
			'4684	+ '63	'883	'5149	+ '71	'956	'5630	- '77	'087
30462 ⁶ 291	+ '47	'658	'4698	+ '74	'886	'5163	+ '60	'960	'5647	- '82	'091
'6304	+ '47	'662	'4712	+ '68	'890	'5177	+ '69	'964	'5665	- '82	'096
'6318	+ '51	'666	'4726	+ '67	'894	'5191	+ '63	'967	'5682	- '86	'101
'6332	+ '50	'669	'4740	+ '66	'897	'5204	+ '68	'971	'5699	- '87	'105
'6346	+ '51	'673	'4753	+ '68	'901	'5218	+ '62	'975	'5717	- '82	'110
'6360	+ '47	'677	'4767	+ '69	'905	'5232	+ '57	'978	'5734	- '89	'114
'6374	+ '44	'680	'4781	+ '71	'908	'5246	+ '52	'982	'5751	- '92	'119
'6387	+ '46	'684	'4795	+ '67	'912	'5260	+ '54	'986	'5769	- '87	'124
'6401	+ '54	'688	'4809	+ '64	'916	'5274	+ '49	'989			
'6415	+ '48	'691	'4823	+ '73	'919	'5288	+ '53	'993	plate 6047		'739
'6429	+ '48	'695	'4836	+ '73	'923	'5301	+ '54	'997			
'6443	+ '52	'699	'4850	+ '75	'927	'5315	+ '43	'000	30488 ⁴ 020	+ '72	'961
'6457	+ '53	'702	'4864	+ '65	'930	'5329	+ '39	'004	'4038	+ '75	'965
'6471	+ '58	'706	'4878	+ '73	'934	'5343	+ '37	'008	'4072	+ '73	'974
'6484	+ '49	'710	'4892	+ '75	'938	'5357	+ '33	'011	'4089	+ '67	'979
'6498	+ '55	'713	'4906	+ '62	'941	'5371	+ '29	'015	'4107	+ '64	'984
'6512	+ '50	'717	'4920	+ '62	'945	'5385	+ '23	'019	'4124	+ '66	'988
'6526	+ '50	'721	'4933	+ '63	'949	'5398	+ '17	'022	'4141	+ '61	'993
plate 5988		'692	'4947	+ '61	'952	'5412	+ '08	'026	'4159	+ '54	'997
			plate 6006		'696	'5426	'00	'030	'4176	+ '52	'002
30463 ⁴ 005	+ '60	'703				'5440	- '02	'033	'4193	+ '43	'006
'4019	+ '55	'706	30465 ³ 812	+ '69	'952	'5454	- '08	'037	'4211	+ '47	'011
'4033	+ '52	'710	'3826	+ '63	'956	'5468	- '17	'041	'4228	+ '38	'016
'4047	+ '59	'714	'3840	+ '61	'959	'5481	- '15	'044	'4245	+ '29	'020
'4061	+ '53	'718	'3854	+ '61	'963	'5495	- '33	'048	'4263	+ '22	'025
'4075	+ '65	'721	'3868	+ '57	'967	'5509	- '38	'052	'4280	+ '21	'029
'4089	+ '58	'725	'3881	+ '66	'970	'5523	- '42	'055	'4297	+ '11	'034
'4102	+ '58	'728	'3895	+ '62	'974	'5537	- '42	'059	'4315	- '02	'039
'4116	+ '60	'732	'3909	+ '58	'978	'5551	- '47	'063	'4332	- '06	'043
'4130	+ '64	'736	'3923	+ '50	'981	'5565	- '55	'067	'4349	- '12	'048
'4144	+ '58	'740	'3937	+ '50	'985	'5578	- '61	'070	'4366	- '21	'052
'4158	+ '56	'743	'3951	+ '55	'989	'5592	- '64	'074	'4384	- '29	'057
'4172	+ '56	'747	'3965	+ '46	'992	'5606	- '65	'077	'4401	- '37	'061
'4186	+ '63	'751	'3978	+ '51	'996	'5620	- '68	'081	'4418	- '39	'066
'4199	+ '57	'754	'3992	+ '40	'000	'5634	- '66	'085	'4436	- '47	'071
'4213	+ '58	'758	'4006	+ '39	'003	'5648	- '71	'089	'4453	- '51	'075
'4227	+ '58	'762	'4020	+ '37	'007	'5662	- '74	'092	'4470	- '57	'080
'4241	+ '62	'765	'4034	+ '39	'011	'5675	- '75	'096	'4488	- '64	'085
'4255	+ '58	'769	'4048	+ '32	'014	'5689	- '72	'099	'4505	- '68	'089
'4269	+ '57	'773	'4061	+ '34	'018	'5703	- '80	'103	'4522	- '73	'094
'4282	+ '56	'776	'4075	+ '22	'022	plate 6045		'735	'4540	- '76	'098
'4296	+ '62	'780	'4089	+ '13	'025				'4557	- '81	'103
'4310	+ '66	'784	'4103	+ '06	'029	30486 ⁵ 163	+ '68	'963	'4574	- '75	'107
'4324	+ '57	'787	'4117	- '01	'033	'5180	+ '59	'968	'4592	- '80	'112
'4338	+ '60	'791	'4131	- '06	'036	'5197	+ '63	'972	'4609	- '78	'117
'4352	+ '53	'795	'4145	- '14	'040	'5215	+ '62	'977	'4626	- '78	'121
'4366	+ '57	'798	'4158	- '18	'044	'5232	+ '59	'981	'4644	- '79	'126
'4379	+ '67	'802	'4172	- '34	'047	'5249	+ '50	'986	'4661	- '79	'130
'4393	+ '60	'806	'4186	- '40	'051	'5267	+ '57	'991	'4678	- '77	'135
'4407	+ '63	'809	'4200	- '44	'055	'5284	+ '53	'995	'4695	- '70	'139
'4421	+ '68	'813	'4214	- '48	'058	'5301	+ '41	'000	'4713	- '71	'144
'4435	+ '57	'817	'4228	- '59	'062	'5318	+ '42	'004	'4730	- '71	'149
'4449	+ '59	'820	'4242	- '62	'066	'5336	+ '35	'009	'4747	- '71	'153
'4463	+ '63	'824	'4255	- '63	'069	'5353	+ '29	'013	'4765	- '71	'158
'4476	+ '63	'828	'4269	- '67	'073	'5370	+ '24	'018	plate 6067		'787
'4490	+ '69	'831	'4283	- '66	'077	'5388	+ '18	'023			
'4504	+ '73	'835	'4297	- '71	'080	'5405	+ '06	'027	30514 ⁴ 362	+ '78	'955
'4518	+ '60	'839	'4311	- '76	'084	'5422	+ '07	'032	'4380	+ '81	'960
'4532	+ '66	'842	'4325	- '76	'088	'5440	- '03	'037	'4397	+ '69	'964
'4546	+ '71	'846	'4339	- '85	'092	'5457	- '18	'041	'4414	+ '63	'969

TABLE 9 (continued)

J. D. Hel. - 2400000	Δm	phase	J. D. Hel. - 2400000	Δm	phase	J. D. Hel. - 2400000	Δm	phase	J. D. Hel. - 2400000	Δm	phase
d 30514 4431	+ '67	P	d 30517 5113	- '79	P	d 30790 5618	+ '60	P	plate 6304		303
4466	+ '62	'973	5131	- '78	'105	5632	+ '48	'731	d	m	P
4483	+ '64	'983	5148	- '84	'109	5646	+ '55	'734	30791 5100	- '17	'243
4501	+ '62	'992	5165	- '80	'114	5660	+ '53	'738	5114	- '10	'247
4518	+ '61	'996	5183	- '79	'118	5674	+ '48	'742	5127	- '23	'251
4535	+ '60	'001	5200	- '74	'123	5688	+ '31	'745	5141	- '14	'254
4553	+ '52	'006	5217	- '84	'128	5701	+ '44	'749	5155	- '12	'258
4570	+ '47	'010	5234	- '73	'132	5715	+ '65	'753	5169	- '04	'262
4587	+ '45	'015	5252	- '73	'137			'756	5183	- '13	'265
4605	+ '43	'020	5269	- '71	'141	plate 6296		301	5197	- '01	'269
4622	+ '28	'024	5286	- '74	'146				5211	- '02	'273
4639	+ '21	'029			'150	30790 6075	+ '57	'852	5224	- '10	'276
4657	+ '17	'033	plate 6121		819	6089	+ '62	'855	5238	- '07	'280
4674	+ '08	'038				6103	+ '63	'859	5252	- '04	'284
4691	- '04	'042				6117	+ '52	'863	5266	- '03	'287
4709	- '11	'047	30531 4318	+ '67	'996	6131	+ '48	'866	5280	- '05	'291
4726	- '24	'052	4335	+ '59	'001	6145	+ '56	'870	5294	- '01	'295
4743	- '30	'056	4352	+ '62	'005	6158	+ '51	'874	5308	- '05	'299
4760	- '41	'061	4370	+ '47	'010	6172	+ '60	'877	5321	+ '02	'302
4778	- '42	'065	4387	+ '48	'014	6186	+ '54	'881	5335	- '01	'306
4795	- '50	'070	4404	+ '46	'019	6200	+ '56	'885	5349	- '03	'309
4812	- '62	'074	4422	+ '42	'024	6214	+ '56	'888	5363	+ '07	'313
4830	- '60	'079	4439	+ '31	'028	6228	+ '61	'892	5377	- '01	'317
4847	- '65	'084	4456	+ '22	'033	6242	+ '55	'896	5391	+ '05	'321
4864	- '69	'088	4473	+ '20	'037	plate 6297		301	5404	+ '06	'324
4882	- '63	'093	4491	+ '16	'042				5418	+ '07	'328
4899	- '79	'097	4508	+ '10	'046	30790 6332	+ '67	'920	5432	+ '04	'331
4916	- '74	'102	4525	- '02	'051	6346	+ '57	'923	5446	+ '10	'335
4934	- '74	'107	4543	- '13	'056	6359	+ '65	'927	5460	+ '10	'339
4951	- '81	'111	4560	- '24	'060	6373	+ '50	'931	5474	+ '08	'343
4968	- '75	'116	4577	- '33	'065	6387	+ '65	'934	5488	+ '09	'346
4986	- '75	'121	4595	- '38	'070	6401	+ '55	'938	5501	+ '09	'350
5003	- '72	'125	4612	- '44	'074	6415	+ '47	'942	5515	+ '18	'353
5020	- '70	'130	4629	- '58	'079	6429	+ '44	'945	5529	+ '17	'357
5037	- '72	'134	4647	- '56	'083	6442	+ '44	'949	5543	+ '23	'361
plate 6097		793	4664	- '64	'088	6456	+ '40	'953	5557	+ '12	'365
			4681	- '72	'092	6470	+ '32	'956	5571	+ '22	'368
			plate 6294		301	6484	+ '33	'960	5585	+ '24	'372
30517 4542	+ '67	'953				6498	+ '30	'964	5598	+ '21	'375
4559	+ '72	'958	30790 5189	+ '46	'617	6512	+ '29	'967	5612	+ '19	'379
4577	+ '70	'963	5203	+ '51	'621	6526	+ '19	'971	5626	+ '27	'383
4594	+ '59	'967	5217	+ '53	'624	6539	+ '22	'975	5640	+ '22	'387
4611	+ '68	'972	5230	+ '47	'628	6553	'00	'978	5654	+ '14	'390
4628	+ '63	'976	5244	+ '48	'631	6567	'00	'982	5668	+ '20	'394
4646	+ '71	'981	5258	+ '55	'635	6581	- '02	'986	5681	+ '22	'397
4663	+ '60	'985	5272	+ '58	'639	6595	- '18	'989	5695	+ '20	'401
4680	+ '57	'990	5286	+ '46	'643	6609	- '11	'993	plate 6305		303
4698	+ '58	'995	5300	+ '49	'646	6623	- '11	'997	30791 5799	+ '29	'429
4715	+ '66	'999	5314	+ '60	'650	6636	- '17	'000	5813	+ '27	'432
4732	+ '62	'004	5327	+ '55	'653	6650	- '27	'004	5827	+ '33	'436
4750	+ '49	'008	5341	+ '45	'657	6664	- '31	'008	5841	+ '26	'440
4767	+ '48	'013	5355	+ '54	'661	6678	- '31	'011	5855	+ '35	'443
4784	+ '42	'017	5369	+ '58	'665	6692	- '35	'015	5869	+ '42	'447
4802	+ '30	'022	5383	+ '41	'668	6706	- '48	'019	5882	+ '24	'451
4819	+ '22	'027	5397	+ '51	'672	6719	- '49	'022	5896	+ '29	'454
4836	+ '17	'031	5411	+ '52	'676	6733	- '52	'026	5910	+ '27	'458
4854	+ '08	'036	5424	+ '51	'679	6747	- '56	'030	5924	+ '41	'462
4871	- '01	'041	5438	+ '45	'683	6761	- '59	'033	5938	+ '44	'465
4888	- '12	'045	5452	+ '55	'687	6775	- '58	'037	5952	+ '29	'469
4905	- '22	'050	5466	+ '54	'690	6789	- '60	'041	5965	+ '24	'473
4923	- '25	'054	5480	+ '33	'694	6803	- '62	'045	5979	+ '33	'476
4940	- '37	'059	5494	+ '42	'698	6816	- '71	'048	5993	+ '34	'480
4957	- '48	'063	5507	+ '54	'701	6830	- '75	'052	6007	+ '35	'484
4975	- '52	'068	5521	+ '51	'705	6844	- '71	'055	6021	+ '39	'487
4992	- '59	'073	5535	+ '54	'709	6858	- '76	'059	6035	+ '44	'491
5009	- '63	'077	5549	+ '48	'712	6872	- '78	'063	6049	+ '45	'495
5027	- '69	'082	5563	+ '51	'716	6886	- '79	'067	6062	+ '37	'498
5044	- '71	'086	5577	+ '42	'720	6900	- '73	'070	6076	+ '43	'502
5061	- '76	'091	5591	+ '43	'723	6913	- '71	'074	6090	+ '38	'506
5079	- '80	'096	5604	+ '45	'727	6927	- '79	'077			
5096	- '78	'100									

TABLE 9 (continued)

J. D. Hel. — 2400000	Δm	phase	J. D. Hel. — 2400000	Δm	phase	J. D. Hel. — 2400000	Δm	phase	J. D. Hel. — 2400000	Δm	phase
d	m	P	d	m	P	d	m	P	d	m	P
30791 ⁶ 104	+ '40	'509	30812 ⁵ 762	— '64	'072	30849 ⁵ 243	+ '05	'990	31144 ⁶ 439	— '92	'103
'6118	+ '42	'513	'5783	— '63	'078	'5264	— '03	'996	'6453	— '82	'106
'6132	+ '52	'517	'5804	— '67	'083	'5284	— '09	'001	'6466	— '83	'110
'6146	+ '50	'521	'5825	— '58	'089	'5305	— '17	'007			
'6159	+ '46	'524	'5845	— '66	'094	'5326	— '20	'012	plate 6565		'012
'6173	+ '37	'528	'5866	— '61	'100	'5347	— '29	'018			
'6187	+ '43	'531	'5887	— '57	'105	'5368	— '38	'023	31172 ⁵ 070	+ '70	'944
'6201	+ '40	'535	'5908	— '64	'111	'5388	— '44	'029	'5084	+ '69	'948
'6215	+ '50	'539				'5409	— '56	'034	'5098	+ '66	'952
'6229	+ '41	'543	plate 6393		'411	'5430	— '61	'040	'5112	+ '64	'955
'6242	+ '46	'546				'5451	— '59	'045	'5126	+ '65	'959
'6256	+ '46	'550	30849 ³ 948	+ '53	'647	'5471	— '65	'051	'5139	+ '66	'962
'6270	+ '48	'553	'3969	+ '55	'653	'5492	— '71	'056	'5153	+ '64	'966
'6284	+ '42	'557	'3989	+ '51	'658	'5513	— '76	'062	'5167	+ '63	'970
'6298	+ '35	'561	'4010	+ '54	'663	'5534	— '78	'067	'5181	+ '50	'974
'6312	+ '40	'565	'4031	+ '50	'669	'5554	— '80	'073	'5195	+ '50	'977
'6326	+ '47	'568	'4052	+ '49	'675	'5575	— '74	'078	'5209	+ '53	'981
'6339	+ '45	'572	'4072	+ '52	'680	'5596	— '76	'084	'5222	+ '57	'984
'6353	+ '43	'575	'4093	+ '47	'685	'5617	— '78	'089	'5236	+ '52	'988
'6367	+ '40	'579	'4114	+ '56	'691	'5638	— '73	'095	'5250	+ '45	'992
'6381	+ '46	'583	'4135	+ '53	'697	'5658	— '74	'100	'5264	+ '50	'996
'6395	+ '55	'587	'4156	+ '58	'702	'5679	— '76	'106	'5278	+ '35	'999
plate 6319		'310	'4176	+ '54	'707	'5700	— '72	'111	'5292	+ '40	'003
			'4197	+ '53	'713	'5721	— '64	'117	'5306	+ '37	'007
			'4218	+ '54	'719	'5741	— '72	'122	'5319	+ '30	'010
30795 ⁵ 238	+ '67	'881	'4239	+ '58	'724	'5762	— '68	'128	'5333	+ '20	'014
'5259	+ '69	'886	'4259	+ '54	'729	'5783	— '64	'133	'5347	+ '25	'018
'5280	+ '67	'892	'4280	+ '60	'735				'5361	+ '20	'021
'5300	+ '73	'897	'4301	+ '52	'741	plate 6562		'960	'5375	+ '15	'025
'5321	+ '68	'903	'4322	+ '56	'746				'5403	+ '03	'032
'5342	+ '67	'908	'4343	+ '55	'752	31144 ⁵ 871	+ '79	'952	'5416	— '03	'036
'5363	+ '56	'914	'4363	+ '60	'757	'5885	+ '78	'956	'5430	— '10	'040
plate 6354		'342	'4384	+ '60	'763	'5899	+ '74	'960	'5444	— '18	'043
			'4405	+ '54	'768	'5912	+ '73	'963	'5458	— '25	'047
			'4426	+ '64	'774	'5926	+ '72	'967	'5472	— '37	'051
30812 ⁵ 014	+ '78	'874	'4446	+ '61	'779	'5940	+ '75	'970	'5486	— '37	'054
'5035	+ '75	'879	'4467	+ '58	'785	'5954	+ '72	'974	'5499	— '41	'058
'5056	+ '74	'885	'4488	+ '61	'790	'5968	+ '62	'978	'5513	— '48	'062
'5077	+ '70	'891	'4509	+ '56	'796	'5982	+ '67	'981	'5527	— '56	'065
'5097	+ '75	'896	'4530	+ '59	'801	'5995	+ '65	'985	'5541	— '59	'069
'5118	+ '75	'901	'4550	+ '59	'807	'6009	+ '67	'989	'5555	— '63	'073
'5139	+ '72	'907	'4571	+ '58	'812	'6023	+ '59	'992	'5569	— '65	'076
'5160	+ '67	'913	'4592	+ '61	'818	'6037	+ '49	'996	'5583	— '68	'080
'5181	+ '63	'918	'4613	+ '61	'823	'6051	+ '50	'000	'5596	— '69	'084
'5201	+ '66	'923	'4633	+ '71	'829	'6065	+ '47	'003	'5610	— '73	'087
'5222	+ '65	'929	'4654	+ '68	'834	'6079	+ '50	'007	'5624	— '71	'091
'5243	+ '60	'935	'4675	+ '64	'840	'6092	+ '43	'011	'5638	— '74	'095
'5264	+ '68	'940	'4696	+ '71	'845	'6106	+ '43	'014	'5652	— '78	'098
'5284	+ '57	'945	'4717	+ '66	'851	'6120	+ '31	'018	'5666	— '62	'102
'5305	+ '57	'951	'4737	+ '67	'856	'6134	+ '30	'022			
'5326	+ '55	'957	'4758	+ '71	'862	'6148	+ '28	'025	plate 6583		'064
'5347	+ '45	'962	'4779	+ '65	'867	'6162	+ '11	'029			
'5368	+ '48	'968	'4800	+ '71	'873	'6176	+ '19	'033	31200 ⁴ 303	+ '64	'945
'5388	+ '38	'973	'4820	+ '71	'878	'6189	+ '08	'036	'4320	+ '65	'950
'5409	+ '31	'979				'6203	+ '00	'040	'4338	+ '66	'954
'5430	+ '26	'984	plate 6394		'411	'6217	— '03	'044	'4355	+ '61	'959
'5451	+ '16	'990				'6231	— '05	'047	'4372	+ '51	'963
'5471	+ '05	'995	30849 ⁴ 952	+ '70	'913	'6245	— '16	'051	'4390	+ '53	'968
'5492	+ '05	'001	'4973	+ '63	'919	'6259	— '24	'055	'4407	+ '42	'973
'5513	— '08	'006	'4994	+ '68	'924	'6272	— '23	'058	'4424	+ '55	'977
'5534	— '18	'012	'5014	+ '63	'930	'6286	— '34	'062	'4442	+ '47	'982
'5554	— '20	'017	'5035	+ '61	'935	'6300	— '38	'066	'4459	+ '39	'987
'5575	— '31	'023	'5056	+ '61	'941	'6314	— '45	'069	'4476	+ '36	'991
'5596	— '33	'028	'5077	+ '55	'946	'6328	— '48	'073	'4494	+ '43	'996
'5617	— '43	'034	'5097	+ '57	'952	'6342	— '62	'077	'4511	+ '33	'000
'5638	— '44	'039	'5118	+ '49	'957	'6356	— '65	'081	'4528	+ '20	'005
'5658	— '51	'045	'5139	+ '44	'963	'6369	— '73	'084	'4546	+ '21	'010
'5679	— '50	'050	'5160	+ '36	'968	'6383	— '75	'088	'4563	+ '20	'014
'5700	— '50	'056	'5181	+ '29	'974	'6397	— '76	'091	'4580	+ '07	'019
'5721	— '56	'061	'5201	+ '27	'979	'6411	— '78	'095	'4597	+ '06	'023
'5741	— '62	'067	'5222	+ '17	'985	'6425	— '82	'099	'4615	+ '00	'028